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MEGHNA ESTUARY STUDY

TECHNICAL NOTE MES-017

NUMERICAL MODELLING

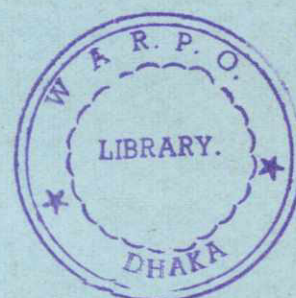
August 1998

DHV CONSULTANTS BV

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KAMPSAX INTERNATIONAL
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MINISTRY OF WATER RESOURCES
BANGLADESH WATER DEVELOPMENT BOARD

MEGHNA ESTUARY STUDY

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Technical Note on:

**NUMERICAL MODELLING OF
HYDRODYNAMICS, SALINITY, WAVES AND SEDIMENT TRANSPORT
IN THE MEGHNA ESTUARY**

Dhaka , June 1998

Project Name : Meghna Estuary Study (MES)

Location : Meghna Estuary

Key words : Bathymetries, Model Set-up, Base Line Simulations,
Simulation with Interventions, Salinity Modelling,
Wind-Wave Modelling, Sediment Transport Modelling

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Executive Summary

Meghna Estuary Study (MES) is a component (FAP5B) of the Flood Action Plan. The study was executed from late 1995 till mid 1998 by Government of Bangladesh, Ministry of Water Resources, represented by Bangladesh Water Development Board (BWDB). DHV, The Netherlands, with associates, participated as a Consultant. Financial support for the project was granted by DGIS, The Netherlands, and Danida, Denmark.

The present report describes the numerical hydraulic modelling, which was carried out as a part of the study by Surface Water Modelling Centre (SWMC) and Danish Hydraulic Institute (DHI). Both institutes participated in the MES project organisation as specialist sub-consultants to DHV.

The purpose of the numerical hydraulic modelling was to establish a tool for description of present and future hydraulic conditions in the study area. The results are required in connection with

- assessment and comparison of development scenarios; and
- impact evaluation and design of various specific schemes.

Numerical hydraulic models have been established for the Meghna Estuary in connection with other studies. However, at the early stages of MES it was realised that the bathymetric data basis on which these models were made had grown partly obsolete and inconsistent due to the dynamic morphological environment. Therefore the modelling was suspended while a comprehensive bathymetric survey was carried out.

With the new bathymetric survey data the hydrodynamic model was set-up, calibrated and validated against available measurements. Also a local hydraulic model for the Nijhum Dwip area was set-up.

In addition to the hydrodynamic models a salinity model, a wind-wave model and a sediment transport model for the study area were set-up.

All together this comprehensive model suite constitutes a valuable and versatile tool for impact assessment in connection with the development of the estuary.

Within the present study a number of intervention scenarios were modelled and key parameters extracted for analysis and interpretation within other study tasks.

On-the-job supervision of SWMC staff by the DHI numerical modelling specialist was carried out throughout the project period. It is recommended that formal training in the further development and application of the models are made.

At the end of the study period emphasis was put on making the model suite, together with the results already obtained, readily available for future use by setting up a CD-ROM archive.

Finally, in order to visualise the results, a presentation was made on CD-ROM (for viewing in a web browser) containing the main parts of the present report together with animation of key results.



Abbreviations

ADCP	Acoustic Doppler Current Profiler
ATT	Admiralty Tide Tables
BITWA	Bangladesh Inland Water Transport Authority
BMD	Bangladesh Meteorological Department
BTM	Bangladesh Transverse Mercator
BUET	Bangladesh University of Engineering and Technology
BWDB	Bangladesh Water Development Board
CD	Chart Datum
CSPS	Cyclone Shelter Preparatory Study
DANIDA	Danish International Development Agency
DGIS	Directorate General for International Cooperation, The Netherlands
DHI	Danish Hydraulic Institute
DHV	DHV Consultants BV
EGIS	Environmental and Geographic Information System support Project
FAP4	Southwest Area Water Resources Management Project
FAP5B	Flood Action Plan project 5B (same as Meghna Estuary Study)
FPCO	Flood Plan Coordination Organisation
GOB	Government of Bangladesh
IFCDR	Institute of Flood Control and Drainage Research (BUET)
KMS	Kort- og Matrikelstyrelsen
LGED	Local Government Engineering Department
LRP	Land Reclamation Project
MES	Meghna Estuary Study
MIKE 21	2 Dimensional Modelling System developed by DHI
MIKE 21 AD	Advection-Dispersion Module of MIKE 21
MIKE 21 HD	Hydrodynamic Module of MIKE 21
MIKE 21 NSW	Nearshore Spectral Wind-Wave Module of MIKE 21
MIKE 21 ST	Sand Sediment Transport Module of MIKE 21
PWD	Public Works Datum
RTK	Real Time Kinematics
SSD	Survey and Study Division (of BWDB)
SPM	Shore Protection Manual
SSE	South-Southeast
SSW	South-Southwest
SWMC	Surface Water Modelling Centre

1 Introduction

1.1 Background

Meghna Estuary Study (MES) is a component (FAP5B) of the Flood Action Plan. The study was executed from late 1995 till mid 1998 by Government of Bangladesh, Ministry of Water Resources, represented by Bangladesh Water Development Board (BWDB). DHV, The Netherlands, with associates, participated as a Consultant. Financial support for the project was granted by DGIS, The Netherlands, and Danida, Denmark.

MES built on results of the Land Reclamation Project (LRP), which was executed by BWDB from 1977 to 1991. The development objectives of MES are to increase the physical safety and social security of the some two million inhabitants of the study area, and to promote sustainable development in the coastal areas and on the islands. The immediate objectives are

- to enhance and strengthen operational knowledge of hydraulic and morphological processes in the Meghna Estuary;
- to find suitable land reclamation and bank protection methods;
- to increase the capacity of BWDB to reclaim new land and protect the eroding river banks; and
- to prepare a plan with priority projects and programmes for flood protection, agricultural and socio-economic development for early implementation.

The present report describes the numerical hydraulic modelling, which was carried out as a part of the study by Surface Water Modelling Centre (SWMC) and Danish Hydraulic Institute (DHI). Both institutes participated in the MES project organisation as specialist sub-consultants to DHV.

1.2 Objectives

The numerical model can describe water levels, flow rates and current velocities, salinities, and mass budgets for solutes, as well as waves and erosive capacity. The model was established as a tool for description of present and future hydraulic conditions in the study area. The results of the modelling are required in connection with

- assessment and comparison of development scenarios; and
- impact evaluation and design of various specific schemes.

During MES, the model was applied for these purposes. Upon completion of the study, the model remains as a tool that can be used in connection with the future development of Meghna Estuary, at the general planning level as well as at the individual project level.

2 Methodology

2.1 Background

The model that was set-up, calibrated and applied for MES is the most recent in a series of numerical hydraulic models of the Estuary. In addition to LRP, previous studies comprise

- Pussur-Sibsa River and Karnafuli Entrance, Ministry of Shipping (1989-92);
- Numerical Simulation of Tides and Saline Water Intrusion, IFCDR, BUET (1989);
- Cyclone Protection Project II, BWDB (1990-91);
- Southwest Area Water Resources Management Project (FAP4), FPCO (1991-93); and
- Cyclone Shelter Preparatory Study (CSPS), Phases I and II, LGED (1995-98).

All these studies involved application of the same modelling system (DHI's MIKE 21, previously named System 21), in a set-up which was gradually upgraded in the course of time. In this connection, large amounts of data and information have been compiled.

Satellite imagery analyses made by EGIS for MES in 1996 showed, however, that the planform of the estuary had changed comprehensively in recent years due to its dynamic morphological environment. Against expectations, the data basis that was available at the time had grown partly obsolete and inconsistent, which caused considerable difficulties in connection with the CSPS model calibration. Further, during that project, it appeared that it was difficult to identify the reference level for the estimated storm surge heights in the field. This was a main reason for initiating the joint CSPS/MES geodetic survey in the area, which took place in the first half of 1996. At the same time, it was decided to suspend the MES modelling activities until better data had been produced. The work was discontinued temporarily, while nearly the entire study area was surveyed by MES from BWDB/SSD's vessel 'Anwesha'.

The MES model, as described in this report, is based on planform, bathymetry and calibration data from 1996-97. Therefore, it is superior to former models with respect to description of present conditions in the area.

2.2 Modelling Procedure

Where earlier models had adopted a nested grid philosophy i.e. with models covering not only the Meghna Estuary but also the northern part of the Bay of Bengal, it was decided to concentrate only on the Meghna Estuary in the present study. In this way it was anticipated that calibration problems which were experienced in the earlier models and which were made more complicated through the use of a nested model approach could be avoided.

Furthermore it was decided to calibrate the model not only against tidal water level variations as earlier models had been, but also against actual water level measurements combined with flow measurements. The measurements and the new bathymetric survey data would constitute a coherent set of model data thus facilitating an improved model calibration.

The area covered by the numerical model is shown in figure 2.1.

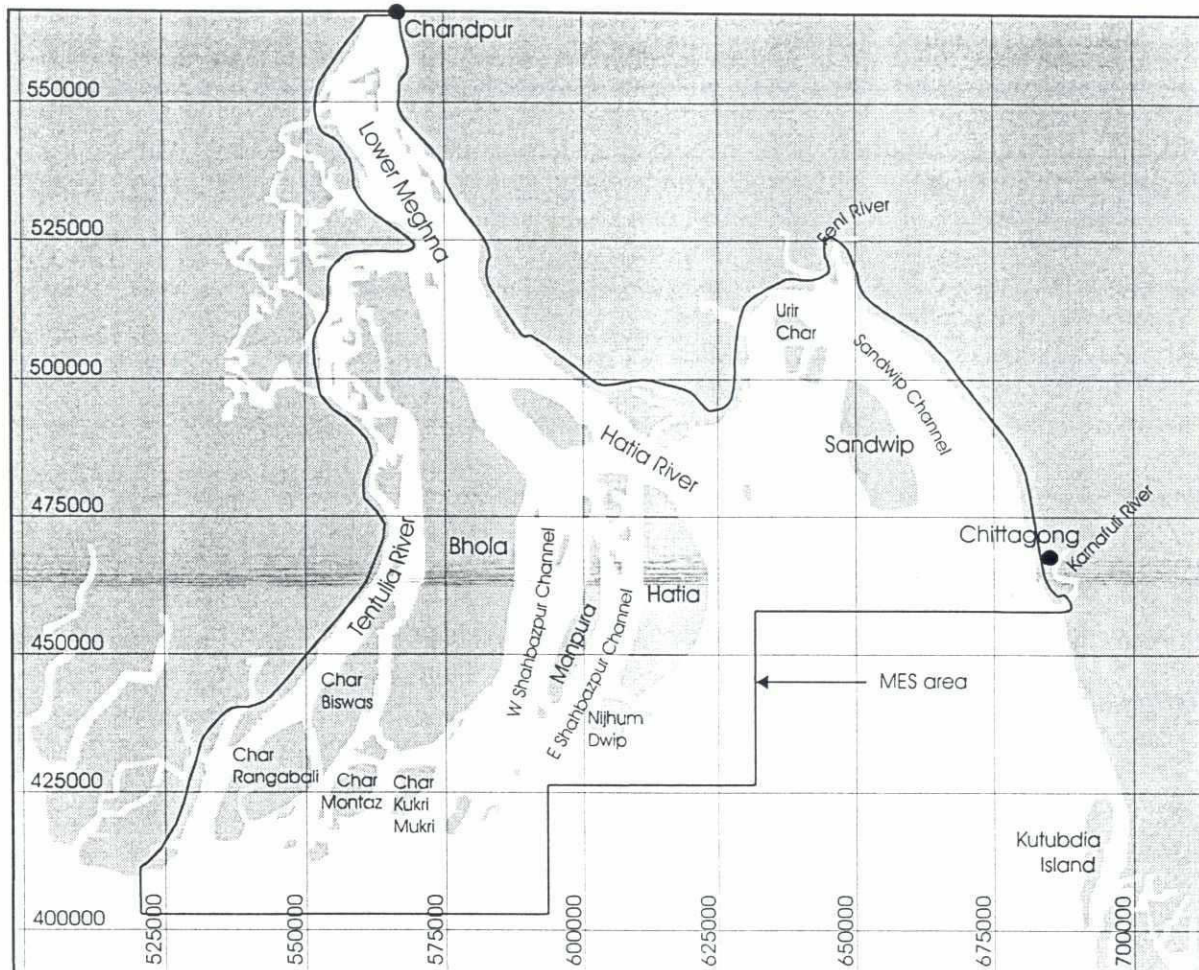
The grid spacing of the model was selected on the basis of:

- required resolution of the flow field within the estuary
- available computer resources

On this basis a resolution of 600 meters in the whole of the estuary was chosen with local models having a resolution (i.e grid spacing) of 200 meters.



Figure 2.1 Area covered by the numerical model



The model has two open boundaries:

- one at Chandpur to the North, where water level measurements were available
- and one to the South, where water level predictions were available at Kutubdia Island.

As the flow in the estuary differs considerable from the dry season to the monsoon season one calibration period was selected for each of these seasons. Furthermore two validation periods were selected, one from each season.

The procedure for the hydrodynamic modelling consisted of the following steps:

- making a bathymetry based on the new survey data combined with satellite imagery and other data sources
- calibration and validation
- applying the model for a number of periods with known conditions (base runs)
- applying the model for a number of selected scenarios (including intervention schemes)

In addition to hydrodynamic modelling also salinity modelling, wave modelling and sediment transport modelling were conducted for the study area.

A calibration of the salinity model was carried out while no data were available for a calibration of the wind-wave model.

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Calibrating the sediment transport model was outside the scope of the present study. The results of this model are therefore to be considered as indicative only.

2.3 MIKE 21 Modelling System

For all types of modelling carried out during the numerical modelling study DHI's Modelling System for two-dimensional flows in one layer, MIKE 21, was applied. MIKE 21 is a software package containing a comprehensive modelling system for 2D free-surface flows. MIKE 21 is applicable to the simulation of hydraulic and related phenomena in lakes, estuaries, bays, coastal areas and seas where stratification can be neglected.

For the present study four different modules of MIKE 21 were applied:

- The Hydrodynamic Module, MIKE 21 HD
- The Advection-Dispersion Module, MIKE 21 AD
- The Nearshore Spectral Wind-wave Module, MIKE 21 NSW and
- The Non-cohesive Sediment Transport Module, MIKE 21 ST

Each of these modules are described in Appendices A to D.

2.4 Overview of Model Simulations

The following model simulations were carried out during the study:

Existing situation (ie with no interventions)

- Hydrodynamic simulations, each 17 days (the whole model area):
 - Dry season 1996 (calibration period and base run)
 - Monsoon season 1996 (validation period)
 - Dry season 1997 (validation period)
 - Monsoon season 1997 (calibration period and base run)
- Hydrodynamic simulation, 2 days during spring tide (local model around Nijhum Dwip):
 - Dry season 1996
- Salinity simulation, 17 days (the whole model area):
 - Dry season 1996
- Wind-wave simulations, stationary conditions (whole model area):
 - wind of 8 m/s from SSE (water level corresponding to monsoon season 1997)
 - wind of 8 m/s from SSW (water level corresponding to monsoon season 1997)
- Sediment Transport simulations (whole model area):
 - Dry season 1996, spring tide, no waves
 - Dry season 1996, neap tide, no waves
 - Monsoon season 1997, spring tide, waves from SSE
 - Monsoon season 1997, spring tide, waves from SSW
 - Monsoon season 1997, neap tide, waves from SSE
 - Monsoon season 1997, neap tide, waves from SSW

Including interventions 1 and 3 (see figure 6.1)

- Hydrodynamic simulations, each 17 days (the whole model area):
 - Dry season 1996
 - Monsoon season 1997
- Hydrodynamic simulation, 2 days during spring tide (local model around Nijhum Dwip):
 - Dry season 1996

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Including all interventions except 8 (see figure 6.1)

- Hydrodynamic simulations, each 17 days (the whole model area):
 - Dry season 1996
 - Monsoon season 1997

Including all interventions (see figure 6.1)

- Hydrodynamic simulations, each 17 days (the whole model area):
 - Dry season 1996
 - Monsoon season 1997
- Hydrodynamic simulation, 2 days during spring tide (local model around Nijhum Dwip):
 - Dry season 1996
- Salinity simulation, 17 days (the whole model area):
 - Dry season 1996

The simulations are described in Chapters 4 through 9.

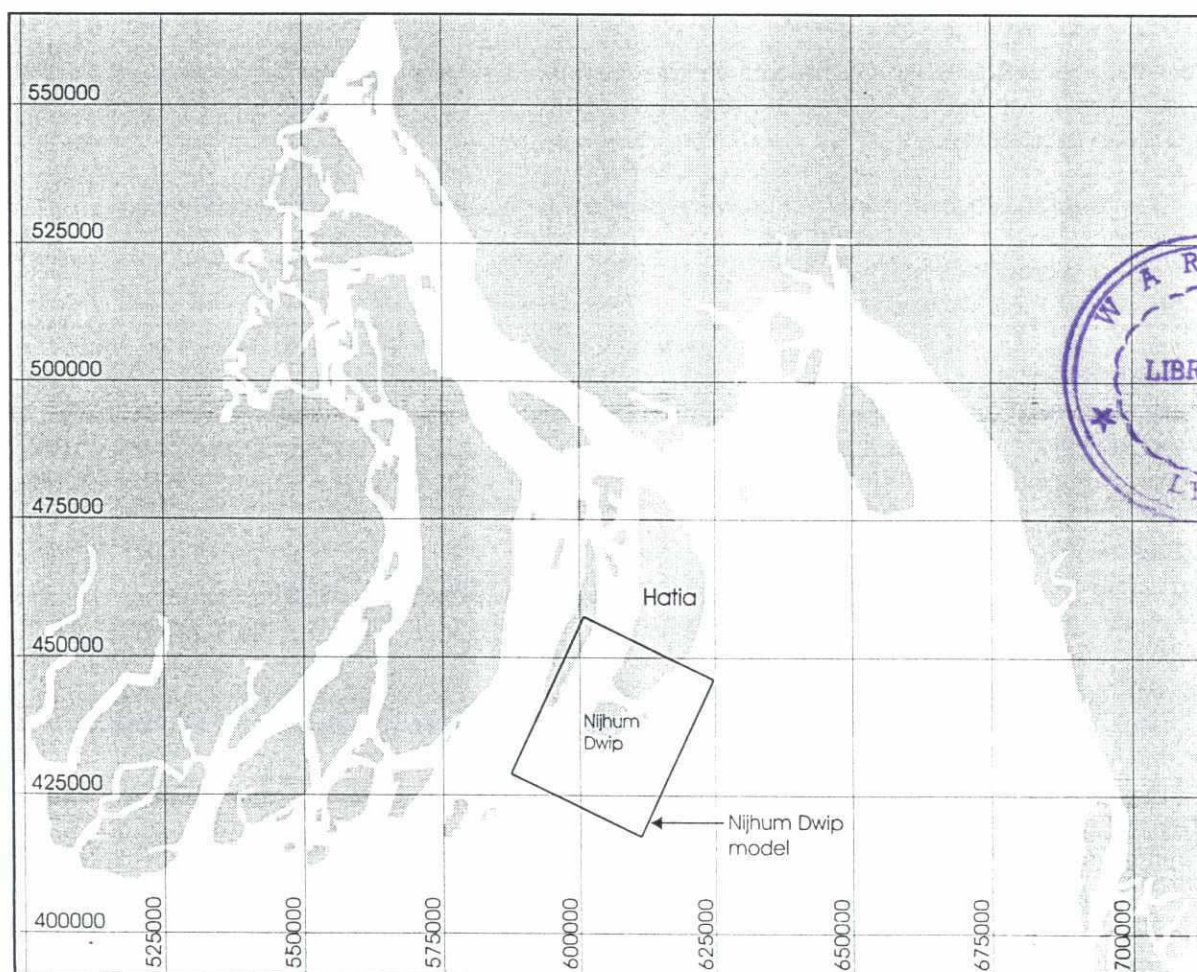
Table 3.1 Model grid definitions

	Meghna Estuary Model	Nijhum Dwip Local Model
Origo (longitude, latitude) (deg)	89.9710, 21.6329	90.8460, 21.9639
Origo (easting, northing) (m BTM)	497000, 392000	587337, 428873
Orientation (deg)	0.0	25.34
Grid extend x-dir., y-dir	0..360, 0..291	0..132, 0..157
Grid spacing (m)	600	200
Model area (km ²)	37948	841

The basic data for the bathymetry for this model was the same as was used for the 600 meter model bathymetry, and the interpolation and smoothing procedure were similar to the one applied for the 600 meter bathymetry.

Drawing 3.6 shows the 200 meter bathymetry of the Local Nijhum Dwip Model, while the model grid definition is given in table 3.1. Finally figure 3.1 shows the location of the model.

Figure 3.1 Location of Nijhum Dwip Local Model



4 Hydrodynamic Model Set-up

4.1 General

Based on the availability of measurements of water levels, wind and discharge (ADCP-data), the four simulation periods listed in table 4.1 were selected. Each simulation covers a period of 17 days allowing for warm-up of the model (1-2 days) plus a neap tide and a spring tide period.

Table 4.1 Simulation periods

Simulation name	Simulation period	
	start	end
Dry season 1996 (calibration period and base run)	03 Feb 96 00:00	20 Feb 96 00:00
Monsoon season 1996 (validation period)	23 Aug 96 00:00	09 Sep 96 00:00
Dry season 1997 (validation period)	01 Jan 97 00:00	18 Jan 97 00:00
Monsoon season 1997 (calibration period and base run)	08 Sep 97 00:00	25 Sep 97 00:00h

The simulation of the hydrodynamics in the Meghna Estuary was carried out using DHI's Hydrodynamic Model for 2D free-surface flows, MIKE 21 HD. A description of the model is included in appendix A.

For the model the following input data were applied in addition to the model bathymetry:

Basic model parameters:

- time step of 60 seconds

Initial conditions:

- water level of 0.46 m PWD corresponding to MSL
- cold start, i.e. all fluxes equal zero
- soft start of 6 hours

Boundary conditions:

- northern boundary: measured water levels (relative to PWD) at Chandpur
- southern boundary: tidal level from Kutubdia predicted from tidal constituents (from ATT [1]) as listed in table 4.2. Seasonal variations in the mean water level of -0.3 m (January), -0.4 m (February), 0.5 m (August), and 0.4 m (September) were applied. The predictions were finally related to PWD by adding 0.46 m. (See the section on model calibration for a final description of this boundary).

Driving forces:

- wind speed and direction measured at Hatia (from BMD) were applied for the whole model area (see drawings 4.1 to 4.4)
- inflow from rivers except for Lower Meghna during the two monsoon simulations: Feni River: 2500 m³/s and Karnafuli River: 600 m³/s. The flow from these two rivers was ignored during the dry season.

Calibration factors:

- bed resistance (see the model calibration below)
- wind friction factor: varying linearly from 0.0016 at 0 m/s to 0.0026 at 24 m/s
- momentum dispersion coefficients (eddy coefficients, E):
 $E = 0.015 \cdot \Delta x^2 / \Delta t$

where

Δx is the grid spacing

Δt is the time step

Table 4.2 Tidal constituents at Kutubdia Island (from ATT [1])

Tidal constituent	Amplitude (m)	Phase (deg) (UTC+6)
M2	1.16	337
S2	0.48	6
K1	0.18	349
O1	0.07	347
1/4 diurnal	0.017	241
1/6 diurnal	0.014	26

4.2 Hydrodynamic Model Calibration, 600 m Model

The model calibration was based on:

- comparison of measured water levels and predicted tidal levels with simulated water levels for the dry season period in 1996
- comparison of tidal constituents derived from the dry season period in 1996 with tidal constituents from tidal tables
- comparison of water levels, predicted tidal levels and measured discharges with simulated data for the monsoon season period in 1997.

Emphasis was put on the water level comparison for the dry season period in 1996.

The bed friction and the water level variation at the southern boundary were used as calibration factors.

The final bed friction coefficients (Manning Numbers) are shown in drawing 4.5. Manning Numbers of up to $100 \text{ m}^{1/3}/\text{s}$ were applied in those parts of the model describing flows through rivers and channels, while Manning Numbers of $60 \text{ m}^{1/3}/\text{s}$ were applied in the open parts of the model area.

The high Manning Numbers (i.e the low bed resistance) in the rivers and channels were necessary in order to compensate for the fact that a computational grid of 600 m is barely adequate to resolve the flow in the braided river channels. Especially flows running at an angle of 45° relative to the computational grid require a small grid size to be resolved without artificial loss of energy. However, using a smaller grid spacing was not possible as the CPU time requirements would thus become too high.

The final time shift of the tidal wave along the southern boundary together with the factor applied to the tidal level is listed in table 4.3.

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The time shift reflects the fact that the tidal wave does not travel in an exactly south to north direction but arrives first at the western part of the boundary. The factor on the water levels shows the difference in tidal elevation along the boundary.

Table 4.3 Time shift and factor on water level along southern model boundary

Grid point	Time shift (hours)	Factor on water levels
1	+1 1/25	0.90
50	+1 1/4	0.925
100	+1	0.95
150	+3/4	0.975
200	+1/2	1.0
250	+1/4	1.0
300	0	1.0
326	+1/4	1.0

4.3 Comparison of Measurements and Simulation Results, Dry Season 1996

Comparison between measured and calculated time series were made at 10 stations where measurements were available and 8 stations where predicted tidal elevations (from ATT [1].) were available. Results are shown in drawings 4.6 through 4.21. The stations are shown in figure 4.1 while their BTM and model coordinates are listed in table 4.4.

An evaluation of each individual station is given in table 4.5.

In addition to standard chart datum (CD) to PWD corrections it has been found necessary to apply extra corrections to the water level measurements and tidal predictions in order to achieve the fit shown. These extra corrections together with the standard corrections are listed in table 4.6.

Table 4.4 BTM and model coordinates of recording stations and tidal prediction stations

Station	BTM coordinates (m)		Model coordinates		Depth in model (m PWD)
	Easting	Northing	J	K	
Chandpur	566690	567978	114	291	-3.0
Char Chenga	610691	458354	188	111	-8.9
Chittal Khali	589871	508155	155	189	-2.9
Dasmunia	557041	458774	100	110	-11.2
Daulatkhan	573636	502898	128	185	-3.9
Dhulasar	522957	415600	43	39	-2.0
Dhulia	555110	494762	98	172	-7.6
Hatia Bar	597713	486428	168	157	-6.8
Khal No. 18	685510	457713	316	111	-3.6
Khepupara	522935	431061	43	65	-4.0
Kochopia	568946	434527	121	66	-1.2
Kutubdia Island	689408	419003	322	45	-6.3
Norman's Point	637276	454036	317	103	-5.4
Rabnabad Channel	537828	440055	68	80	-3.5

Station	BTM coordinates (m)		Model coordinates		Depth in model (m PWD)
	Easting	Northing	J	K	
Ramdaspur (Ilsa Ghat)	567662	522585	118	216	-3.5
Sandwip	649194	482135	254	150	-9.0
MES 1	540014	412723	72	35	-4.1
MES 2	591975	426766	158	58	-9.4
MES 4	664455	500204	279	180	-9.0
MES 5	637347	513778	234	203	-5.7
MES 6	592000	500000	158	180	-5.3
MES SE	694105	413510	329	36	-5.1

Figure 4.1 Locations used for comparison of measured/predicted water levels with simulated water levels.

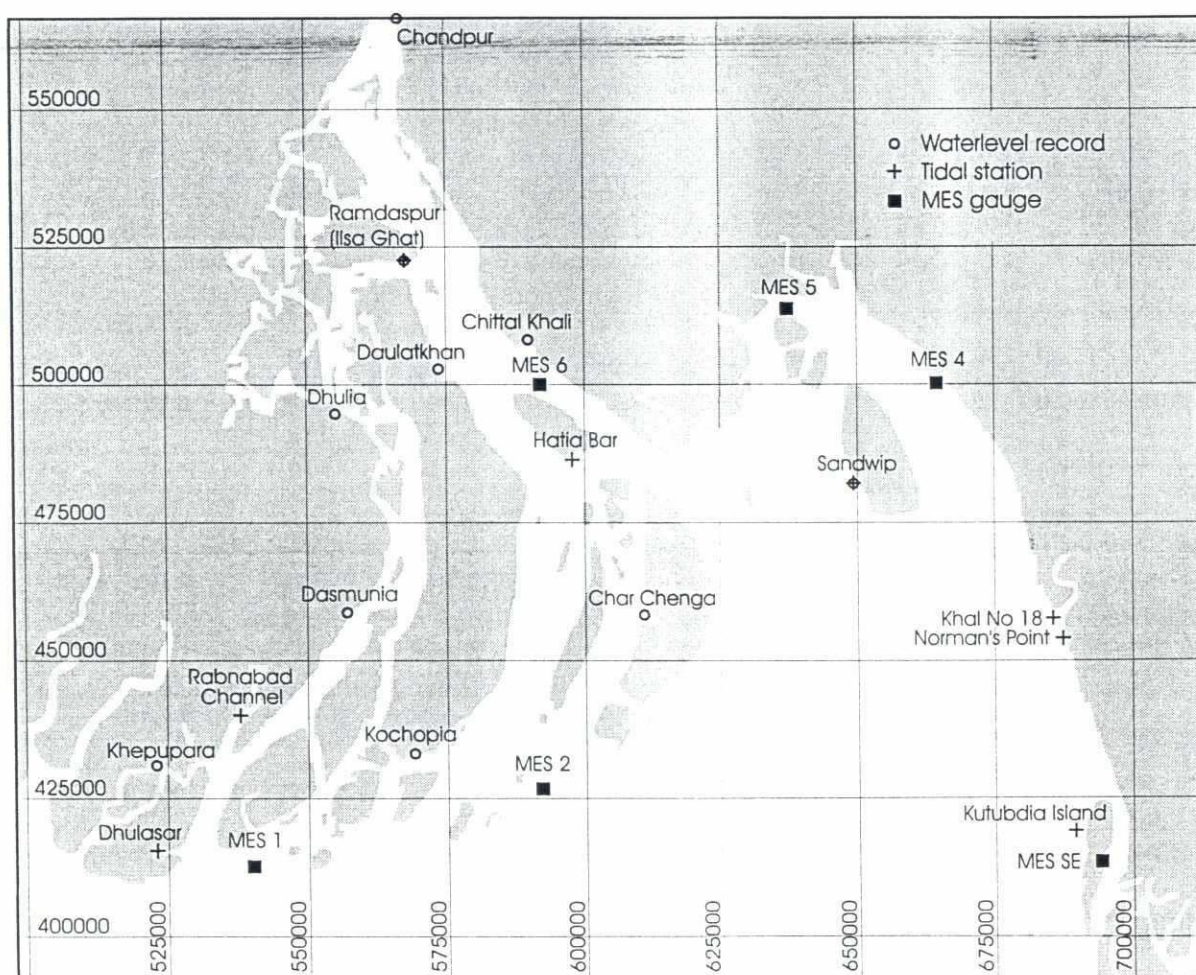


Table 4.5 Comparison of measured/predicted water levels and simulated water levels for dry season 1996 period.

Station	Measurement (M) and/or tidal prediction (TP)	Evaluation
Chandpur	M	This is the prescribed northern boundary. Therefore a perfect fit is seen.
Char Chenga	M	A good fit.
Chittal Khali	M	A good fit.
Dasmunia	M	A good fit.
Daulatkhan	M	A good fit.
Dhulasar	TP	The amplitude of the simulation results are a little higher than the tidal prediction.
Dhulia	M	Although the amplitude of the simulation results are smaller than the measured amplitudes the fit is considered good.
Hatia Bar	TP	The simulated amplitudes are smaller than the predicted ones. These however are based on tidal constants which are most likely computed when the flow in this changing and dynamic area was different.
Khal No. 18	TP	A good fit.
Khepupara	M	Khepupara is up a small river where a 2-D model is not very accurate. Most likely this explains the phase difference between simulated and predicted water levels.
Kochopia	M	A minor shift in mean level and in phase is found. Otherwise a good fit.
Kutubdia Island	TP	A very good fit as this station is applied at the nearby southern model boundary.
Norman's Point	TP	A good fit.
Rabnabad Channel	TP	A good fit.
Ramdaspur (Ilsa Ghat)	M & TP	The amplitude of the simulation results is considerable smaller than the measurements but fit the tidal prediction reasonable well. (It should be noted that the simulation results in this part of the model are very sensitive to changes in the depth of the Lower Meghna.)
Sandwip	M & TP	A good fit.

Table 4.6 Water level corrections for measurements (meas) and tidal stations (tide)

Station	Meas*	ATT tide station no.	Seasonal corr. on tide	MSL to PWD corr. for tide	Extra corr. on tide	CD to PWD corr. on meas.	Extra corr. on meas.
Chandpur	x					0.25	
Char Chenga	x					-1.18	-0.22
Chittal Khali	x					-1.35	
Dasmunia	x					-0.55	
Daulatkhan	x					0.04	

Station	Meas*	ATT tide station no.	Seasonal corr. on tide	MSL to PWD corr. for tide	Extra corr. on tide	CD to PWD corr. on meas.	Extra corr. on meas.
Dhulasar		4502	**	0.46	0.18		
Dhulia	x					-0.66	0.27
Hatia Bar		4506	**	0.46	0.53		
Khal No. 18		4511	**	0.46	0.10		
Khepupara	x					-1.96	0.18
Kochopia	(x)					-1.60	
Kutubdia Island		4514	**	0.46	0.06		
Norman's Point		4510	**	0.46	0.09		
Rabnabad Channel		4503	**	0.46	0.28		
Ramdaspur (Ilsa Ghat)	x	4507a	**	0.46	1.02	-0.66	
Sandwip	x	4507	**	0.46	0.07	-1.71	-0.85
MES 1	(x)						-0.76
MES 2	(x)						-0.75
MES 4	(x)						-0.95
MES 5	(x)						-1.26
MES 6	(x)						-0.40
MES SE	(x)						-0.45

- * (x): Measurements only available for one of the four calibration and validation periods, ie the dry season 1997 period.
- ** Seasonal variations for the four calibration and validation periods are given in table 4.7.

Table 4.7 Tidal seasonal variations (from ATT [1])

Station	ATT tide station no.	Dry season period 1996	Monsoon season period 1996	Dry season period 1997	Monsoon season period 1997
Dhulasar	4502	-0.40	0.45	-0.30	0.45
Hatia Bar	4506	-0.40	0.45	-0.30	0.45
Khal No. 18	4511	-0.40	0.45	-0.30	0.45
Kutubdia Island	4514	-0.40	0.45	-0.30	0.45
Norman's Point	4510	-0.40	0.45	-0.30	0.45
Rabnabad Channel	4503	-0.40	0.45	-0.30	0.45
Ramdaspur (Ilsa Ghat)	4507a	-0.70	0.95	-0.60	0.95
Sandwip	4507	-0.40	0.45	-0.30	0.45

A tidal analysis of the simulation has been carried out in order to make a comparison of tidal constituents from [1] with tidal constituents from the model simulation. It should be noted that the length of the simulation period (16 days) is not sufficient to extract important tidal constituents like K_2 , as the magnitude of the tidal constants from the model simulations are influenced by non-resolved constituents. Furthermore wind is included in the simulation which may also influence the magnitude of the constants.

Co-tidal charts showing amplitudes and phases for the four main tidal constituents (M_2 , S_2 , O_1 and K_1) are shown in drawings 4.22 through 4.29. Furthermore tables 4.8a and b list a comparison between tidal constituents from [1] and from the tidal analysis of the simulation, while table 4.8c lists the shallow water corrections also included in the ATT. Generally a good agreement is found keeping in mind that the simulation was not intended for tidal analysis but for comparison on a time series basis. If tidal constituents are required for the study area a longer tide-only simulation should be carried out and a tidal analysis performed

Table 4.8a Comparison of semi-diurnal tidal constituents from ATT [1]. and the dry season 1996 period simulation

Station	M ₂ amplitude (m)		M ₂ phase (deg)		S ₂ amplitude (m)		S ₂ phase (deg)	
	ATT	model	ATT	model	ATT	model	ATT	model
Dhulasar	0.73	0.92	317	312	0.35	0.42	358	6
Hatia Bar	1.19	0.99	69	62	0.47	0.36	111	119
Khal No. 18	1.63	1.53	15	5	0.53	0.64	55	62
Kutubdia Island	1.16	1.31	337	335	0.48	0.58	6	27
Norman's Point	1.36	1.48	359	3	0.54	0.62	30	59
Rabnabad Channel	0.75	0.77	336	348	0.29	0.33	27	43
Ramdaspur (Ilsa Ghat)	0.67	0.57	136	118	0.67	0.19	179	174
Sandwip	1.84	1.79	33	36	0.65	0.74	81	97

Table 4.8b Comparison of diurnal tidal constituents from [1]. and the dry season 1996 period simulation

Station	K ₁ amplitude (m)		K ₁ phase (deg)		O ₁ amplitude (m)		O ₁ phase (deg)	
	ATT	model	ATT	model	ATT	model	ATT	model
Dhulasar	0.13	0.14	9	16	0.04	0.07	355	339
Hatia Bar	0.12	0.12	46	62	0.07	0.08	12	13
Khal No. 18	0.18	0.18	12	30	0.09	0.09	2	353
Kutubdia Island	0.18	0.18	349	18	0.07	0.08	347	346
Norman's Point	0.18	0.18	351	30	0.06	0.09	354	352
Rabnabad Channel	0.16	0.12	25	35	0.05	0.07	10	351
Ramdaspur (Ilsa Ghat)	0.11	0.08	82	104	0.07	0.06	57	49
Sandwip	0.15	0.18	25	44	0.09	0.09	1	4

Table 4.8c Shallow water corrections included in ATT [1]

Station	1/4 diurnal		1/6 diurnal	
	Amplitude (m)	Phase (deg)	Amplitude (m)	Phase (deg)
Dhulasar	0.095	227		
Hatia Bar	0.097	278		
Khal No. 18	0.026	249	0.007	59
Kutubdia Island	0.017	241	0.014	26
Norman's Point	0.045	240		
Rabnabad Channel	0.135	250	0.051	106
Ramdaspur (Ilsa Ghat)	0.279	280	0.080	165
Sandwip	0.041	289	0.011	67

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Based on the comparisons shown and discussed above the model calibration is considered satisfactory.

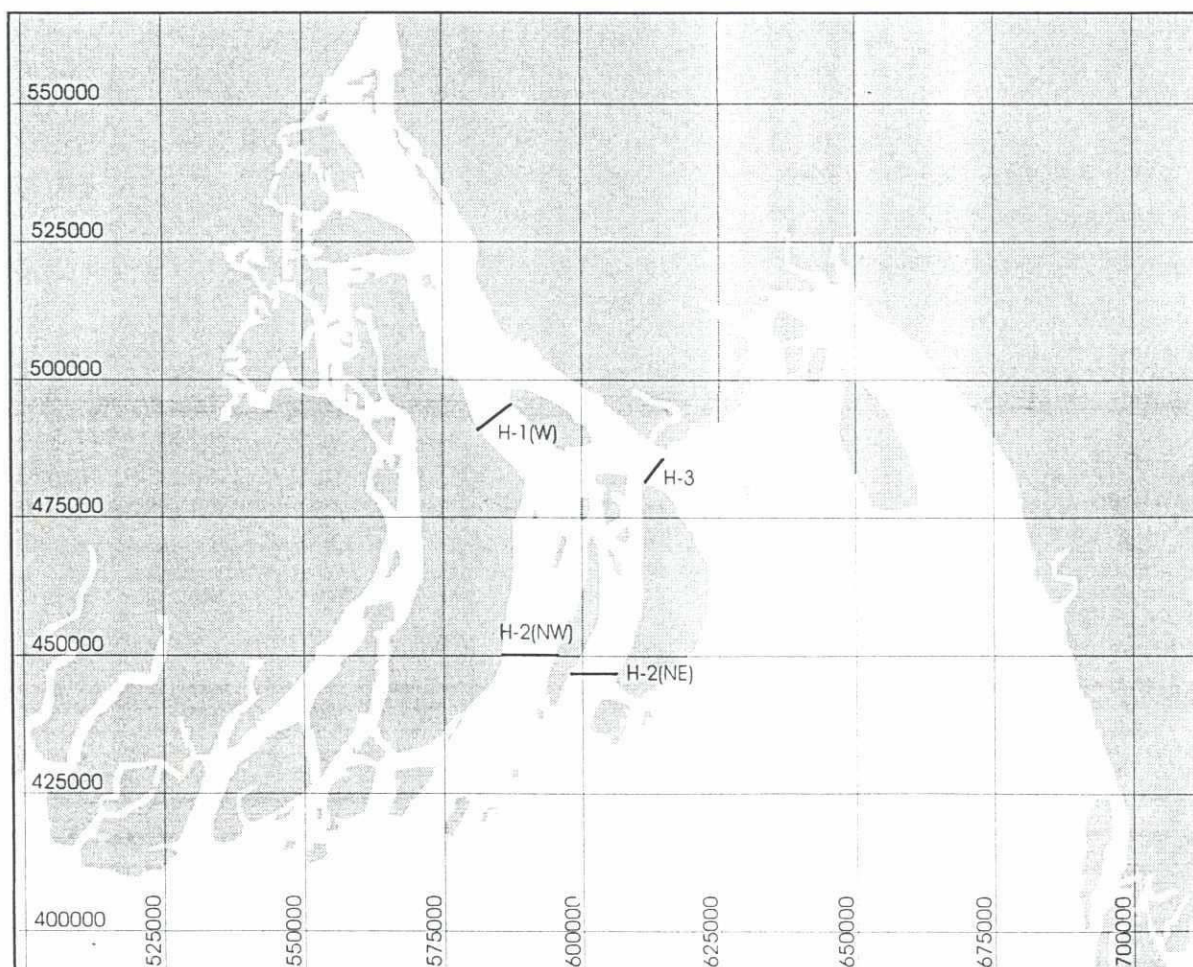
4.4 Comparison of Measurements and Simulation Results, Monsoon Season 1997

At 9 stations, water level measurements were available and at 8 stations, predicted tidal elevations (from ATT [1].) were available. For these stations comparisons with simulated water levels are shown in drawings 4.30 through 4.44. The stations are shown in figure 4.1 while their BTM and model coordinates are listed in table 4.4.

Also, comparisons of discharges have been made. These are shown in drawings 4.45 to 4.50. The cross sections where the ADCP measurements are made are shown in figure 4.2. Generally the measured/predicted water levels and the simulated water levels compare well although not as good as for the dry season 1996 period, while the discharge measurements and the simulated discharge compare well.

In all the calibration is considered to be satisfactory.

Figure 4.2 *Locations of cross sections with ADCP measurements used for comparison with simulated discharges*



4.5 Hydrodynamic Model Validation

For validation a dry season period in 1997 and a monsoon period in 1996 (see table 4.1) were simulated using the calibrated model.

Comparisons of time series of measured/predicted and simulated water levels for the two simulations are shown in drawings 4.51 through 4.88. The stations are shown in figure 4.1 while their BTM and model coordinates are listed in table 4.4.

For both periods, the comparison is satisfactory, although the concordance is better for the dry season period than for the monsoon season period as it was the case for the model calibration.

4.6 Nijhum Dwip Local Hydrodynamic Model

No measurements were available for a calibration or validation of the Nijhum Dwip Local Model. Therefore the same model parameters were used for this model as for the surrounding 600 meter model.

A local model simulation was carried out covering 4 tidal periods during spring tide of the dry season 1996 period: 06 February 1996 00:00 to 8 February 1996 01:30. The boundary conditions were taken from the surrounding 600 meter model.

The simulation results are discussed in section 5.3.

5 Hydrodynamic Baseline Simulations

5.1 Dry Season 1996

As reference simulation (or baseline simulation) for the dry season the calibration simulation of 1996 was selected.

In order to be able to assess the impact of various interventions on the flow patterns in the estuary the following parameters were extracted for each grid point in the model:

- maximum velocities during spring tide
- maximum velocities during neap tide
- net flow during spring tide
- net flow during neap tide

These parameters are shown in drawings 5.1 to 5.4.

5.2 Monsoon Season 1997

As base line simulation for the monsoon season the calibration simulation of 1997 was selected.

The base line conditions for the monsoon season were extracted and presented similar to the dry season base line simulation.

These maximum velocities and net flows for the monsoon season base line simulation are shown in drawings 5.5 to 5.8.

5.3 Nijhum Dwip Local Model, Dry Season 1996

For the Nijhum Dwip Local Model the base line simulation covered four tidal cycles during spring tide, dry period 1996 as described under local model set-up.

From this simulation the following parameters were extracted:

- maximum velocities, spring tide (see drawing 5.9)
- net flow, spring tide (see drawing 5.10)



6 Hydrodynamic Simulations including Intervention Schemes

6.1 Dry Season 1996

Three different scenarios involving three different combinations of intervention schemes (see figure 6.1) were considered in hydrodynamic simulations of the dry season period in 1996:

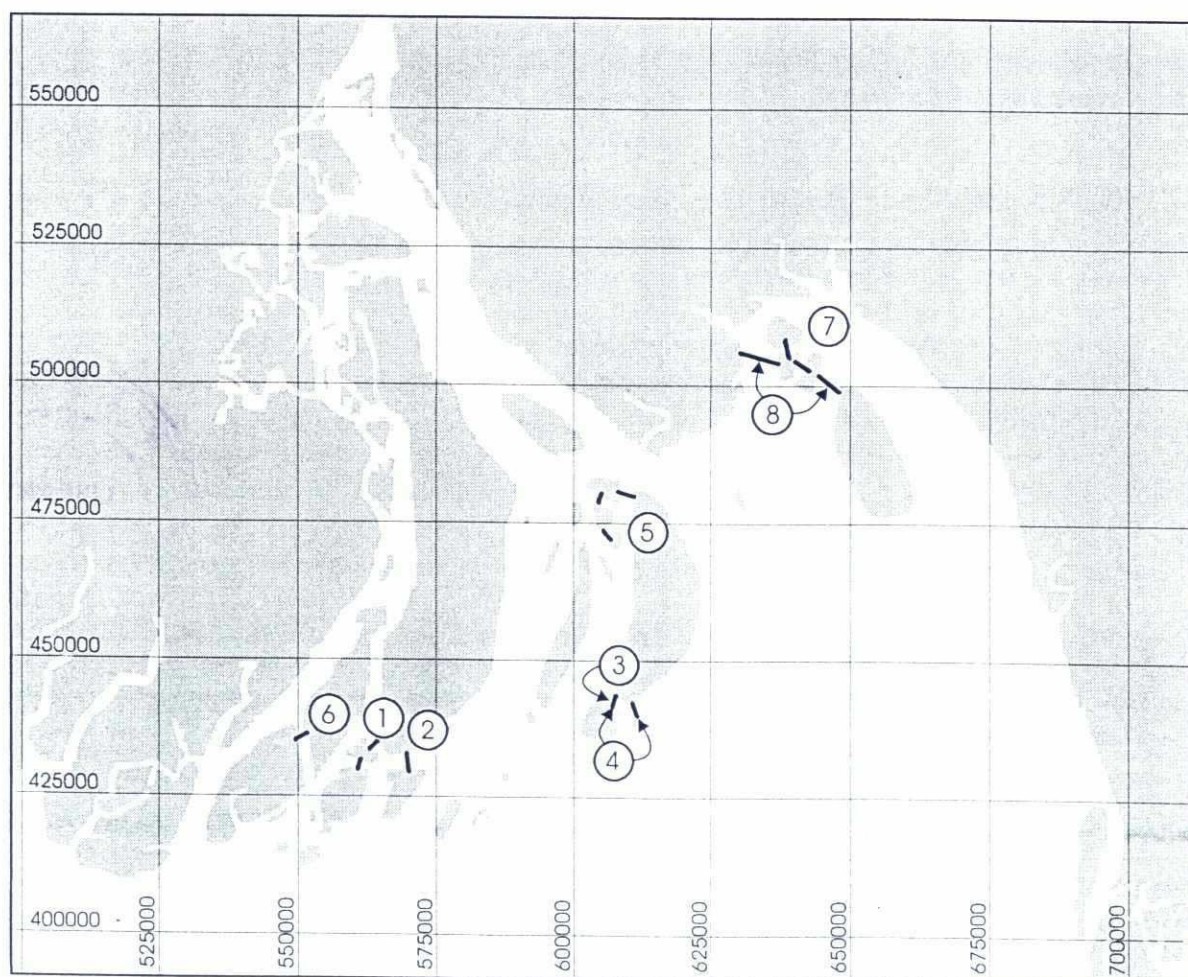
- including interventions no. 1 and 3
- including all interventions except no. 8
- including all eight interventions

For each of these three scenarios the following parameters were extracted from the simulations for comparison with the base line simulation:

- maximum velocities during spring tide
- maximum velocities during neap tide
- net flow during spring tide
- net flow during neap tide

These parameters are shown in drawings 6.1 through 6.12.

Figure 6.1 Intervention schemes considered in the numerical modelling



6.2 Monsoon Season 1997

Simulations were made for the monsoon season 1997 similar to those carried out for the dry season 1996, and maximum velocities and net flows were extracted (see drawings 6.13 through 6.24).

6.3 Nijhum Dwip Local Model, Dry Season 1996

For the local model two different scenarios (see figure 6.1) were considered in hydrodynamic simulations of four tidal periods (spring tide) during the dry season period in 1996:

- including intervention no. 3
- including interventions no. 3 and 4

For each of these scenarios the following parameters were extracted from the simulations for comparison with the baseline simulation:

- maximum velocities during spring tide
- net flow during spring tide

These parameters are shown in drawings 6.25 through 6.28.

7 Salinity Modelling

7.1 General

The salinity in the Meghna Estuary varies considerably from area to area and from season to season depending mainly on the outflow from the rivers and the tidal flow entering from the sea. During the monsoon season the large outflow from the rivers pushes the salt water well out into the Bay of Bengal, while the salt water during the dry season enters the estuary and the southernmost parts of the rivers emptying into the estuary.

The salinity is an important factor for many parts of the present study. Examples are fisheries, agriculture (especially salinity intrusion) and sedimentation rates.

In the present numerical study only the salinity variation during the dry season has been simulated as the salinity front during this season lies within the study area. If the salinity variation during the monsoon season is to be studied a much larger model area would be required.

7.2 Set-up of Salinity Model

The hydrodynamic model described in the previous chapters is a depth-integrated model assuming one-layer vertically homogeneous flow. In estuaries stratified two-layer flow occurs often with fresh water on top of salt water. In the Meghna Estuary the two layers are, however, well mixed most of the time (according to [2]), so the use of a one-layer model is therefore justified.

DHI's Advection-Dispersion Model, MIKE 21 AD, was applied for the same model area (and using the same model bathymetry) as the hydrodynamic model described in the previous chapters. MIKE 21 AD simulates the spreading of a dissolved or suspended substance in an aquatic environment under the influence of the fluid transport and associated natural dispersion processes. A more detailed description is given in Appendix B.

In addition to simulating the transport and spreading of salt and fresh water MIKE 21 AD also takes into account the density driven currents, i.e. the current generated by the difference in density of fresh water and saline water. The results of MIKE 21 AD is thus not only salinity concentration fields but also water levels and fluxes like MIKE 21 HD. By comparing the water levels from the two models the effect of the density differences can be quantified.

7.3 Salinity Model Calibration

Two sources of salinity data for calibrating the salinity model for a dry season period were available:

- LRP data [2] (0.5 m above sea bed and 0.5 m below surface)
- MES data (profiles)

As the LRP data covered the estuary more extensively than the MES data it was decided to base the salinity modelling on the LRP data by using these data as the initial salinity concentration within the estuary and at the boundary of the salinity model. The MES data were used for model calibration in combination with the LRP data. Drawing 7.1 shows the initial salinity concentrations based on the LRP measurements.

As calibration period for the dry season the period in February 1996 already applied for the hydrodynamic model calibration was selected.

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The calibration factors in MIKE 21 AD are dispersion coefficients in the x and y-direction, D_x and D_y , which describe the subgrid scale mixing. Suitable methods for determining these coefficients are subject to intense research but no final formulations have been found. A number of indicative formulations do however exist, and one of these reads:

$$D = K \cdot \Delta x^2 / \Delta t$$

where D is the dispersion coefficient in the x or y direction

K is a constant

Δx is the grid spacing

Δt is the time step

Using a value for K of 0.015 as was used for the eddy coefficient in the hydrodynamic simulations yields a first guess of 90 m²/s for the dispersion factor, which is applied both for D_x and D_y .

A salinity simulation using these dispersion factors does however give salinity concentrations, which are too small in the inner parts of the estuary when comparing both to LRP and MES data. The dispersion coefficient is therefore increased by a factor of 5 to 450 m²/s, which yields results comparing satisfactory to the measurements (see below). As only limited data are available for calibration of the salinity no further calibration seemed justified.

Drawing 7.2 show the variation of the salinity at different stations throughout the simulation. From this drawing it is concluded that the salinity variations have reached a stable level (taking into account the varying tidal conditions) around 13 February 1996. Minimum, mean and maximum salinities are therefore extracted for the last 14 tidal cycles of the simulation, i.e from 12 February 1996 18:30 to 20 February 1996 00:00. This period also covers the transition from neap to spring tide (see the hydrodynamic model calibration for February 1996).

Table 7.1 shows a comparison of MES measurements in different parts of the estuary (see figure 7.1) with extracted salinity statistics from the simulation. The two sets of data generally show a good agreement:

- *Around northern and eastern part of Hatia*
a very good agreement is found
- *Around northern half of Sandwip*
the simulation results vary between 13 ppt and 19 ppt, while most of the measurements are between 3 and 4 ppt. A salinity of 16 ppt has however also been measured close to a location where 3.4 ppt was measured only two days earlier, thus documenting a large salinity variation in time. By looking at the flow pattern during the measuring period an explanation for the variation and thus the difference between the simulation results and the measurements may be found.
- *South and east of Nijhum Dwip:*
Generally a very good agreement between measurements and simulation results is found. The only difference occurs in a location with a measured salinity of 4.5 and 8.5 ppt, where the maximum salinity simulated was 3.9 ppt.

- *Southwest corner of study and south of Char Montaz:*

The measurements in this area vary between 10 and 14 ppt, which is comparable to the simulation results. However in one location the measurement is smaller than the simulation result while in another one the measurement is larger than the simulation results. This discrepancy illustrates the large salinity variations in this part of the study area, variations which are also found in the simulation results. The comparison is thus considered to be satisfactory.

Table 7.1 Comparison of measured and simulated salinities during the dry season.

Area	Position		Measurements		Model simulation results		
	Easting	Northing	Date	Depth average salinity (ppt)	Min. salinity (ppt)	Mean salinity (ppt)	Max. salinity (ppt)
Around Northern and Eastern part of Hatia	610150	472736	29-jan-97	12.2	1.3	4.5	10.5
	610243	473018	02-feb-97	6.3	1.3	4.6	10.6
	609563	477570	03-feb-97	10.7	1.3	4.9	11.0
	611069	486729	26-feb-97	2.5	0.2	2.6	8.9
	614263	480411	26-feb-97	3.0	0.4	5.3	12.2
Around Northern half of Sandwip	623242	454113	04-feb-97	12.3	11.3	12.8	13.9
	663610	501628	27-feb-97	3.2	15.3	17.5	19.0
	664128	499958	01-mar-97	16.4	15.7	17.7	19.2
	646987	486798	01-mar-97	3.4	14.4	15.4	16.4
	644780	493520	02-mar-97	3.4	12.9	14.9	16.7
South and East of Nijhum Dwip	647021	486864	03-mar-97	3.4	14.4	15.4	16.4
	599503	439430	22-jan-97	4.5	1.7	2.3	3.9
	600070	439411	26-feb-97	8.5	1.7	2.3	3.9
	604569	447173	24-jan-97	4.6	1.6	2.3	5.4
	591570	427291	25-jan-97	4.2	1.2	3.3	9.5
	604503	447114	25-jan-97	4.7	1.6	2.3	5.3
	609540	426473	25-jan-97	7.9	5.8	9.2	11.8
Southwest corner of study area and South of Char Montaz	611734	431077	27-jan-97	7.0	5.4	9.5	12.1
	603739	425163	28-jan-97	6.8	3.3	5.8	8.0
	536009	394292	26-mar-97	13.7	19.6	24.3	26.5
	530421	411814	28-mar-97	10.7	7.7	13.3	21.9
	526622	412950	29-mar-97	10.2	6.9	12.9	21.3
	537494	411913	30-mar-97	12.7	9.8	13.0	18.8
	552648	421998	28-mar-97	14.1	2.8	5.2	8.3
	565342	417901	27-mar-97	11.2	2.5	5.9	11.8

7.4 Salinity Model Simulations

Two salinity simulations as listed in table 7.2 have been carried out. In addition to the simulation carried out for calibration one simulation for the same period but including all intervention schemes has also been made. For each of these simulations the minimum, mean and maximum salinity have been extracted.

Furthermore the difference in mean water level caused by the inclusion of density differences in the hydrodynamic computations is shown in drawing 7.3. From this drawing it is seen that the mean water level in the estuary is increased by up to 10 cm by including this effect.

The variation of the salinity in the estuary during the simulation period is also shown as an animation on the Presentation CD-ROM prepared as part of the reporting. Looking at such an animation often gives a better explanation of the dynamic salinity variation in the Meghna Estuary than tables and drawings do. (Note for example the inflow of saline water North of Hatia.)

Figure 7.1 Location of measured salinities used for comparison with simulated salinities

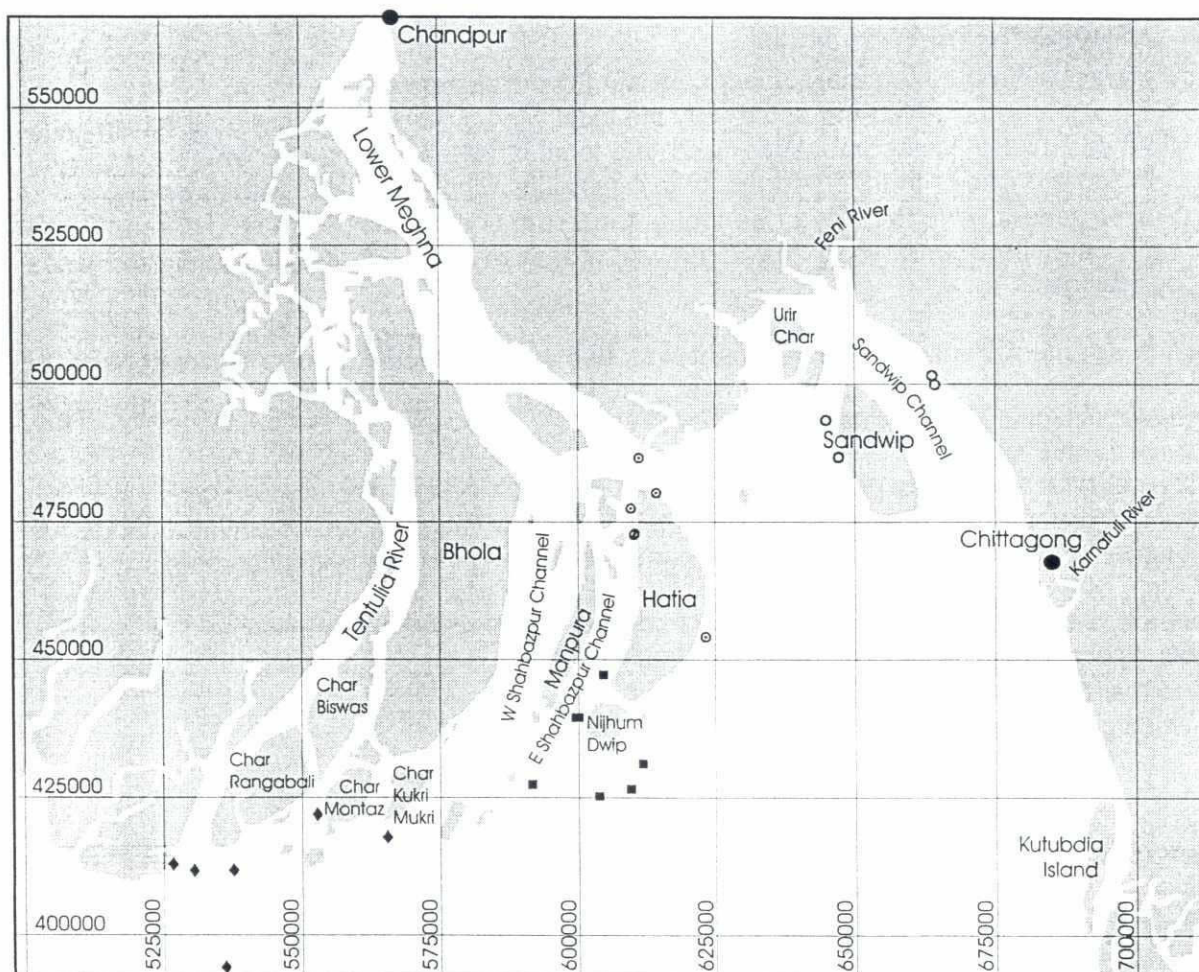


Table 7.2 Salinity model simulations

Intervention Schemes	Min., mean and max. salinity shown in drawings
Existing situation (no intervention schemes)	7.4, 7.5 and 7.6
Including all interventions	7.7, 7.8 and 7.9

8 Wind-Wave Modelling

8.1 General

The purpose of the wind-wave modelling was to determine the wind-wave fields for a number of normally occurring wave conditions within the study area. The simulated wind-wave fields were then subsequently applied in the sediment transport simulations.

8.2 Set-up of Wind-Wave Model

Wind-waves within the Meghna Estuary consist of two types of waves:

- Waves generated within the estuary by the local wind, which may either be the prevailing Northeast or Southwest monsoon wind, the local land/sea breeze, the winds associated with depressions or thunder storms, or in rare cases wind associated with a cyclone.
- Waves generated in the Bay of Bengal to the south of and outside the study area. These waves may be generated by the Southwest monsoon or by depressions or in rare cases by cyclones.

For the sediment transport simulations it was decided to consider waves corresponding to the Southwest monsoon only. On this basis, the model area and the software for making the wind-wave calculations were selected.

DHI's Nearshore Spectral Wind-Wave Model, MIKE 21 NSW, was chosen as this model computes the stationary wave field within a given area for given offshore wave conditions (i.e. wave conditions entering the area from the South) and for given wind conditions.

Generally MIKE 21 NSW describes the growth and decay of short-period waves in nearshore areas. The model takes into account the effects of

- refraction and shoaling due to varying depth
- wind generation
- energy dissipation due to bottom friction and wave breaking.

A short description of MIKE 21 NSW is given in Appendix C.

As only southwest monsoon winds were considered, the wave model area was chosen to coincide with the model area used for the hydrodynamic simulations. If for example waves generated by cyclonic winds were to be computed, a non-stationary wind-wave model covering the whole of the northern part of the Bay of Bengal should have been applied.

Due to the computational scheme applied in MIKE 21 NSW, the grid spacing in the main wave direction should be only 1/4 of the grid spacing perpendicular to the main wave direction. Therefore a grid spacing of 150 m x 600 m was applied. The model bathymetry is shown in drawing 8.1. The depth corresponds to mean sea level computed during the monsoon season simulation for 1997 by the hydrodynamic model.

As no wave measurements were available, no calibration was carried out. The wave fields computed by an uncalibrated model do however still give a good description of the wave conditions in the area. In the calculations the following parameters were applied:

- wave breaking (using Battjes and Janssens formulation): $\gamma_1=1.0$, $\gamma_2=0.8$ and $\alpha=2.0$
- bottom friction: Nikuradse roughness parameter, k_N of 0.0002 m

Significant wave heights and wave periods required at the southern model boundary (i.e. the boundary facing the Bay of Bengal) were calculated using the revised Shore Protection

Manual (SPM) formulae given in [3]. A fetch length of 500 km, a 10 m wind speed of 8 m/s and the actual water depth along the boundary were applied.

8.3 Wind-Wave Model Simulations

For use in the sediment transport simulations the wind-wave model simulations listed in table 8.1 were carried out.

Table 8.1 *Wind-wave model simulations*

Wind conditions	Wave conditions shown in drawings
8 m/s from South-Southeast	8.2
8 m/s from South-Southwest	8.3

9 Sediment Transport Modelling

9.1 General

Making a numerical sediment transport model of the Meghna Estuary is a large complicated task requiring extensive model calibration. Within the present study period, only a limited effort was envisaged and carried out. The results are thus indicative only and can be considered as a basis for further studies.

9.2 Set-up of Sediment Transport Model

The type of sediment transport model required for a specific area depends on the grain size of the sediment as well as on the governing transport processes. For the Meghna Estuary the sediment can be considered as largely non-cohesive, while the main governing sediment transport mechanisms are the tidal flow and the outflow from the rivers. The effect of the wind-waves on the sediment transport rates is also of importance and should be considered.

On this background DHI's Sand Transport Module of MIKE 21, MIKE 21 ST, was chosen. This model calculates sediment transport rates on a rectangular grid covering the area of interest on the basis of

- hydrodynamic data obtained from MIKE 21 HD simulations,
- wave data obtained from a simulation using MIKE 21 NSW (or another of the MIKE 21 wave models)
- characteristics of the bed material (like grain size and distribution)

When computing the sediment transport rates, MIKE 21 ST takes into account the following effects:

- pure current flow or combined wave-current flow
- arbitrary wave propagation angle relative to the flow direction
- breaking/non-breaking waves
- graded/uniform bed material
- plane/ripple-covered bed

For the present study the formulation of the total load (suspended load plus bed load) by Bijker was applied for pure current flow. For more details on MIKE 21 ST see appendix D.

The following bed material characteristics were applied in the simulations:

- $d_{50} = 0.099$ mm, grading = 1.44, porosity = 0.4 and relative density = 2.57

Furthermore the following model parameters were applied:

- $B = 2.5$ (the transport coefficient) and water temperature = 27 °C

The area covered by the sediment transport model corresponded to the area covered by the hydrodynamic model and the wind-wave model.

9.3 Sediment Transport Model Simulations

For use in the assessment of the morphological development of the Meghna Estuary a number of characteristic combinations of tidal regime, river outflow (i.e. season) and wave conditions were selected and simulated. Each simulation covers one tidal cycle (i.e. 12.5 hours) of the hydrodynamic base run simulations as listed in table 9.1, while all simulations are listed in table 9.2 together with the number of the drawing depicting the results of the simulations. The drawings show the sediment transport rates.

The wave conditions applied are described in the previous chapter.

Table 9.1 Tidal periods applied in sediment transport simulations

Season	Tidal regime	Start of tidal period	End of tidal period
Dry season 1996	Spring tide	07 Feb 1996 02:00	07 Feb 1996 14:30
Dry season 1996	Neap tide	13 Feb 1996 20:00	14 Feb 1996 08:30
Monsoon season 1997	Spring tide	18 Sep 1997 01:00	18 Sep 1997 13:30
Monsoon season 1997	Neap tide	11 Sep 1997 07:30	11 Sep 1997 20:00

Table 9.2 Sediment transport simulations

Season	Tidal regime	Wave conditions	Results shown in drawings
Dry season 1996	Spring tide	No waves	9.1
Dry season 1996	Neap tide	No waves	9.2
Monsoon season 1997	Spring tide	Waves from SSE	9.3
Monsoon season 1997	Spring tide	Waves from SSW	9.4
Monsoon season 1997	Spring tide	No waves	9.5
Monsoon season 1997	Neap tide	Waves from SSE	9.6
Monsoon season 1997	Neap tide	Waves from SSW	9.7
Monsoon season 1997	Neap tide	No waves	9.8

Please note that the sediment transport rates should only be applied qualitatively.

10 Recommendations for Future Model Development

10.1 General

The numerical modelling of the Meghna Estuary has been an on-going learning process throughout the study period. One example is the realisation during the early phases of the study that a bathymetric survey of the entire study area was required in order to be able to describe the existing hydrodynamic conditions properly.

During the later stages of the numerical modelling a number of other possible improvements to the basic modelling data and modelling procedures have been identified. It has not been possible to include all of these in the present study and they are therefore included in this section as recommendation for future modelling work.

On-the-job supervision of SWMC staff by the DHI numerical modelling specialist was carried out throughout the project period. However, in order to properly transfer the modelling techniques it is recommended that formal training in connection with further development and application of the models are conducted.

10.2 Model Bathymetries

Although a bathymetric survey has been carried out for the major part of the study area some parts have not yet been covered. These include especially shallow areas like the shallow area to the West of Sandwip. The shallow areas are important from a hydrodynamic point of view because of their blocking effect on the flow. For the model simulations described in the present report the elevations of these shallow un-surveyed areas are only known with an accuracy of a couple of meters, which makes the degree of "blocking effect" computed by the models uncertain. Therefore it is recommended that the shallow areas within the study area be surveyed and included in the models.

Coastlines and riverbanks are changing rapidly in certain areas of the estuary. The coastlines in the present models are based on satellite mapping in February 1996 supplemented with a few data around Nijhum Dwip from November 1997. In connection with future use of the models, it is recommended that coastlines (and thus riverbanks) are updated regularly.

Due to erosion and accretion, the depths in the estuary are also changing. Regular updates of the model bathymetry are therefore required in order to keep the model up to date.

Interpolation from bathymetric survey lines to a square model grid in rivers and areas with channels in the sea bed is not well performed by standard interpolation routines. Often the depth in between survey lines will be underestimated leading to an unrealistic small flow in the area. During the set-up of the bathymetry this problem was identified but only tedious ad hoc solutions to the problem found. It is therefore recommended that alternative interpolation routines are checked and if necessary developed or acquired. In this way the bathymetric survey data will be better utilised.

10.3 Hydrodynamic Modelling

During the course of MES, water level measurements and ADCP measurements have been collected and utilised in the calibration of the hydrodynamic models. When the model bathymetry is updated with new survey data in the future, and if this update introduces

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significant changes in the bathymetry, a recalibration of the model with new water levels and new ADCP measurements is recommended.

If the hydrodynamic model is going to be used for modelling of cyclonic surges, a nested model approach as used in the Cyclone Shelter Preparatory Study [4] is required, because a larger area must be covered by the model.

10.4 Salinity Modelling

The salinity modelling carried out and described in the present report describes the salinity variations only during the dry season and only for one case with a known salinity distribution in the estuary. The reason is that the model applied only covers the estuary itself, while the area to the south of the model, which will effect the salinity variation within the estuary especially during the monsoon season but also during the dry season, is not included. Therefore it was only possible to do a simulation with known salinity along the southern model boundary.

If more general salinity simulations are to be made and especially if simulations during the monsoon season are to be carried out, it is recommended to adopt a nested grid approach like the one applied in the Cyclone Shelter Preparatory Study [4]. On the other hand, a demand for such simulations has not been identified.

It is also recommended to carry out more salinity measurements for the calibration of the salinity model. Only on the basis of measurements from the estuary will it be possible to improve the model calibration carried out and described in the present report. Such measurements cost next to nothing if combined with other survey activities.

10.5 Wind-Wave Modelling

The purpose of carrying out wave modelling in the present study was to support the sediment transport assessment. As the tidal flow and the river outflow are the governing forces, only minor emphasis was placed on the wave modelling. A limited number of wave measurements within the estuary to be used for future wave model calibration are however recommended.

It should also be mentioned that satellite measurements of wave heights are available. These do however presently only have an accuracy of 0.5 m or 10% (whichever is the higher) for the significant wave height, and they are only available for open sea areas. They could however be used for the open parts of the estuary as a supplement to the wave measurements.

10.6 Sediment Transport Modelling

The purpose of the sediment transport modelling carried out as part of the present study was to make an assessment of the sediment transport within the study area, while a detailed sediment transport study and a morphological study was outside the scope of the study. A sediment transport model of the Meghna Estuary is a valuable tool in for example impact assessments but it requires an extensive and detailed calibration effort with correspondingly extensive data requirements. As the estuary is a very dynamic area from a sedimentological/morphological point of view it is recommended to further develop the sediment transport model for the estuary, supported by a targeted field programme.

11 References

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- [2] Meghna Estuary Study, Technical Note MES-004, Salinity Distribution in the Estuary, January 1997.
- [3] Hurdle, D.P. and Stive, R. J. H., Revision of SPM 1984 Wave Hindcast Model to Avoid Inconsistencies in Engineering Applications, Coastal Engineering, Vol. 12, pp. 339-351, 1989.
- [4] European Commission, Cyclone Shelter Preparatory Study, Stage II: Feasibility Phase, Final Report, Supporting Volume 1, Mathematical Modelling of Cyclone-surge and related Flooding, Appendix C: Bay of Bengal Modelling Complex (MIKE 21), May 1998.

Appendices

Appendix A

MIKE 21 HD Hydrodynamic Module A Short Description



MIKE 21 HD - Release 1.1

HYDRODYNAMIC MODULE

A SHORT DESCRIPTION



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MIKE 21 HD - HYDRODYNAMIC MODULE

SHORT DESCRIPTION

Introduction

MIKE 21 is a comprehensive modelling system for 2-dimensional free surface flows where stratification can be neglected.

MIKE 21 HD is the basic module of the entire MIKE 21 system. It provides the hydrodynamic basis for the computations performed in most of the other modules, for example the Advection-Dispersion, Water Quality and Sediment Transport modules.

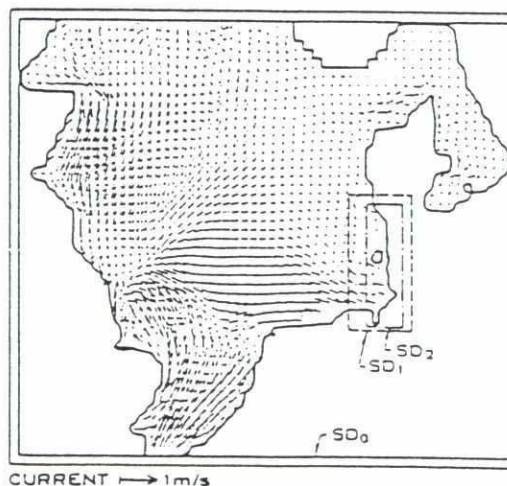
MIKE 21 HD simulates the water level variations and flows in response to a variety of forcing functions in lakes, estuaries, bays and coastal areas. The water levels and flows are resolved on a rectangular grid covering the area of interest when provided with the bathymetry, bed resistance coefficients, wind field, hydrographic boundary conditions, etc.

The system solves the equations of continuity and conservation of momentum using implicit finite difference methods.

Applications

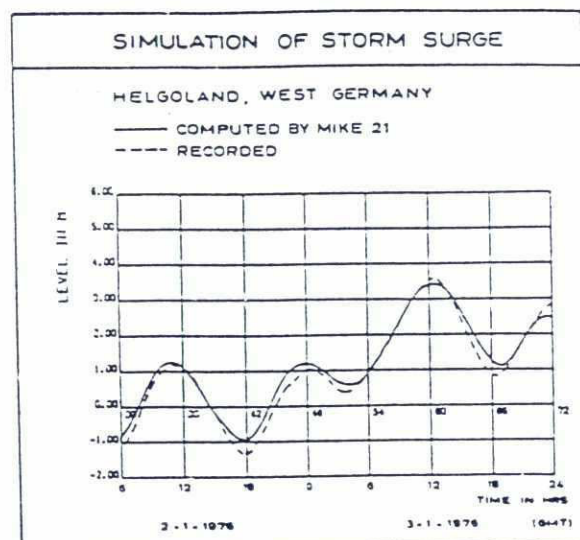
MIKE 21 HD is applicable to a wide range of hydraulic phenomena:

- Tidal exchange and currents

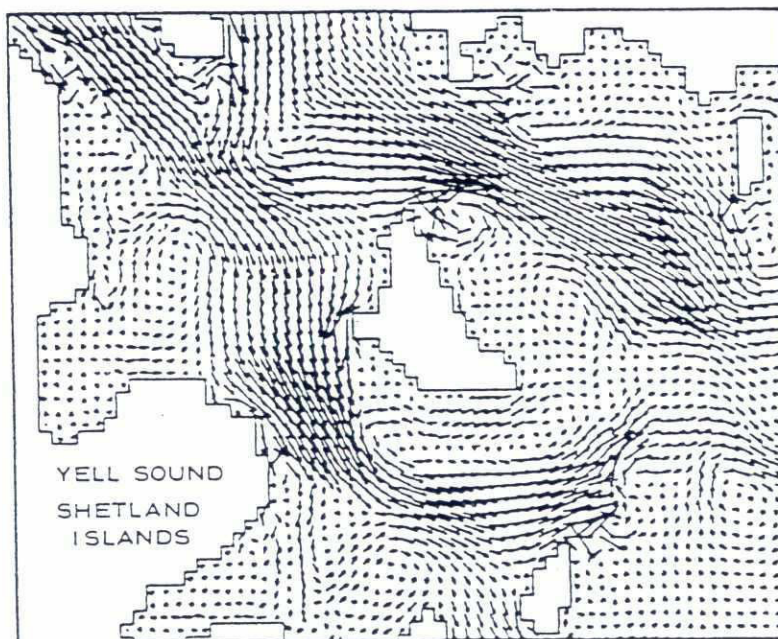


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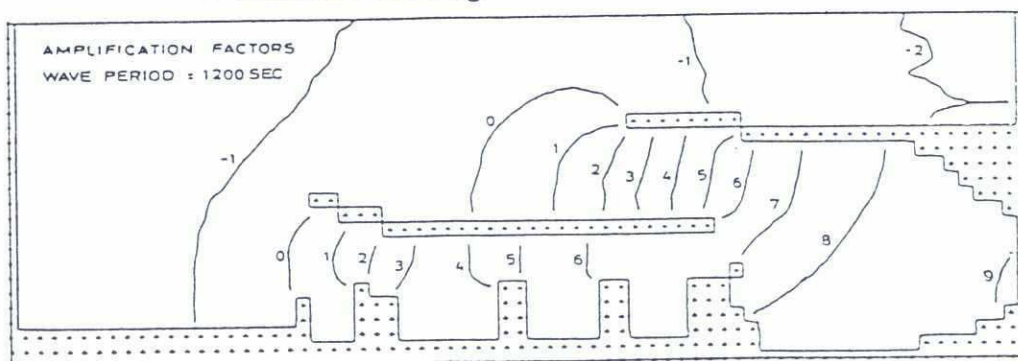
- Storm surge



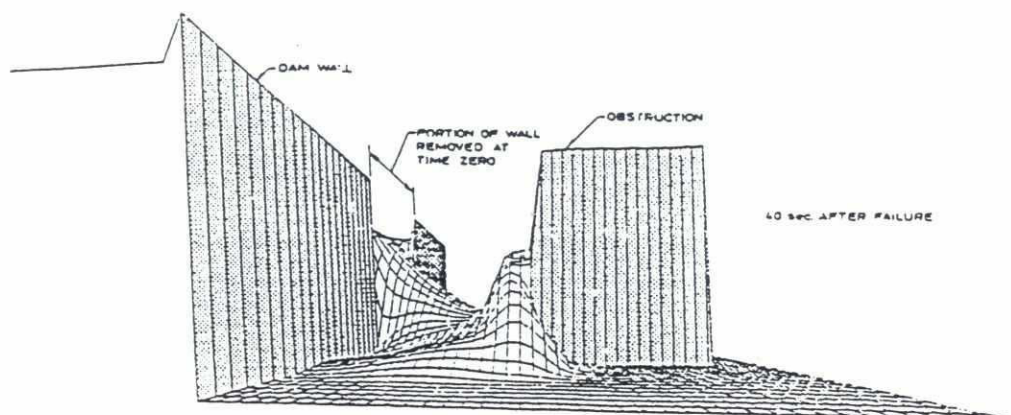
- Secondary circulations, eddies and vortices



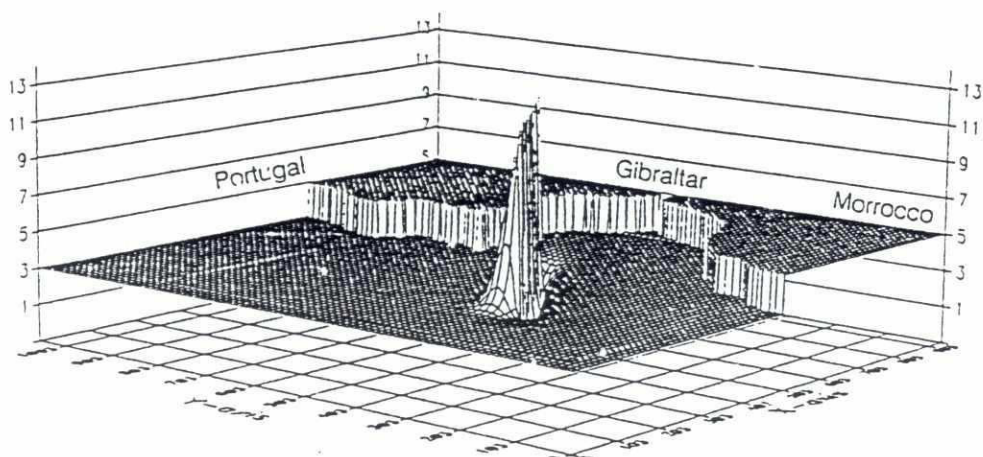
- Harbour seiching



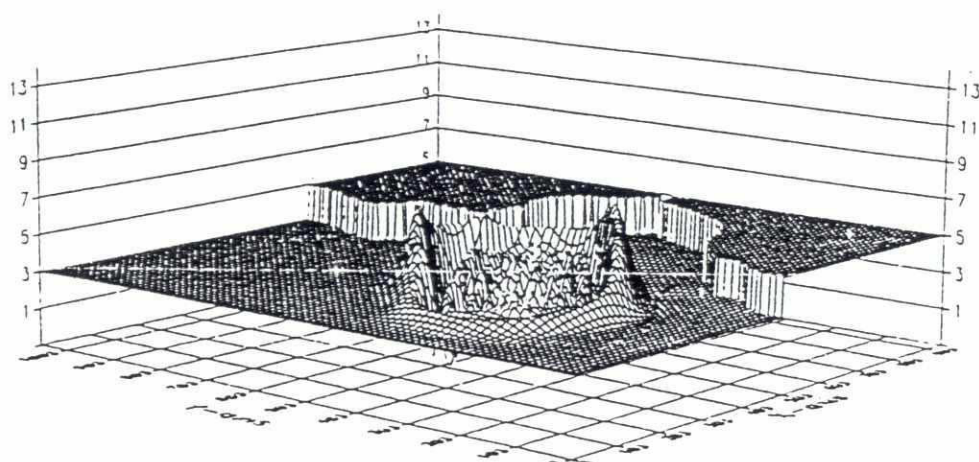
• Dam-break



• Tsunamis



SEA SURFACE IMMEDIATELY AFTER EARTHQUAKE



TSUNAMI AFTER 14 min.

Equations

The hydrodynamic module of MIKE 21 solves the vertically integrated equations of continuity and conservation of momentum in two horizontal dimensions. The following effects are included in the equations:

- convective and cross momentum
- wind shear stress at the surface
- barometric pressure gradients
- Coriolis forces
- momentum dispersion ('eddy')
- sources and sinks (both mass and impulse)
- evaporation.

Continuity

$$\frac{\partial \zeta}{\partial t} + \frac{\partial p}{\partial x} + \frac{\partial q}{\partial y} = s - e$$

x-Momentum

$$\frac{\partial p}{\partial t} + \frac{\partial}{\partial x} \left[\frac{p^2}{h} \right] + \frac{\partial}{\partial y} \left[\frac{p \cdot q}{h} \right] + gh \frac{\partial \zeta}{\partial x}$$

$$+ \frac{g}{C^2} \sqrt{\frac{p^2}{h^2} + \frac{q^2}{h^2}} \cdot \frac{p}{h} - fVV_x - \frac{h}{\rho_w} \cdot \frac{\partial p_a}{\partial x}$$

$$- \Omega q - \left[\frac{\partial}{\partial x} \left(E_x \cdot h \cdot \frac{\partial u}{\partial x} \right) + \frac{\partial}{\partial y} \left(E_y \cdot h \cdot \frac{\partial u}{\partial y} \right) \right] = S_{ix}$$

y-Momentum

$$\frac{\partial q}{\partial t} + \frac{\partial}{\partial y} \left[\frac{q^2}{h} \right] + \frac{\partial}{\partial x} \left[\frac{p \cdot q}{h} \right] + gh \frac{\partial \zeta}{\partial y}$$



$$+ \frac{g \sqrt{\frac{p^2}{h^2} + \frac{q^2}{h^2}} \cdot \frac{g}{h}}{C^2} - f V V_y - \frac{h}{\rho_w} \cdot \frac{\partial p_a}{\partial y}$$

$$+ \eta p - \left[\frac{\partial}{\partial x} \left(E_x \cdot h \cdot \frac{\partial v}{\partial x} \right) + \frac{\partial}{\partial y} \left(E_y \cdot h \cdot \frac{\partial v}{\partial y} \right) \right] = S_{iy}$$

Symbol List

$\zeta(x,y,t)$	- water surface level above datum (m)
$p(x,y,t)$	- flux density in the x-direction ($m^3/s/m$)
$q(x,y,t)$	- flux density in the y-direction ($m^3/s/m$)
$h(x,y,t)$	- water depth (m)
S	- source magnitude per unit horizontal area ($m^3/s/m^2$)
S_{ix}, S_{iy}	- source impulse in x- and y-directions ($m^3/s/m^2 \cdot m/s$)
e	- evaporation rate (m/s)
g	- gravity (m/s^2)
C	- Chezy resistance No. ($m^{1/2}/s$)
f	- wind friction factor
$V, V_x, V_y(x,y,t)$	- wind speed and components in x- and y-directions (m/s)
$p_a(x,y,t)$	- barometric pressure ($kg/m/s^2$)
ρ_w	- density of water (kg/m^3)
Ω	- Coriolis coefficient (latitude dependent) (s^{-1})
$E(x,y)$	- eddy or momentum dispersion coefficient (m^2/s)
x, y	- space coordinates (m)
t	- time (s)

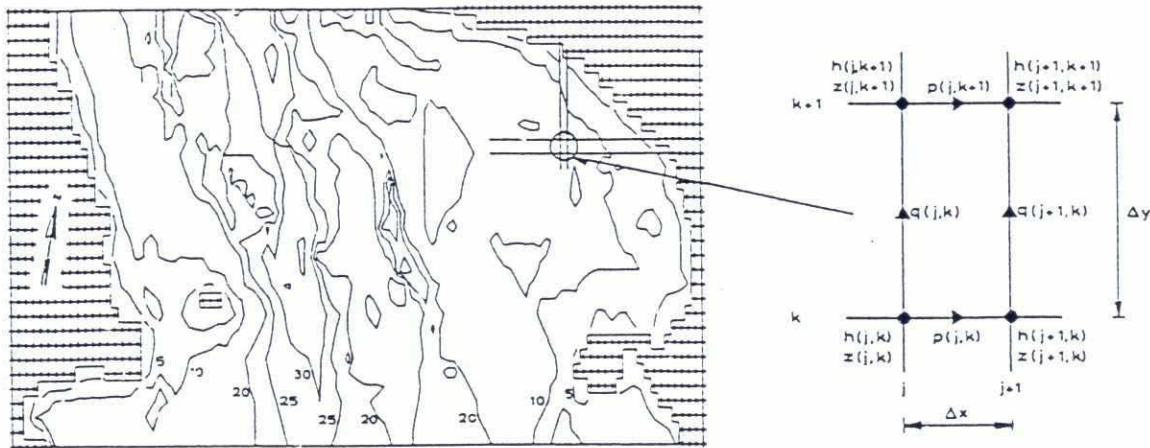
Calibration Factors

A MIKE 21 HD generated model has only three calibration factors, namely bed resistance C , wind friction factor f , and momentum dispersion coefficient E (normally called an eddy coefficient). Using these factors alone, calibration of a model is normally quite easy. In practice, the calibration of a model depends far more on the accuracy of the data, e.g. bathymetry, boundary data and wind speeds.

The bed resistance, C , and momentum dispersion coefficient, E , can both be specified as a function of space. Further, E can vary in time in accordance with a special formulation of Smagorinsky's theory for turbulence.

Solution Technique

The equations are solved by implicit finite difference techniques with the variables defined on a space-staggered rectangular grid as shown below.



A 'fractioned-step' technique combined with an Alternating Direction Implicit (ADI) algorithm is used in the solution to avoid the necessity for iteration. Second order accuracy is ensured through the centering in time and space of all derivatives and coefficients. The ADI algorithm implies that at each time step a solution is first made in the x-direction using the continuity and x-momentum equations followed by a similar solution in the y-direction.

As a simple example, the finite difference scheme for the time derivative of flux density is shown below.

$$\frac{\partial p}{\partial t} \approx \left[\frac{p^{n+1} - p^n}{\Delta t} \right] - \frac{\Delta t^2}{24} \cdot \frac{\partial^3 p}{\partial t^3}$$

truncation error

The truncation error is of second order, $O(\Delta t^2)$.

The application of the implicit finite difference scheme results in a tridiagonal system of equations for each grid line in the model. The solution is obtained by inverting the tridiagonal matrix using the Double Sweep algorithm, a very fast and accurate form of Gauss elimination.

The implicit scheme is used in MIKE 21 in such a way that stability problems do not occur provided, of course, that the input data is physically reasonable, so that the time step used in the computations is limited only by accuracy requirements.

Data Requirements

The necessary data can be divided into several groups as briefly described below.

Basic Model Parameters:

- Model grid size and extent
- Time step and length of simulation
- Type of output required and its frequency
- Latitude and its orientation

Bathymetry.

Calibration Factors:

- Bed resistance
- Momentum dispersion coefficients
- Wind friction factor

Initial Conditions:

- Water surface level
- Flux densities in x- and y-directions

Boundary Conditions:

- Water levels or flow magnitude
- Flow direction

Other Driving Forces:

- Wind speed and direction
- Source/sink discharge magnitude and speed.

Pre- and Post-processing Software

The MIKE 21 HD module includes a range of pre- and post-processing software which eases the input of data and analysis of simulation results. The software can be applied to the data and results of all the MIKE 21 modules.

Some examples of the software capabilities are:

- Input of time series and 2-D data
- Isoline plots of any variable
- 2-D vector plots of current patterns
- Plots of the variation in space of a variable along any line through the model
- 3-D plots of bathymetries, surface levels, concentrations
- Statistical analysis of time or space variation of any variable.



All graphical presentations can be in colour, produced with the UNIRAS graphics package.

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Appendix B

MIKE 21 AD Advection-Dispersion Module A Short Description



MIKE 21 AD - Release 1.0

ADVECTION-DISPERSION MODULE

A SHORT DESCRIPTION



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MIKE 21 AD - ADVECTION-DISPERSION MODULE

SHORT DESCRIPTION

Introduction

MIKE 21 is a comprehensive modelling system for 2-dimensional free surface flows where stratification can be neglected.

The advection-dispersion module of **MIKE 21** simulates the spreading of a dissolved or suspended substance in an aquatic environment under the influence of the fluid transport and associated natural dispersion processes. The substance may be a pollutant of any kind, conservative or non-conservative, inorganic or organic: salt, heat, dissolved oxygen, inorganic phosphorus, nitrogen and other such water quality parameters.

In a similar way to the hydrodynamic stage, the concentration of the substance is calculated at each point of a rectangular grid covering the area of interest. Information on the transport, i.e. currents and water depths at each point of the grid, are provided by the hydrodynamic module. Other data required includes substance concentrations and discharge quantities at outfalls, together with concentrations at boundaries.

The system solves the equation of conservation of mass for a dissolved or suspended substance using a two-dimensional form of the **QUICKEST** finite difference scheme.

Applications

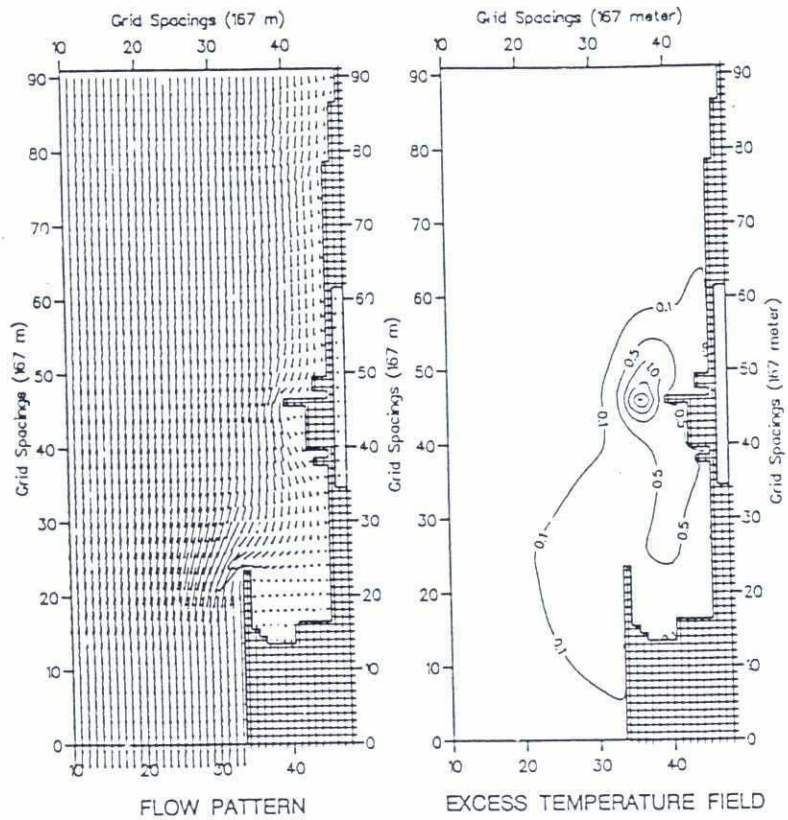
There are in principle two types of investigations for which the **M21AD** module is an essential part:

- Cooling water recirculation studies for power plants and salt recirculation studies for desalination plants
- Water quality studies connected with sewage outfalls and non-point pollution sources

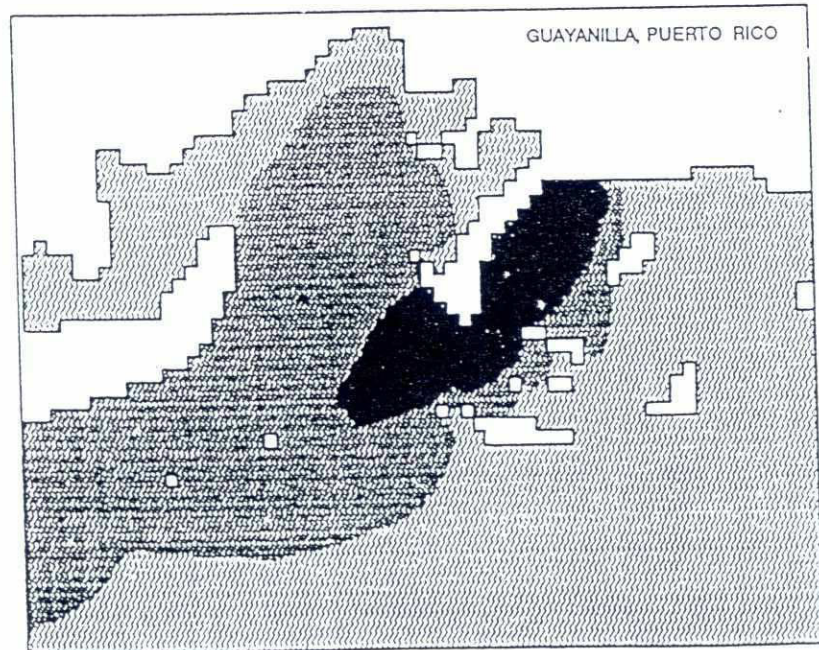
Some illustrations follow:



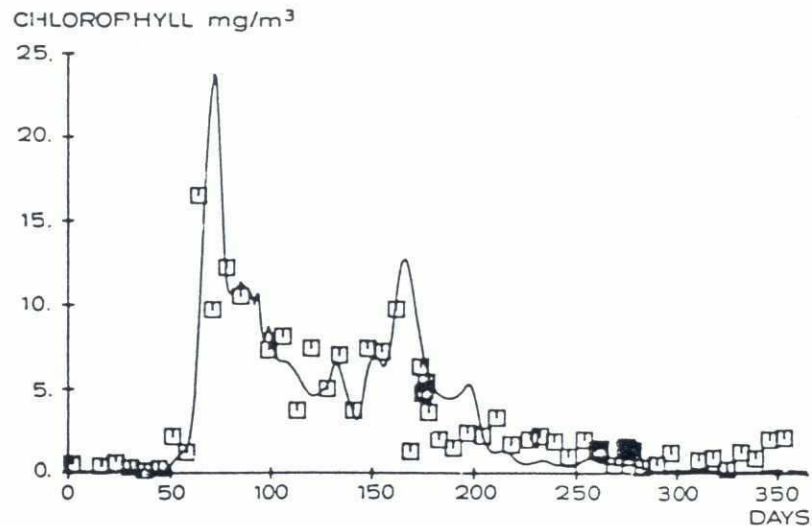
- Cooling water recirculation



- Spreading of bacteria or pollutants from sewage outfalls



• Water quality studies



Equation

M21AD solves the so-called advection-dispersion equation for dissolved or suspended substances in two dimensions. This is in reality the mass-conservation equation. Discharge quantities and compound concentrations at source and sink points are included together with a decay rate.

$$\frac{\partial}{\partial t}(hC) + \frac{\partial}{\partial x}(uhC) + \frac{\partial}{\partial y}(v hC) = \frac{\partial}{\partial x} \left(h \cdot D_x \cdot \frac{\partial C}{\partial x} \right) + \frac{\partial}{\partial y} \left(h \cdot D_y \cdot \frac{\partial C}{\partial y} \right) - F \cdot h \cdot C + S$$

Symbol List

C	-	compound concentration (arbitrary units)
u,v	-	horizontal velocity components in the x,y directions (m/s)
h	-	water depth (m)
D _x ,D _y	-	dispersion coefficients in the x,y directions (m ² /s)
F	-	linear decay coefficient (1/s)
S =		Q _s · (C _s -C)
Q _s	-	source/sink discharge per unit horizontal area (m ³ /s/m ²)



6 a)

C_s - concentration of compound in the source/sink discharge.

Information on u , v and h at each time step is provided by the hydrodynamic module M21HD.

Calibration Factors

Calibration Factors are the dispersion coefficients D_x and D_y , and the decay coefficient F .

Suitable methods for calculating or assigning dispersion coefficients are the subject of intense research and have not yet been resolved. One of the few well-established theories is for the dispersion due to the vertical logarithmic velocity profile. Elder (1959) found that the equivalent dispersion coefficient is proportional to $u_* h$, where u_* is the friction velocity. This is the basis for one of the options in M21AD where the dispersion coefficient can be chosen proportional to the flux density $u_* h$.

The other option is for the user to select his own coefficients to reproduce measured dispersion. These are constant in time but can be variable in space.

Heat Dissipation

In cooling water recirculation studies, the compound concentration, C , becomes excess temperature, ΔT , and the decay rate, F , becomes the heat exchange with the atmosphere. F is primarily dependent on the wind speed and ambient temperature.

$$F = \frac{0.2388}{\rho C_p h} (4.6 - 0.09 (T + C)) \\ + 4.06 W \exp (0.033 (T + C))$$

Symbol List

T	-	reference temperature ($^{\circ}\text{C}$)
W	-	wind speed (m/s), constant or time varying
ρ	-	density of water (kg/m^3)
C_p	-	specific heat of water.

Future Developments

Future releases of the AD module will include more advanced methods for automatic calculation of dispersion coefficients.

Solution Technique

The advection-dispersion equation is solved using an explicit, third-order finite difference scheme which is generally known as the QUICKEST scheme. This scheme has been described in various papers dealing with turbulence modelling, environmental modelling and other problems involving the advection-dispersion equation. It has several advantages over other schemes, especially that it avoids the "wobble" instability problem associated with central differencing of the advection terms, and at the same time it greatly reduces the numerical damping which is characteristic of first-order upwinding methods.

The scheme itself is a Lax-Wendroff or Leith-like scheme in the sense that it cancels out the truncation error terms due to time differencing up to a certain order by using the basic equation itself. In the case of QUICKEST, truncation error terms up to third-order are cancelled for both space and time derivatives. See Reference List for further information.

Data Requirements

Basic Model Parameters

- Model grid size and extent
- Time step and length of simulation
- Type of output required and its frequency

Bathymetry and Hydrodynamic Input

Calibration Factors

- Dispersion coefficients
- Decay coefficient

Initial Conditions

- Compound concentrations

Boundary Conditions

- Compound concentrations



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Other Driving Forces

Wind speed and ambient temperature for cooling water studies

Source/sink discharge magnitude and compound concentrations.

List of References

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Appendix C

MIKE 21 NSW
Nearshore Spectral Wind-Wave Module
A Short Description



MIKE 21 NSW - Release 1.2

NEARSHORE SPECTRAL WIND-WAVE MODULE

A SHORT DESCRIPTION



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MIKE 21 NSW - NEARSHORE SPECTRAL WIND-WAVE MODULE

SHORT DESCRIPTION

Introduction

MIKE 21 NSW is DHI's wind-wave model which describes the propagation, growth and decay of short-period waves in nearshore areas. The model takes into account the effects of refraction and shoaling due to varying depth, wind generation and energy dissipation due to bottom friction and wave breaking. The effects of current on these phenomena are included.

MIKE 21 NSW is a stationary, directionally decoupled parametric model. To take into account the effect of current the basic equations in the model are derived from the conservation equation for the spectral wave action density. A parameterization of the conservation equation in the frequency domain is performed introducing the zero-th and the first moment of the action spectrum as dependent variables. From these variables wave parameters such as the significant wave height, the mean wave period and the mean wave direction can be determined.

The basic equations are solved using an Eulerian finite-difference technique.

Basic Equations

The conservation equations for the zero-th and the first moment, m_0 and m_1 , of the action spectrum A can be written (Holthuijsen et al., 1989)

$$\frac{\partial (c_{gx} m_0)}{\partial x} + \frac{\partial (c_{gy} m_0)}{\partial y} + \frac{\partial (c_\theta m_0)}{\partial \theta} = T_0 \quad (1)$$

$$\frac{\partial (c_{gx} m_1)}{\partial x} + \frac{\partial (c_{gy} m_1)}{\partial y} + \frac{\partial (c_\theta m_1)}{\partial \theta} = T_1$$

where

- $m_0(x, y, \theta)$ - Zero-th moment of the action spectrum
- $m_1(x, y, \theta)$ - First moment of the action spectrum
- c_{gx} and c_{gy} - Components in the x- and y-direction, respectively, of the group velocity c_g
- c_θ - Propagation speed representing the change of action in the θ -domain
- x and y - Cartesian coordinates
- θ - Direction of wave propagation
- T_0 and T_1 - Source terms

The moments $m_n(\theta)$ are defined

$$m_n(\theta) = \int_0^\infty \omega^n A(\omega, \theta) d\omega \quad (2)$$

where ω is the absolute frequency.

From $m_0(\theta)$ and $m_1(\theta)$ two wave parameters can be calculated: the directional action spectrum $A_0(\theta) = m_0(\theta)$ and the mean frequency per direction $\omega_0(\theta) = m_1(\theta)/m_0(\theta)$.

The propagation speeds c_{gx} , c_{gy} and c_θ are obtained using linear wave theory.

The left hand side of the basic equations (1) takes into account the effect of refraction and shoaling. The source terms T_0 and T_1 take into account the effect of energy input from the wind, bottom dissipation, wave breaking and wave blocking. The effects of current on these phenomena are included. The formulation of the source terms for wind generation of waves is based on empirical formulas for the wave growth for fetch-limited sea states in deep water (Shore Protection Manual). The description of the bottom dissipation is based on the quadratic



friction law to represent bottom shear stress (Svendsen and Johnsson, 1980) and the description of the wave breaking is based on the expressions given by Battjes and Janssen (1978). The effect of the bottom dissipation and wave breaking on the mean frequency is also included.

Numerical Solutions

The two coupled partial differential equations are solved using Eulerian finite-difference technique. The zero-th and the first moment are calculated on a rectangular grid for a number of discrete directions.

A once-through marching procedure is applied in the predominant direction of wave propagation restricting the angle between the direction of wave propagation and the marching direction to less than 90° . Due to stability conditions the angle is usually less than 60° depending on the mesh sizes.

Input/Output

The basic input to the model is the bathymetry, the current and wind field and the boundary condition at the up-wave boundary. The boundary conditions can be given in form of transfer-data (the directional spectrum of m_0 and m_1 along the boundary) from a previous calculation, or in form of the significant wave height, the mean wave period and the directional distribution at the boundary.

The results of the computations can be stored in the form of the discrete values of the zero-th and the first moments of the action spectrum, or in form of selected wave parameters such as the significant wave height, the mean wave period, the mean wave direction and the directional standard deviation. These results can then be presented graphically through the use of a range of service programs. It is possible to obtain for example:

- Isoline plots of any variable
- Plots of variation in space of a variable along any line through the model area
- 2D vector plots showing the mean wave direction
- 3D plots of bathymetries.



yx

(A few examples of the graphical presentation are shown on the following page).

Calibration Factors

The main calibration factors using MIKE 21 NSW are the bottom friction coefficients - the wave friction factor f_w and the current friction factor f_c . The friction factor f_w can be given either explicit or calculated using a semi-empirical formula given the Nikuradse roughness parameter k_n .

Normally, the calibration of the model for a specific study is quite easy. In practice, the most important factor in the calibration is the accuracy of the data, e.g. bathymetry, boundary data, and wind and current fields.

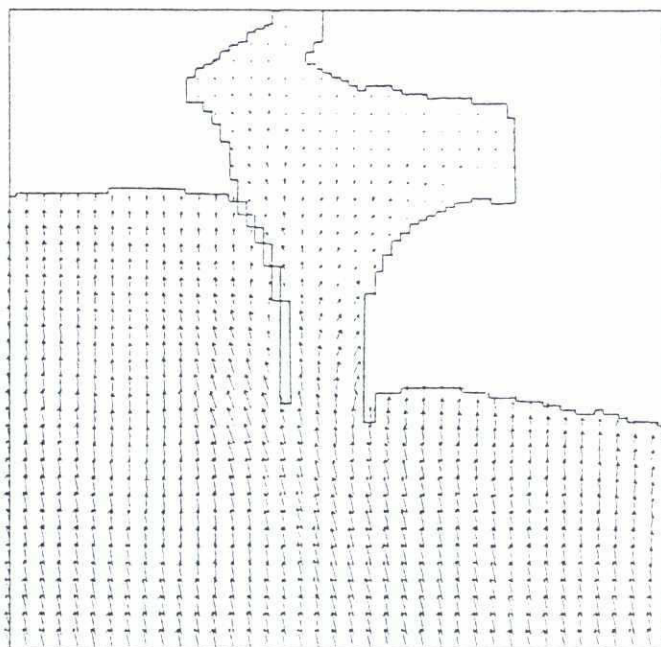


Fig. 1 Vector plot showing the mean wave direction where the vector length is scaled relative to the significant wave heights.

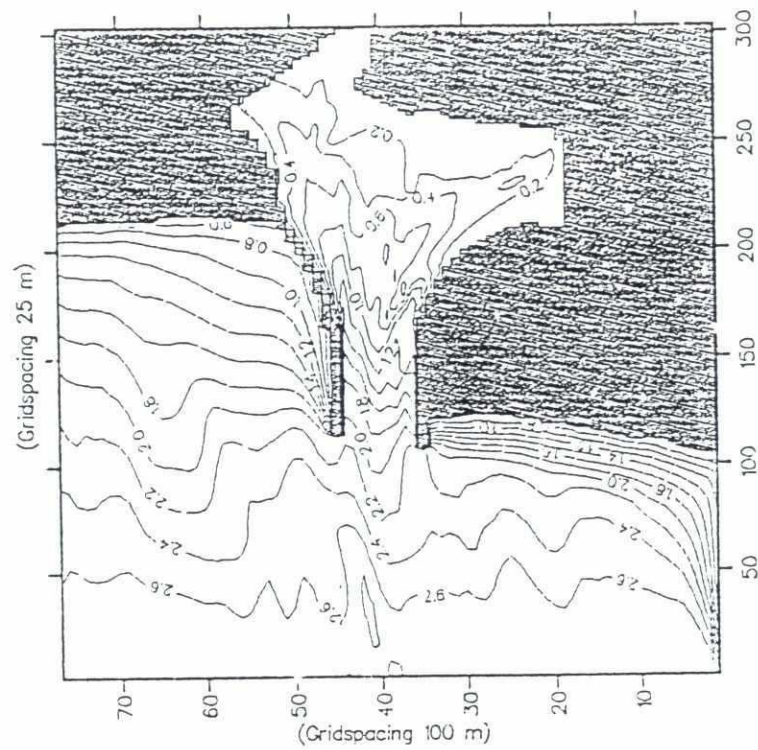


Fig. 2 Contour plot of the significant wave height.



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CERC, "Shore Protection Manual", U.S. Army Coastal Eng. Res. Center, Corps Engineers, Volume 1, 1984.

Appendix D

MIKE 21 ST
Non-Cohesive Sediment Transport Module
A Short Description



MIKE 21 ST - Release 2.0
NON-COHESIVE SEDIMENT TRANSPORT MODULE
A SHORT DESCRIPTION



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MIKE 21 ST - NON-COHESIVE SEDIMENT TRANSPORT MODULE

SHORT DESCRIPTION

Introduction

MIKE 21 is a comprehensive modelling system for 2-dimensional free surface flows where stratification can be neglected.

MIKE 21 ST is a sediment transport module of the system for assessing rates of bed level changes in coastal areas subject to the action of waves and currents. The sediments are assumed to be non-cohesive, i.e. sand, but may vary in grain size throughout the model area. The currents may be due to tide, they may be wind-driven or even wave-driven. The effect of both non-breaking and breaking waves are included in the module computations.

For given bathymetry, sediment type, water depth, currents and wave patterns, the MIKE 21 ST module calculates the sediment transport capacity at each point of a rectangular grid covering the area of interest. Erosion and deposition rates in the model area are thereby estimated.

The data concerning current and wave conditions is provided by other modules of the MIKE 21 system and are prepared prior to the simulations with MIKE 21 ST. The water depth and current conditions due to tide and wind will be calculated with the hydrodynamic module MIKE 21 HD which can also give the wave-driven currents through the inclusion of the wave radiation stresses. The wave fields can be calculated by MIKE 21 SW, the deterministic wave module, or by MIKE 20 NS, DHI's spectral wind-wave modelling system for near-shore areas. Even a wave field developed from a refraction/diffraction model or a desk study can be used.

The structure of the module and the possible connections with other MIKE modules are illustrated in Figure 1.

The principal applications of MIKE 21 ST concern the estimation of erosion and deposition around large coastal structures such as large groynes, breakwaters, river mouths and protection works generally.

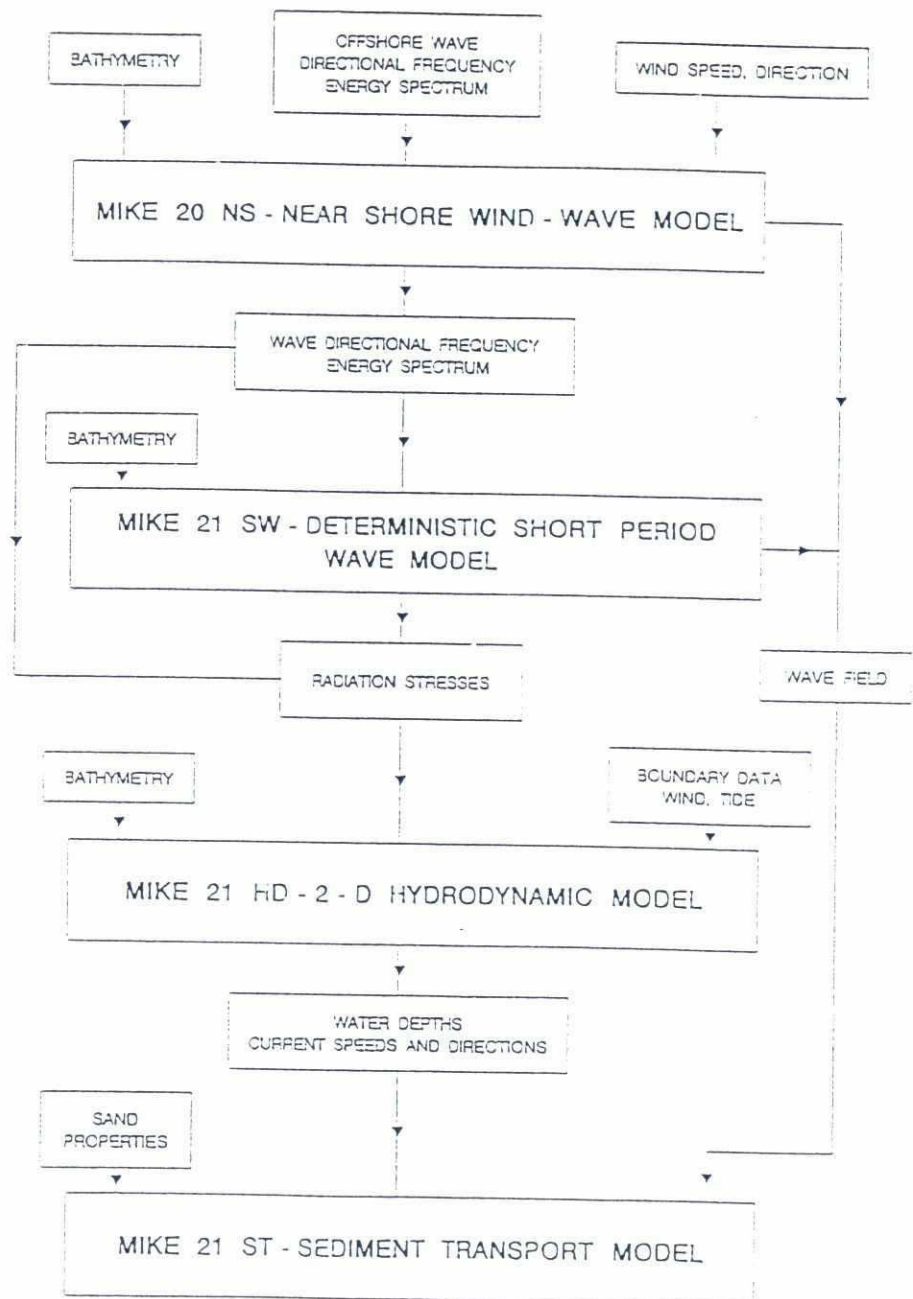


Fig. 1a

The interaction of MIKE 21 ST with other modules of the MIKE system.

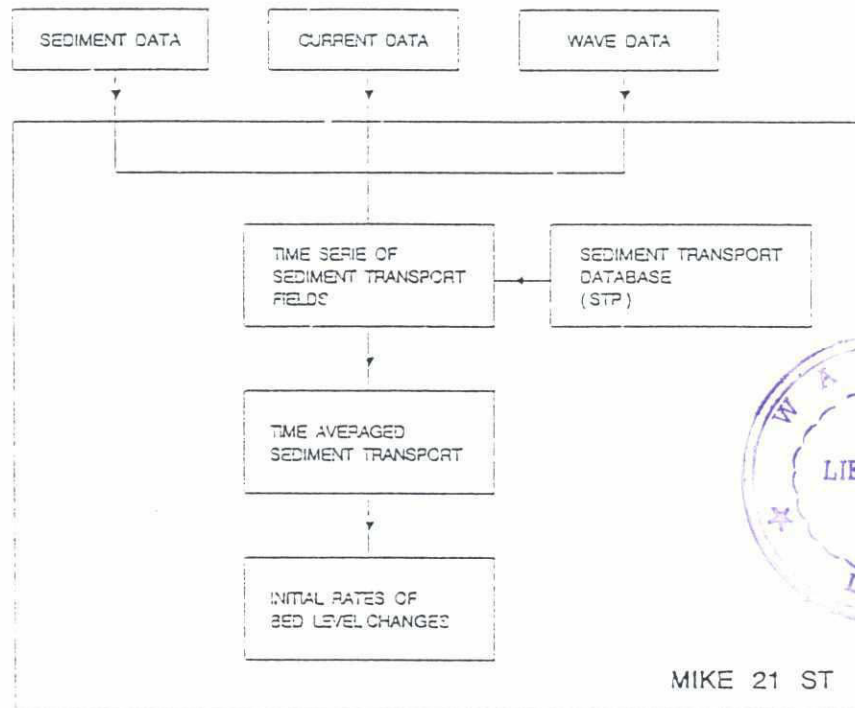


Fig. 1b

Illustration of structure of MIKE 21 ST.

Theoretical Background

The core of the MIKE 21 ST is the calculation of the sediment transport capacity as function of the local wave, current and sediment conditions. This calculation is carried out by the DHI model STP which is a detailed intra-wave-period model for description of the time-varying distribution of suspended sediment and bed load over the wave period in combined wave and current motion, including effects of wave breaking if relevant.

The STP model is included directly in MIKE 21 ST where it is used to establish a comprehensive data base of transport rates



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corresponding to the relevant ranges of the parameters: current speed, depth, wave height and period, breaking/non-breaking waves, grain size.

The rates of bed level changes, $\partial z/\partial t$, are described by the equation of continuity:

$$\frac{\partial z}{\partial t} + \frac{1}{1-n} \frac{\partial q_x}{\partial x} + \frac{1}{1-n} \frac{\partial q_y}{\partial y} = 0 \quad ,$$

where

x, y, t are independent variables
 q_x, q_y are sediment transport components in x - and y -directions
 z is the bed level
 n is the porosity of the bed material.

This equation is solved by a finite difference model.

The module, STP, which calculates the sediment transport rates, is briefly described below.

The Sediment Transport Module, STP

In combined waves and current the turbulent interaction in the near bed boundary layer is of importance for the bed shear stresses as well as for the eddy viscosity distribution. The basis for the sediment transport description is the model for turbulent wave-current boundary layers of Fredsøe (1984). The boundary layer is composed of two regions:

Close to the bed the turbulence and the shear stress in the wave boundary layer vary with the wave period, giving rapidly changing bed concentration and turbulent diffusion coefficients.

Outside the wave boundary layer the mean velocity is described by a log-profile. The increased turbulence level in the wave boundary layer retards the mean current, an effect which is expressed through an apparent wave roughness, k_w , which is larger than the natural bed roughness k .

The transport of non-cohesive material is calculated according to the model presented by Engelund and Fredsøe (1976). Through subsequent developments this model has been extended to cover combined waves and current, and conditions in the surf zone.

The total sediment load is split into bed load and suspended load, which are calculated separately. The bed load transport is

calculated as a function of the bed shear stress through the dimensionless bed shear stress, θ :

$$\theta = U_f^2 / (s-1)gd$$

s is the relative sediment density, g the acceleration of gravity, d the grain size and U_f is the shear velocity. The bed load transport is assumed to correspond to the instantaneous bed shear stress under unsteady conditions, e.g. under wave action.

The suspended load transport, q_s , is described through the sediment concentration c , which is determined from the vertical turbulent diffusion equation:

$$\frac{\partial c}{\partial t} = \frac{\partial}{\partial z} \left[\epsilon_s \frac{\partial c}{\partial z} \right] + w \frac{\partial c}{\partial z}$$

t is time, z the vertical coordinate (zero at the bed) ϵ_s the turbulent diffusion coefficient and w is the settling velocity of the sediment. ϵ_s is taken to be equal to the turbulent eddy viscosity of the flow field. The near-bed boundary condition is given as bed concentration C_b at the level $z = 2d$. C_b is determined as a function of θ using the dynamic considerations of Bagnold (1954), that a certain sediment concentration is required near the bed in order to transfer the shear stress to the bed through grain-grain interaction.

The bed concentration, C_b , is only valid for the plane bed case, i.e. sheet flow, which is found for θ larger than about 0.8. At smaller θ -values the bed is covered by wave ripples. The sediment transport model by Fredsøe et. al (1985) has been modified to take the effect of wave ripples into account. The modification involves the bed concentration, turbulent diffusion and the bed roughness. The values of C_b and ϵ are based directly on the laboratory measurements of Nielsen (1979). The roughness is expressed through the ripple dimensions as given by Raudkivi (1988). The sediment transport model converges gradually towards a plane bed description with increasing bed shear stress or mean current velocity.

Inside the surf zone, the wave energy is dissipated due to breaking, and the production of turbulence is very intense. This has been taken into account by use of a one-equation turbulence model (Deigaard et. al. (1986)).

Figure 2 shows the vertical mean sediment concentration profile calculated by STP, compared to full scale field measurements.



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The main results from STP are

- bed load
- suspended load

in combined breaking or non-breaking waves and current.

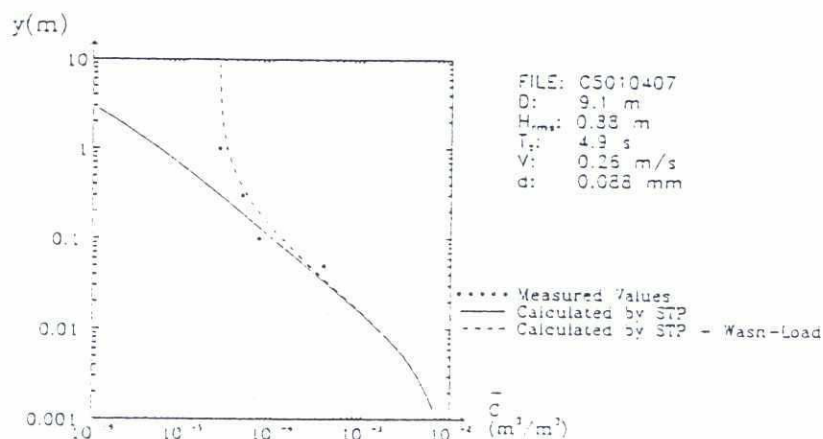


Fig. 2 Vertical profiles of mean sediment concentrations

Data Requirements

The basic parameters are: Model grid size and extent, bathymetry, length of simulation and time step between calculations of sediment transport fields and requirements to the output. Further, the module requires hydrodynamic input, water depths and currents, significant wave heights and periods in the defined grid points and grain size distribution over the model area. Prior to the MIKE 21 ST simulations, the service programme STP must produce a catalog of sediment transport rates. Input to STP is relevant ranges of the parameters wave heights and periods, current speed, depth, grain size ($d_{50\%}$).

Model Calibration

The hydrodynamic and wave models should be calibrated in the normal way by comparisons with field data.

The accuracy of the STP model should also be checked against field measurements of suspended sediment concentrations under a variety of wave and current conditions. However, a large number of comparisons have already been made so that the default parameter values can be used with confidence.

Further Developments

The present version of the sediment transport programme STP uses an average grain size $d_{50\%}$ and the corresponding fall velocity. A new version of STP which includes the effect of grading of the bed material will be available during 1991. This improvement requires input of a parameter all over the model area which reflects the grading of the bed material, for instance the spreading of a log normal distribution which represents the grain sizes.

The present version of STP calculates the transport rate assuming logarithmic current profiles. Inside the surf zone, the vertical distribution of flow might differ significantly from log-profiles due to undertow. Another more advanced version of STP includes calculation of the form of the current profile under quasi uniform conditions in breaking waves and current at an arbitrary angle. Implementation of this advanced version and extraction of the relevant parameters from the basic wave and current simulations, i.e. wave energy dissipation in the wave propagation direction and angle between waves and current will allow the effect of undertow to be included. This version will be tested during 1991.

The present model setup calculates the sediment transport capacity as a function of the local wave and current conditions. This assumption is good for medium to coarse sand, but for very fine sand there might be so-called time and space lag effects which attenuate the transport rates due to the time it takes to adjust the concentration profile to changed hydrodynamic conditions. A model complex which uses the MIKE 21 AD module (Advection Dispersion Module) to simulate this phenomenon is under development.

The present module MIKE 21 ST represents a single time step in a so-called morphological model with feedback from changed bathymetry to the wave and current calculations. MIKE 21 ST now works as a module in a research version of a deterministic morphological model which is currently being developed at DHI.



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Applications

An example of the application of MIKE 21 ST is taken from the Venice lagoon study.

The Venice lagoon is located in the north-western part of the Adriatic Sea, Figure 3.

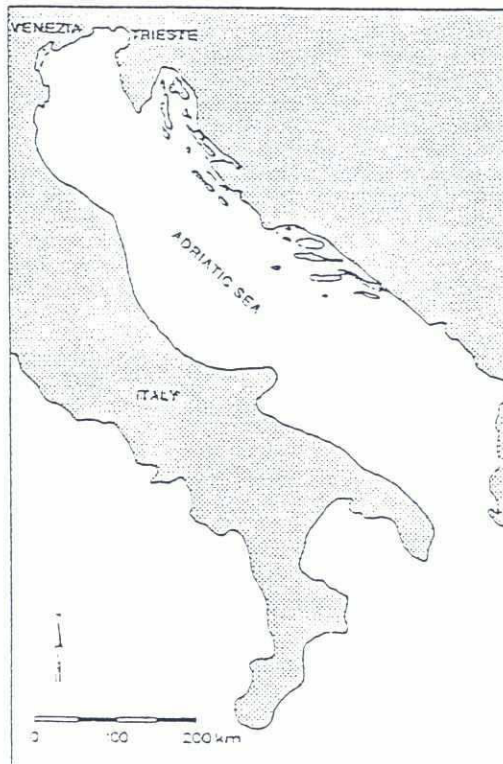


Fig. 3 Location map

The detail of the Venice coastline is shown in Figure 4.

This example treats the local area around Chioggia inlet for the existing constructions and strong Scirocco wind conditions, $H_s \approx 2.8$ m, tidal range 0.8 m.

Figure 5 shows the bathymetry of the area. The grain size of the bed material is digitized in a similar way and used as input to the model complex.

The calculated wave field is illustrated in Figure 6, in which isolines for significant wave heights are shown.

The time varying current field is calculated by the hydrodynamic model MIKE 21 HD. The driving forces included in

this simulation are wind, tide and variation in the radiation stresses (wave-driven currents). As an example, the current field at maximum flood flow is shown in Figure 7.

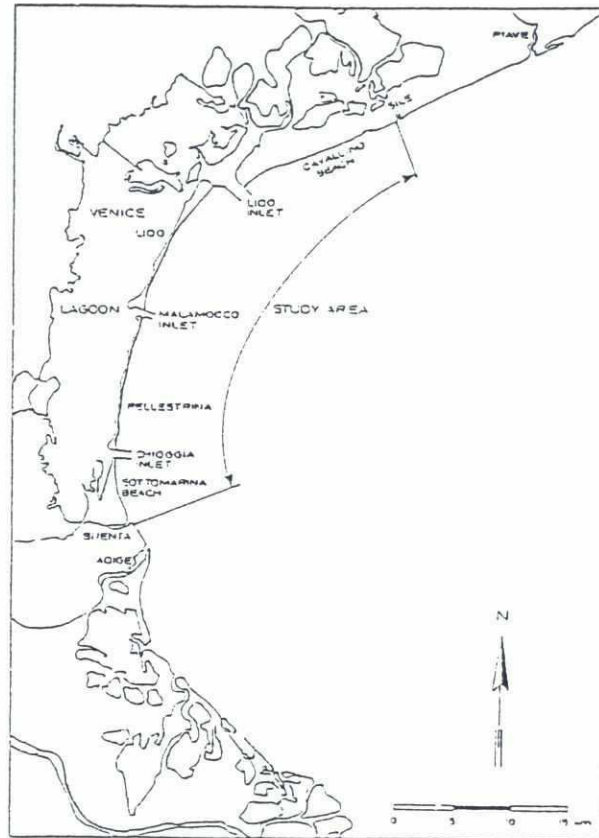


Fig. 4 Venice Lagoon and adjacent coast

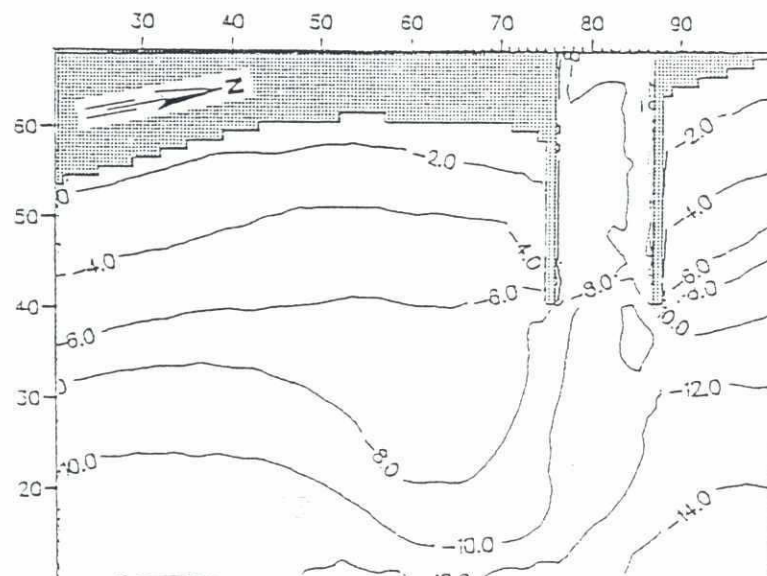


Fig. 5 Bathymetry

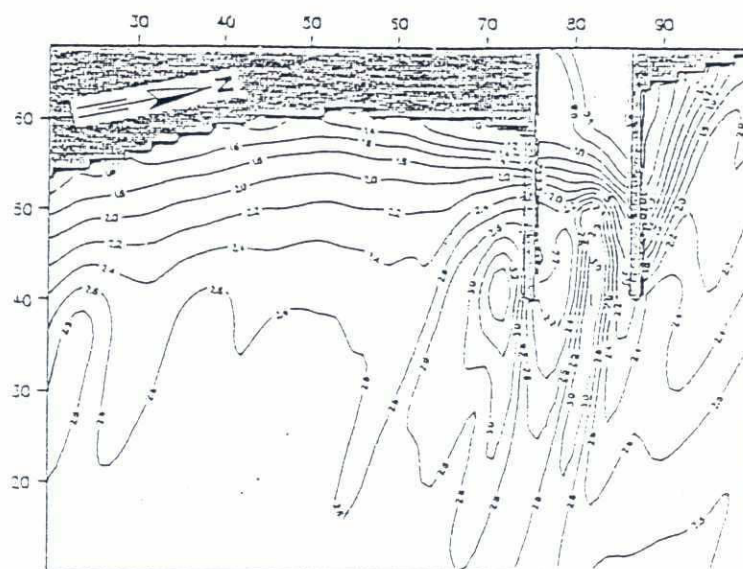


Fig. 6 Significant wave heights

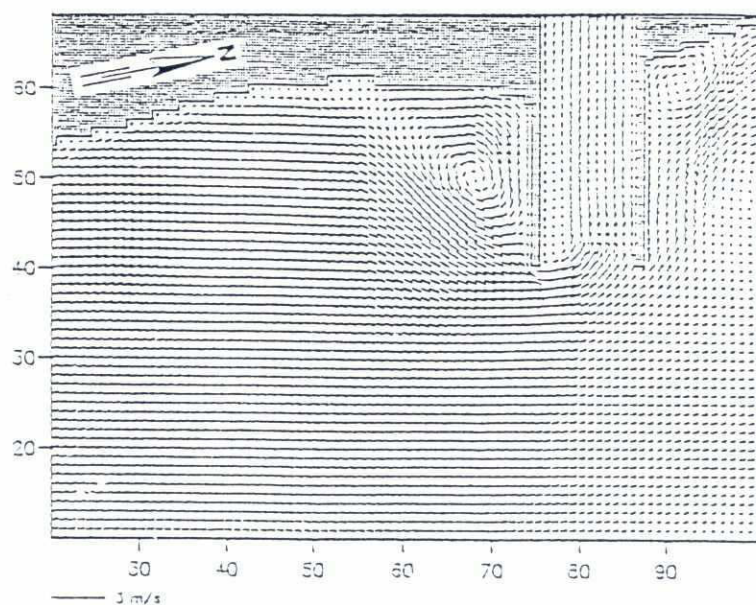


Fig. 7 Current pattern at maximum flood flow

The sediment transport field averaged over the tidal cycle has been calculated based on the wave field, the current fields and the grain size distribution.

The calculated average transport field is shown in Figure 8.

It appears that the wave-driven currents along Sottomarina carry large amounts of sediment. This so-called littoral drift is responsible for the evolution of Sottomarina Beach, which advances $\sim 6\text{m/year}$. Close to the southern jetty a large counter clockwise current vortex appears. This wave-driven current pattern occurs because the wave fronts are refracted around the shoal SE of the inlet. The sediment transport rates along the jetty increase strongly from outside to inside the surf zone. This is because the breaking waves are able to carry more sediment in suspension than the non-breaking waves.

The net transport in the inlet appears to be close to zero in this case. This is because the current speeds during ebb and flood flow are found from the current simulations to be nearly identical.

The duration per year of the conditions simulated in this example is estimated at 1.8 day/year - assuming that this condition represents all strong Scirocco wind cases.

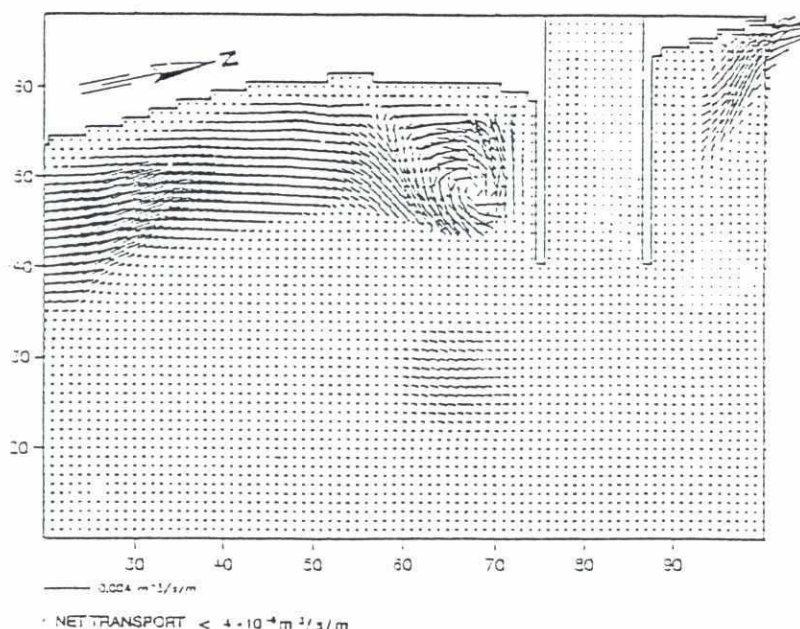


Fig. 8 Sediment transport field averaged over the tidal cycle

From the sediment transport field described above, the initial bed level changes per year corresponding to Scirocco wind are

determined. These calculated bed level changes are illustrated in Figure 9.

The bed level changes reflect the variations in the transport capacities. Along Sottomarina Beach the decrease in littoral drift leads to large deposition areas. The counter clockwise current and sediment transport pattern south of the jetty leads to erosion where the transport capacity is increased due to the increase from outside to inside the surf zone in the amount of suspended sediment. Inside the inlet no net erosion is seen because the transport capacity is identical during ebb and flood.

The erosion NE of the inlet takes place during ebb flow where the ebb flow jet passes this area.

The pattern SE of the inlet occurs due to the shoal. Erosion takes place where the water depth decreases in the current direction, and deposition takes place where the current has passed the shoal and the water depth increases (north of the shoal).

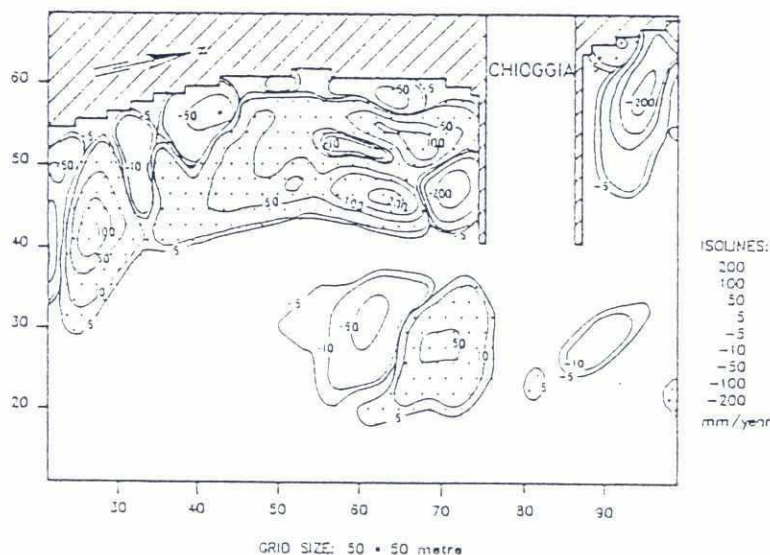


Fig. 9 Calculated initial bed level changes per year corresponding to strong scirocco wind



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Appendix E

Description of MES Numerical Modelling CD-ROM Archive

E Description of MES Numerical Modelling CD-ROM Archive

E.1 Contents of CD-ROMs

All major results from the numerical simulations have been saved in a CD-ROM archive as listed in table no. E.1, while the contents of all CD-ROM except the presentation CD-ROM are listed in sections E.3 - E.10.

Table no E.1 Contents of MES Numerical Modelling CD-ROM Archive

Volume Id	Contents
MES_DRY96A	Hydrodynamic Modelling, Dry Season 1996, calibration and base run, existing situation
MES_DRY96B	Hydrodynamic Modelling, Dry Season 1996, including intervention schemes
MES_MON96A	Hydrodynamic Modelling, Monsoon 1996, validation, existing situation
MES_DRY97A	Hydrodynamic Modelling, Dry Season 1997, validation, existing situation
MES_MON97A	Hydrodynamic Modelling, Monsoon 1997, calibration and base run, existing situation
MES_MON97B	Hydrodynamic Modelling, Monsoon 1997, including intervention schemes
MES_SALI	Salinity Modelling, Dry Season 1996, existing situation and including intervention schemes
MES_OTHER	<ul style="list-style-type: none">• Wind-wave Modelling of waves from SSE and SSW for use in sediment transport modelling• Sediment Transport Modelling, Dry Season 1996 (Spring Tide and Neap Tide) and Monsoon 1997 (Spring Tide and Neap Tide)• Hydrodynamic Modelling, Dry Season 1996, Nijhum Dwip Local Model, existing situation and including interventions• Raw bathymetry files (LANDSAT data, MES survey data etc.)• Water level measurements and tidal level predictions for calibration and validation periods• Program source codes for hdf flow and htmbnd.
MES_PRESENT	Presentation of Meghna Estuary Study Numerical Modelling including study report and animations of model results.

E.2 Format of CD-ROM Data

The CD-ROMs have been written using Joliet filename format, while the file formats used on the CD-ROMS are described in table no E.2.

Table no. E.2 MES CD-ROM file formats

Volume Id	File Formats
MES_DRY96A MES_DRY96B MES_MON96A MES_DRY97A MES_MON97A MES_MON97B MES_SALI	All files in subdirectories of the <i>cat</i> directory are MIKE 21 data files in UNIX/DOS/Windows format, while files in <i>wrk</i> directories are MIKE 21 specification files in UNIX format. The specification files correspond to MIKE 21 version 2.6.
MES_OTHER	<p>All files in subdirectories of the <i>cat</i> directory are MIKE 21 data files in UNIX/DOS/Windows format, while files in <i>wrk</i> and <i>work</i> directories are MIKE 21 specification files in UNIX format. The specification files correspond to MIKE 21 version 2.6.</p> <p>The <i>source</i> directory contains FORTRAN 77 source codes for programs <i>hdflow</i> (used to derive net and maximum flow from HD simulations) and <i>htmbnd</i> (used to compute boundary conditions for NSW simulations).</p> <p>The <i>bathyraw</i> directory contains XYZ data for model bathymetry generation:</p> <ul style="list-style-type: none"> • <i>orikms</i>: MES survey data • <i>water0</i>: Classified Landsat data (600 m grid) • <i>mes200</i>: Classified Landsat data (200 m grid) • <i>niz97</i>: 1997 shallow area line around Nijhum Dwip • <i>eXXX</i> and <i>cXXX</i>: BITWA data from charts XXX. <p>The <i>cat/bathyraw</i> directory contains MIKE 21 data files showing the bathymetry data sources:</p> <ul style="list-style-type: none"> • <i>bat-csps</i>: Bathymetry data used from CSPS • <i>bat-spot</i>: Landsat data • <i>bat-kms</i>: MES survey data • <i>bat-land</i>: land area outside Landsat data area
MES_PRESENT	The MES Numerical Modelling Presentation CD-ROM is viewed using a web browser like Netscape Navigator or Microsoft Internet Explorer. To start viewing the CD-ROM open file <i>index.htm</i> in the root directory of the CD-ROM in the web browser.

E.3 Contents of CD-ROM MES_DRY96A

Volume in drive F is MES_DRY96A

Volume Serial Number is 0B96-8A51

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WRKHDD-7	<DIR>	05-18-98	3:22p	wrkHDDry96
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Directory of F:\cat

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..	<DIR>	05-18-98	3:22p	..
BATHY	<DIR>	05-18-98	3:22p	bathy
BOUND	<DIR>	05-18-98	3:22p	bound
DRY96	<DIR>	05-18-98	3:22p	Dry96
WIND	<DIR>	05-18-98	3:22p	wind
	0 file(s)		0 bytes	

Directory of F:\cat\bathy

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..	<DIR>	05-18-98	3:22p	..
BATHYFIN CT2	1,052	04-27-98	11:07a	bathyfin.ct2
BATHYFIN DT2	421,648	04-27-98	11:07a	bathyfin.dt2
BEDFRIC CT2	1,052	05-03-98	11:54a	bedfric.ct2
BEDFRIC DT2	421,648	04-21-98	3:40p	bedfric.dt2
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HDFLNM DT2	1,686,592	05-26-98	2:38p	hdflNm.dt2
HDFLNN CT2	1,052	05-26-98	2:38p	hdflNn.ct2
HDFLNN DT2	1,686,592	05-26-98	2:38p	hdflNn.dt2
HDFLSM CT2	1,052	05-26-98	2:39p	hdflSm.ct2
HDFLSM DT2	1,686,592	05-26-98	2:39p	hdflSm.dt2
HDFLSN CT2	1,052	05-26-98	2:39p	hdflSn.ct2

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HDFLSN	DT2	1,686,592	05-26-98	2:39p	hdflsn.dt2
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HDMAX	DT2	843,296	05-17-98	4:21p	hdmax.dt2
HDMEAN	CT2	1,052	05-17-98	4:24p	hdmean.ct2
HDMEAN	DT2	843,296	05-17-98	4:24p	hdmean.dt2
HDMIN	CT2	1,052	05-17-98	4:26p	hdmin.ct2
HDMIN	DT2	843,296	05-17-98	4:26p	hdmin.dt2
NEAP96	CT2	1,052	05-04-98	2:33a	Neap96.ct2
NEAP96	DT2	126,916,048	05-03-98	11:41p	Neap96.dt2
SIM0296A	CT0	1,052	05-12-98	10:04a	sim0296A.ct0
SIM0296A	DT0	49,216	05-12-98	10:04a	sim0296A.dt0
SIM0296B	CT0	1,052	05-12-98	10:23a	sim0296B.ct0
SIM0296B	DT0	24,608	05-12-98	10:23a	sim0296B.dt0
SPRING96	CT2	1,052	05-04-98	2:33a	Spring96.ct2
SPRING96	DT2	126,916,043	05-03-98	6:48p	Spring96.dt2
TIDCON	CT2	1,052	05-23-98	6:02a	tidcon.ct2
TIDCON	DT2	4,638,128	05-23-98	6:02a	tidcon.dt2
		26 file(s)	592,502,940 bytes		

Directory of F:\cat\wind

.	<DIR>		05-18-98	3:22p	.
..	<DIR>		05-18-98	3:22p	..
HATIA0-6	CT0	1,052	04-23-98	12:37p	hatia0296.ct0
HATIA0-8	DT0	1,792	04-23-98	12:37p	hatia0296.dt0
		2 file(s)	2,844 bytes		

Directory of F:\wrkHDDry96

.	<DIR>		05-18-98	3:22p	.
..	<DIR>		05-18-98	3:22p	..
M21HD	INP	5,012	05-03-98	3:23p	m21hd.inp
		1 file(s)	5,012 bytes		

Total files listed:

37 file(s)	595,564,372 bytes
18 dir(s)	0 bytes free

E.4 Contents of CD-ROM MES_DRY96B

Volume in drive F is MES_DRY96B

Volume Serial Number is A403-09FF

Directory of F:\

CAT	<DIR>	05-26-98	5:13p	cat
WRKHDD~7	<DIR>	05-26-98	5:13p	wrkHDDdry96
	0 file(s)		0 bytes	

Directory of F:\cat

.	<DIR>	05-26-98	5:13p	.
..	<DIR>	05-26-98	5:13p	..
BATHY	<DIR>	05-26-98	5:13p	bathy
BOUND	<DIR>	05-26-98	5:13p	bound
DRY96	<DIR>	05-26-98	5:13p	Dry96
WIND	<DIR>	05-26-98	5:13p	wind
	0 file(s)		0 bytes	

Directory of F:\cat\bathy

.	<DIR>	05-26-98	5:13p	.
..	<DIR>	05-26-98	5:13p	..
BATHYI13 CT2	1,052	05-24-98	11:13a	bathyI13.ct2
BATHYI13 DT2	421,648	05-24-98	10:16a	bathyI13.dt2
BATHY~10 CT2	1,052	05-24-98	11:04a	bathyIall.ct2
BATHY~12 DT2	421,648	05-24-98	11:04a	bathyIall.dt2
BATHY~14 CT2	1,052	05-24-98	10:27a	bathyIex8.ct2
BATHY~16 DT2	421,648	05-24-98	10:27a	bathyIex8.dt2
BEDFRIC CT2	1,052	05-03-98	11:54a	bedfric.ct2
BEDFRIC DT2	421,648	04-21-98	3:40p	bedfric.dt2
	8 file(s)		1,690,800 bytes	

Directory of F:\cat\bound

.	<DIR>	05-26-98	5:13p	.
..	<DIR>	05-26-98	5:13p	..
CHAN02~6 CT0	1,052	04-19-98	11:03a	chan0296PW.ct0
CHAN02~8 DT0	76,640	04-19-98	11:03a	chan0296PW.dt0
S96DRY CT1	1,052	05-03-98	12:08p	s96Dry.ct1
S96DRY DT1	2,129,432	03-07-98	12:11p	s96Dry.dt1
	4 file(s)		2,208,176 bytes	

Directory of F:\cat\Dry96

.	<DIR>	05-26-98	5:13p	.
..	<DIR>	05-26-98	5:13p	..
HDFLI1~6 CT2	1,052	05-26-98	3:02p	hdflI13Nn.ct2
HDFLI1~8 DT2	1,686,592	05-26-98	3:02p	hdflI13Nm.dt2
HDFLI~10 CT2	1,052	05-26-98	3:03p	hdflI13Sm.ct2
HDFLI~12 DT2	1,686,592	05-26-98	3:02p	hdflI13Nn.dt2
HDFLI~14 CT2	1,052	05-26-98	3:03p	hdflI13Sn.ct2
HDFLI~16 DT2	1,686,592	05-26-98	3:03p	hdflI13Sm.dt2



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HDFLI-18	CT2	1,052	05-26-98	3:02p	hdflI13Nm.ct2
HDFLI-20	DT2	1,686,592	05-26-98	3:03p	hdflI13Sn.dt2
HDFLI-22	CT2	1,052	05-26-98	3:17p	hdflIallNm.ct2
HDFLI-24	DT2	1,686,592	05-26-98	3:17p	hdflIallNm.dt2
HDFLI-26	CT2	1,052	05-26-98	3:17p	hdflIallNn.ct2
HDFLI-28	DT2	1,686,592	05-26-98	3:17p	hdflIallNn.dt2
HDFLI-30	CT2	1,052	05-26-98	3:18p	hdflIallSm.ct2
HDFLI-32	DT2	1,686,592	05-26-98	3:18p	hdflIallSm.dt2
HDFLI-34	CT2	1,052	05-26-98	3:18p	hdflIallSn.ct2
HDFLI-36	DT2	1,686,592	05-26-98	3:18p	hdflIallSn.dt2
HDFLI-38	CT2	1,052	05-26-98	3:11p	hdflIex8Nm.ct2
HDFLI-40	DT2	1,686,592	05-26-98	3:11p	hdflIex8Nm.dt2
HDFLI-42	CT2	1,052	05-26-98	3:11p	hdflIex8Nn.ct2
HDFLI-44	DT2	1,686,592	05-26-98	3:11p	hdflIex8Nn.dt2
HDFLI-46	CT2	1,052	05-26-98	3:12p	hdflIex8Sm.ct2
HDFLI-48	DT2	1,686,592	05-26-98	3:12p	hdflIex8Sm.dt2
HDFLI-50	CT2	1,052	05-26-98	3:12p	hdflIex8Sn.ct2
HDFLI-52	DT2	1,686,592	05-26-98	3:12p	hdflIex8Sn.dt2
HDI13MAX	CT2	1,052	05-25-98	11:18a	hdI13max.ct2
HDI13MAX	DT2	843,296	05-25-98	11:18a	hdI13max.dt2
HDI13MIN	CT2	1,052	05-25-98	12:08p	hdI13min.ct2
HDI13MIN	DT2	843,296	05-25-98	12:08p	hdI13min.dt2
HDI13TSA	CT0	1,052	05-25-98	10:17a	hdI13tsA.ct0
HDI13TSA	DT0	49,216	05-25-98	10:16a	hdI13tsA.dt0
HDI13TSB	CT0	1,052	05-25-98	10:28a	hdI13tsB.ct0
HDI13TSB	DT0	24,608	05-25-98	10:27a	hdI13tsB.dt0
HDI13-62	CT2	1,052	05-25-98	11:51a	hdI13mean.ct2
HDI13-64	DT2	843,296	05-25-98	11:51a	hdI13mean.dt2
HDIALl	CT2	1,052	05-26-98	2:55a	hdIall.ct2
HDIALl	DT2	324,668,960	05-26-98	2:55a	hdIall.dt2
HDIAL-78	CT0	1,052	05-26-98	12:14p	hdIalltsA.ct0
HDIAL-80	CT2	1,052	05-26-98	12:06p	hdIallmax.ct2
HDIAL-82	DT0	49,216	05-26-98	12:14p	hdIalltsA.dt0
HDIAL-84	DT2	843,296	05-26-98	12:06p	hdIallmax.dt2
HDIAL-86	CT0	1,052	05-26-98	12:14p	hdIalltsB.ct0
HDIAL-88	CT2	1,052	05-26-98	12:14p	hdIallmean.ct2
HDIAL-90	DT0	24,608	05-26-98	12:14p	hdIalltsB.dt0
HDIAL-92	DT2	843,296	05-26-98	12:14p	hdIallmean.dt2
HDIAL-94	CT2	1,052	05-26-98	12:14p	hdIallmin.ct?
HDIAL-96	DT2	843,296	05-26-98	12:14p	hdIallmin.dt2
HDIE-98	CT0	1,052	05-25-98	10:41a	hdIex8tsA.ct0
HDIE-100	CT2	1,052	05-25-98	12:24p	hdIex8max.ct2
HDIE-102	DT0	49,216	05-25-98	10:41a	hdIex8tsA.dt0
HDIE-104	DT2	843,296	05-25-98	12:24p	hdIex8max.dt2
HDIE-106	CT0	1,052	05-25-98	10:45a	hdIex8tsB.ct0
HDIE-108	CT2	1,052	05-25-98	12:39p	hdIex8mean.ct2
HDIE-110	DT0	24,608	05-25-98	10:45a	hdIex8tsB.dt0
HDIE-112	DT2	843,296	05-25-98	12:39p	hdIex8mean.dt2
HDIE-114	CT2	1,052	05-25-98	12:45p	hdIex8min.ct2
HDIE-116	DT2	843,296	05-25-98	12:45p	hdIex8min.dt2
NEAP-118	CT2	1,052	05-26-98	2:55a	Neap96Iall.ct2
NEAP-120	DT2	126,916,048	05-25-98	5:18p	Neap96Iall.dt2
SPR9-122	CT2	1,052	05-26-98	2:55a	Spr96Iall.ct2
SPR9-124	DT2	126,916,048	05-24-98	11:38p	Spr96Iall.dt2
60 file(s) 606,582,856 bytes					

Directory of F:\cat\wind

.	<DIR>	05-26-98	5:13p	.
..	<DIR>	05-26-98	5:13p	..
HATIA0-6	CT0	1,052	04-23-98	12:37p hatia0296.ct0

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HATIA0-8 DTO 1,792 04-23-98 12:37p hatia0296.dto
 2 file(s) 2,844 bytes

Directory of F:\wrkHDdry96

.	<DIR>	05-26-98	5:13p	.
..	<DIR>	05-26-98	5:13p	..
M21HDI13	INP	5,048	05-24-98 11:08a	m21hdI13.inp
M21HDI~8	INP	5,067	05-24-98 11:11a	m21hdIex8.inp
M21HD~10	INP	5,052	05-24-98 11:12a	m21hdIall.inp
3 file(s)		15,167 bytes		

Total files listed:

77 file(s)	610,499,843 bytes
18 dir(s)	0 bytes free

E.5 Contents of CD-ROM MES_MON96A

Volume in drive F is MES_MON96A

Volume Serial Number is E97E-793F

Directory of F:\

CAT	<DIR>	05-22-98 10:23a cat
WRKHDM~7	<DIR>	05-22-98 10:23a wrkHdmon96
0 file(s)		0 bytes

Directory of F:\cat

.	<DIR>	05-22-98 10:23a .
..	<DIR>	05-22-98 10:23a ..
BATHY	<DIR>	05-22-98 10:23a bathy
BOUND	<DIR>	05-22-98 10:23a bound
MON96	<DIR>	05-22-98 10:23a Mon96
WIND	<DIR>	05-22-98 10:23a wind
0 file(s)		0 bytes

Directory of F:\cat\bathy

.	<DIR>	05-22-98 10:23a .
..	<DIR>	05-22-98 10:23a ..
BATHYFIN CT2	1,052	04-27-98 11:07a bathyfin.ct2
BATHYFIN DT2	421,648	04-27-98 11:07a bathyfin.dt2
BEDFRIC CT2	1,052	05-03-98 11:54a bedfric.ct2
BEDFRIC DT2	421,648	04-21-98 3:40p bedfric.dt2
4 file(s)		845,400 bytes

Directory of F:\cat\bound

.	<DIR>	05-22-98 10:23a .
..	<DIR>	05-22-98 10:23a ..
CHAN08-6 CT0	1,052	04-19-98 3:12p chan0896PW.ct0
CHAN08-8 DT0	4,800	04-19-98 3:12p chan0896PW.dt0
S96MCN CT1	1,052	05-03-98 12:09p s96Mon.ct1
S96MON DT1	2,253,312	04-16-98 12:05p s96Mon.dt1
4 file(s)		2,260,216 bytes

Directory of F:\cat\Mon96

.	<DIR>	05-22-98 10:23a .
..	<DIR>	05-22-98 10:23a ..
HD CT2	1,052	05-05-98 5:37a hd.ct2
HD DT2	324,668,960	05-05-98 5:37a hd.dt2
HDMAX CT2	1,052	05-22-98 11:01a hdmax.ct2
HDMAX DT2	843,296	05-22-98 11:01a hdmax.dt2
HDMEAN CT2	1,052	05-22-98 11:32a hdmean.ct2
HDMEAN DT2	843,296	05-22-98 11:32a hdmean.dt2
HDMIN CT2	1,052	05-22-98 11:27a hadmin.ct2
HDMIN DT2	843,296	05-22-98 11:27a hadmin.dt2
NEAP96 CT2	1,052	05-05-98 5:37a Neap96.ct2
NEAP96 DT2	126,916,048	05-05-98 3:58a Neap96.dt2

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SIM0996A	CT0	1,052	05-12-98	9:23a	sim0996A.ct0
SIM0996A	DT0	49,216	05-12-98	9:23a	sim0996A.dt0
SIM0996B	CT0	1,052	05-12-98	9:23a	sim0996B.ct0
SIM0996B	DT0	24,608	05-12-98	9:23a	sim0996B.dt0
SPRING96	CT2	1,052	05-05-98	5:37a	Spring96.ct2
SPRING96	DT2	126,916,048	05-04-98	7:02p	Spring96.dt2
		16 file(s)	581,113,184 bytes		

Directory of F:\cat\wind

.	<DIR>		05-22-98	10:23a	.
..	<DIR>		05-22-98	10:23a	..
HATIA0~6	CT0	1,052	04-23-98	12:31p	hatia0996.ct0
HATIA0~8	DT0	1,920	04-23-98	12:31p	hatia0996.dt0
		2 file(s)	2,972 bytes		

Directory of F:\wrkHDmon96

.	<DIR>		05-22-98	10:23a	.
..	<DIR>		05-22-98	10:23a	..
M21HD	INP	5,011	05-03-98	3:17p	m21hd.inp
		1 file(s)	5,011 bytes		

Total files listed:

27 file(s)	584,226,783 bytes
18 dir(s)	0 bytes free

E.6 Contents of CD-ROM MES_DRY97A

Volume in drive F is MES_DRY97A

Volume Serial Number is 9CF3-E5D2

Directory of F:\

CAT	<DIR>	05-21-98	4:07p	cat
WRKHDD~7	<DIR>	05-21-98	4:07p	wrkHDDry97
	0 file(s)		0 bytes	

Directory of F:\cat

.	<DIR>	05-21-98	4:07p	.
..	<DIR>	05-21-98	4:07p	..
BATHY	<DIR>	05-21-98	4:07p	bathy
BOUND	<DIR>	05-21-98	4:07p	bound
DRY97	<DIR>	05-21-98	4:07p	Dry97
WIND	<DIR>	05-21-98	4:07p	wind
	0 file(s)		0 bytes	

Directory of F:\cat\bathy

.	<DIR>	05-21-98	4:07p	.
..	<DIR>	05-21-98	4:07p	..
BATHYFIN CT2	1,052	04-27-98	11:07a	bathyfin.ct2
BATHYFIN DT2	421,648	04-27-98	11:07a	bathyfin.dt2
BEDFRIC CT2	1,052	05-03-98	11:54a	bedfric.ct2
BEDFRIC DT2	421,648	04-21-98	3:40p	bedfric.dt2
	4 file(s)		845,400 bytes	

Directory of F:\cat\bound

.	<DIR>	05-21-98	4:07p	.
..	<DIR>	05-21-98	4:07p	..
CHAN01~6 CT0	1,052	04-19-98	11:11a	Chan0197PW.ct0
CHAN01~8 DT0	11,328	04-19-98	11:11a	Chan0197PW.dt0
S97DRY CT1	1,052	05-03-98	5:36p	s97Dry.ct1
S97DRY DT1	2,145,080	05-03-98	5:36p	s97Dry.dt1
	4 file(s)		2,158,512 bytes	

Directory of F:\cat\Dry97

.	<DIR>	05-21-98	4:07p	.
..	<DIR>	05-21-98	4:07p	..
HD CT2	1,052	05-04-98	8:07p	hd.ct2
HD DT2	324,668,960	05-04-98	8:07p	hd.dt2
HDMAX CT2	1,052	05-22-98	11:11a	hdmax.ct2
HDMAX DT2	843,296	05-22-98	11:11a	hdmax.dt2
HDMEAN CT2	1,052	05-22-98	11:34a	hdmean.ct2
HDMEAN DT2	843,296	05-22-98	11:34a	hdmean.dt2
HDMIN CT2	1,052	05-22-98	11:30a	hadmin.ct2
HDMIN DT2	843,296	05-22-98	11:29a	hadmin.dt2
NEAP97 CT2	1,052	05-04-98	8:07p	Neap97.ct2
NEAP97 DT2	126,916,048	05-04-98	11:08a	Neap97.dt2
SIM0197A CT0	1,052	05-11-98	3:43p	sim0197A.ct0
SIM0197A DT0	49,216	05-11-98	3:43p	sim0197A.dt0

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SIM0197B	CT0	1,052	05-11-98	3:47p	sim0197B.ct0
SIM0197B	DT0	24,608	05-11-98	3:47p	sim0197B.dt0
SPRING97	CT2	1,052	05-04-98	8:07p	Spring97.ct2
SPRING97	DT2	126,916,048	05-04-98	4:25p	Spring97.dt2
		16 file(s)	581,113,184 bytes		

Directory of F:\cat\wind

.	<DIR>		05-21-98	4:07p	.
..	<DIR>		05-21-98	4:07p	..
HATIA0~6	CT0	1,052	04-23-98	12:45p	hatia0197.ct0
HATIA0~8	DT0	1,408	04-23-98	12:45p	hatia0197.dt0
		2 file(s)	2,460 bytes		

Directory of F:\wrkHDDry97

.	<DIR>		05-21-98	4:07p	.
..	<DIR>		05-21-98	4:07p	..
M21HD	INP	5,012	05-03-98	3:49p	m21hd.inp
		1 file(s)	5,012 bytes		

Total files listed:

27 file(s)	584,124,568 bytes
18 dir(s)	0 bytes free

E.7 Contents of CD-ROM MES_MON97A

Volume in drive F is MES_MON97A

Volume Serial Number is 0F9A-8453

Directory of F:\

CAT	<DIR>	05-22-98	4:51p	cat
WRKHDM~7	<DIR>	05-22-98	4:51p	wrkHDmon97
	0 file(s)		0 bytes	

Directory of F:\cat

.	<DIR>	05-22-98	4:51p	.
..	<DIR>	05-22-98	4:51p	..
BATHY	<DIR>	05-22-98	4:51p	bathy
BOUND	<DIR>	05-22-98	4:51p	bound
MON97	<DIR>	05-22-98	4:51p	Mon97
WIND	<DIR>	05-22-98	4:51p	wind
	0 file(s)		0 bytes	

Directory of F:\cat\bathy

.	<DIR>	05-22-98	4:51p	.
..	<DIR>	05-22-98	4:51p	..
BATHYFIN CT2	1,052	04-27-98	11:07a	bathyfin.ct2
BATHYFIN DT2	421,648	04-27-98	11:07a	bathyfin.dt2
BEDFRIC CT2	1,052	05-03-98	11:54a	bedfric.ct2
BEDFRIC DT2	421,648	04-21-98	3:40p	bedfric.dt2
	4 file(s)		845,400 bytes	

Directory of F:\cat\bound

.	<DIR>	05-22-98	4:51p	.
..	<DIR>	05-22-98	4:51p	..
CHAN08~6 CT0	1,052	04-19-98	11:17a	Chan0897PW.ct0
CHAN08~8 DT0	6,352	04-19-98	11:17a	Chan0897PW.dt0
S97MON CT1	1,052	05-03-98	12:09p	s97Mon.ct1
S97MON DT1	3,999,368	04-23-98	5:20p	s97Mon.dt1
	4 file(s)		4,007,824 bytes	

Directory of F:\cat\Mon97

.	<DIR>	05-22-98	4:51p	.
..	<DIR>	05-22-98	4:51p	..
HD CT2	1,052	05-04-98	9:02a	hd.ct2
HD DT2	324,668,960	05-04-98	9:02a	hd.dt2
HDFLNM CT2	1,052	05-26-98	2:52p	hdflNm.ct2
HDFLNM DT2	1,686,592	05-26-98	2:52p	hdflNm.dt2
HDFLNN CT2	1,052	05-26-98	2:52p	hdflNn.ct2
HDFLNN DT2	1,686,592	05-26-98	2:52p	hdflNn.dt2
HDFLSM CT2	1,052	05-26-98	2:52p	hdflSm.ct2
HDFLSM DT2	1,686,592	05-26-98	2:52p	hdflSm.dt2
HDFLSN CT2	1,052	05-26-98	2:52p	hdflSn.ct2
HDFLSN DT2	1,686,592	05-26-98	2:52p	hdflSn.dt2
HDMAX CT2	1,052	05-17-98	4:04p	hdmax.ct2
HDMAX DT2	843,296	05-17-98	4:04p	hdmax.dt2
HDMEAN CT2	1,052	05-22-98	10:23a	hdmean.ct2
HDMEAN DT2	843,296	05-22-98	10:23a	hdmean.dt2

HDMIN	CT2	1,052	05-17-98	4:04p	hdmin.ct2
HDMIN	DT2	843,296	05-17-98	4:04p	hdmin.dt2
NEAP97	CT2	1,052	05-04-98	9:02a	Neap97.ct2
NEAP97	DT2	126,916,048	05-03-98	6:18p	Neap97.dt2
SIM0997A	CT0	1,052	05-11-98	4:36p	sim0997A.ct0
SIM0997A	DT0	49,216	05-11-98	4:36p	sim0997A.dt0
SIM0997B	CT0	1,052	05-11-98	4:37p	sim0997B.ct0
SIM0997B	DT0	24,608	05-11-98	4:37p	sim0997B.dt0
SPRING97	CT2	1,052	05-04-98	9:02a	Spring97.ct2
SPRING97	DT2	126,916,048	05-04-98	2:35a	Spring97.dt2
		24 file(s)	587,863,760 bytes		

Directory of F:\cat\wind

.	<DIR>		05-22-98	4:51p	.
..	<DIR>		05-22-98	4:51p	..
HATIA0~6	CT0	1,052	04-23-98	12:58p	hatia0897.ct0
HATIA0~8	DT0	3,912	04-23-98	12:58p	hatia0897.dt0
		2 file(s)	4,964 bytes		

Directory of F:\wrkHDmon97

.	<DIR>		05-22-98	4:51p	.
..	<DIR>		05-22-98	4:51p	..
M21HD	INP	5,329	05-03-98	3:21p	m21hd.inp
		1 file(s)	5,329 bytes		

Total files listed:

35 file(s)	592,727,277 bytes
18 dir(s)	0 bytes free

E.8 Contents of CD-ROM MES_MON97B

Volume in drive F is MES_MON97B

Volume Serial Number is 3108-0570

Directory of F:\

CAT	<DIR>	05-28-98 12:20p	cat
WRKHDM-7	<DIR>	05-28-98 12:20p	wrkHDmon97
0 file(s)		0 bytes	

Directory of F:\cat

.	<DIR>	05-28-98 12:20p	.
..	<DIR>	05-28-98 12:20p	..
BATHY	<DIR>	05-28-98 12:20p	bathy
BOUND	<DIR>	05-28-98 12:20p	bound
MON97	<DIR>	05-28-98 12:20p	Mon97
WIND	<DIR>	05-28-98 12:20p	wind
0 file(s)		0 bytes	

Directory of F:\cat\bathy

.	<DIR>	05-28-98 12:20p	.
..	<DIR>	05-28-98 12:20p	..
BATHYI13 CT2	1,052	05-24-98 11:13a	bathyI13.ct2
BATHYI13 DT2	421,648	05-24-98 10:16a	bathyI13.dt2
BATHY-10 CT2	1,052	05-24-98 11:04a	bathyIall.ct2
BATHY-12 DT2	421,648	05-24-98 10:27a	bathyIex8.dt2
BATHY-14 CT2	1,052	05-24-98 10:27a	bathyIex8.ct2
BATHY-16 DT2	421,648	05-24-98 11:04a	bathyIall.dt2
BEDFRIC CT2	1,052	05-03-98 11:54a	bedfric.ct2
BEDFRIC DT2	421,648	04-21-98 3:40p	bedfric.dt2
8 file(s)		1,690,800 bytes	

Directory of F:\cat\bound

.	<DIR>	05-28-98 12:20p	.
..	<DIR>	05-28-98 12:20p	..
CHAN08-6 CT0	1,052	04-19-98 11:17a	Chan0897PW.ct0
CHAN08-8 DT0	6,352	04-19-98 11:17a	Chan0897PW.dt0
S97MON CT1	1,052	05-03-98 12:09p	s97Mon.ct1
S97MON DT1	3,999,368	04-23-98 5:20p	s97Mon.dt1
4 file(s)		4,007,824 bytes	

Directory of F:\cat\Mon97

.	<DIR>	05-28-98 12:20p	.
..	<DIR>	05-28-98 12:20p	..
HDFLI1-6 CT2	1,052	05-27-98 2:53p	hdflI13Nn.ct2
HDFLI1-8 DT2	1,686,592	05-27-98 2:52p	hdflI13Nm.dt2
HDFLI-10 CT2	1,052	05-27-98 2:54p	hdflI13Sm.ct2
HDFLI-12 DT2	1,686,592	05-27-98 2:53p	hdflI13Nn.dt2
HDFLI-14 CT2	1,052	05-27-98 2:55p	hdflI13Sn.ct2
HDFLI-16 DT2	1,686,592	05-27-98 2:54p	hdflI13Sm.dt2
HDFLI-18 CT2	1,052	05-27-98 2:52p	hdflI13Nm.ct2
HDFLI-20 DT2	1,686,592	05-27-98 2:55p	hdflI13Sn.dt2
HDFLI-22 CT2	1,052	05-28-98 9:40a	hdflIallNm.ct2
HDFLI-24 DT2	1,686,592	05-28-98 9:40a	hdflIallNm.dt2

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HDFLI~26	CT2	1,052	05-28-98	9:41a	hdflIallNn.ct2
HDFLI~28	DT2	1,686,592	05-28-98	9:41a	hdflIallNn.dt2
HDFLI~30	CT2	1,052	05-28-98	9:42a	hdflIallSm.ct2
HDFLI~32	DT2	1,686,592	05-28-98	9:42a	hdflIallSm.dt2
HDFLI~34	CT2	1,052	05-28-98	9:43a	hdflIallSn.ct2
HDFLI~36	DT2	1,686,592	05-28-98	9:43a	hdflIallSn.dt2
HDFLI~38	CT2	1,052	05-28-98	8:54a	hdflIex8Nm.ct2
HDFLI~40	DT2	1,686,592	05-28-98	8:54a	hdflIex8Nm.dt2
HDFLI~42	CT2	1,052	05-28-98	8:55a	hdflIex8Nn.ct2
HDFLI~44	DT2	1,686,592	05-28-98	8:55a	hdflIex8Nn.dt2
HDFLI~46	CT2	1,052	05-28-98	8:56a	hdflIex8Sm.ct2
HDFLI~48	DT2	1,686,592	05-28-98	8:56a	hdflIex8Sm.dt2
HDFLI~50	CT2	1,052	05-28-98	8:56a	hdflIex8Sn.ct2
HDFLI~52	DT2	1,686,592	05-28-98	8:56a	hdflIex8Sn.dt2
HDI13MAX	CT2	1,052	05-27-98	3:09p	hdI13max.ct2
HDI13MAX	DT2	843,296	05-27-98	3:09p	hdI13max.dt2
HDI13MIN	CT2	1,052	05-27-98	3:27p	hdI13min.ct2
HDI13MIN	DT2	843,296	05-27-98	3:27p	hdI13min.dt2
HDI13TSA	CT0	1,052	05-27-98	3:34p	hdI13tsA.ct0
HDI13TSA	DT0	49,216	05-27-98	3:34p	hdI13tsA.dt0
HDI13TSB	CT0	1,052	05-27-98	3:41p	hdI13tsB.ct0
HDI13TSB	DT0	24,608	05-27-98	3:41p	hdI13tsB.dt0
HDI13~62	CT2	1,052	05-27-98	3:18p	hdI13mean.ct2
HDI13~64	DT2	843,296	05-27-98	3:18p	hdI13mean.dt2
HDIALl	CT2	1,052	05-28-98	5:44a	hdIall.ct2
HDIALl	DT2	324,668,960	05-28-98	5:44a	hdIall.dt2
HDIAL~78	CT0	1,052	05-28-98	10:23a	hdIalltsA.ct0
HDIAL~80	CT2	1,052	05-28-98	9:52a	hdIallmax.ct2
HDIAL~82	DT0	49,216	05-28-98	10:23a	hdIalltsA.dt0
HDIAL~84	DT2	843,296	05-28-98	9:52a	hdIallmax.dt2
HDIAL~86	CT0	1,052	05-28-98	10:30a	hdIalltsB.ct0
HDIAL~88	CT2	1,052	05-28-98	10:04a	hdIallmean.ct2
HDIAL~90	DT0	24,608	05-28-98	10:30a	hdIalltsB.dt0
HDIAL~92	DT2	843,296	05-28-98	10:04a	hdIallmean.dt2
HDIAL~94	CT2	1,052	05-28-98	10:16a	hdIallmin.ct2
HDIAL~96	DT2	843,296	05-28-98	10:16a	hdIallmin.dt2
HDIE~98	CT0	1,052	05-28-98	9:33a	hdIex8tsA.ct0
HDIE~100	CT2	1,052	05-28-98	9:06a	hdIex8max.ct2
HDIE~102	DT0	49,216	05-28-98	9:32a	hdIex8tsA.dt0
HDIE~104	DT2	843,296	05-28-98	9:06a	hdIex8max.dt2
HDIE~106	CT0	1,052	05-28-98	9:39a	hdIex8tsB.ct0
HDIE~108	CT2	1,052	05-28-98	9:16a	hdIex8mean.ct2
HDIE~110	DT0	24,608	05-28-98	9:39a	hdIex8tsB.dt0
HDIE~112	DT2	843,296	05-28-98	9:16a	hdIex8mean.dt2
HDIE~114	CT2	1,052	05-28-98	9:25a	hdIex8min.ct2
HDIE~116	DT2	843,296	05-28-98	9:25a	hdIex8min.dt2
NEAP~118	CT2	1,052	05-28-98	5:44a	Neap97Iall.ct2
NEAP~120	DT2	126,916,048	05-27-98	8:40p	Neap97Iall.dt2
SPR9~122	CT2	1,052	05-28-98	5:44a	Spr97Iall.ct2
SPR9~124	DT2	126,916,048	05-28-98	1:51a	Spr97Iall.dt2
60 file(s) 606,582,856 bytes					

Directory of F:\cat\wind

.	<DIR>	05-28-98 12:20p	.
..	<DIR>	05-28-98 12:20p	..
HATIA0~6	CT0	1,052	04-23-98 12:58p hatia0897.ct0
HATIA0~8	DT0	3,912	04-23-98 12:58p hatia0897.dt0
2 file(s) 4,964 bytes			

Directory of F:\wrkHDmon97

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```
.          <DIR>          05-28-98 12:20p .
..         <DIR>          05-28-98 12:20p ..
M21HDI13 INP          5,044 05-26-98  3:59p m21hdI13.inp
M21HDI~8 INP          5,048 05-26-98  4:02p m21hdIex8.inp
M21HD~10 INP          5,033 05-26-98  4:04p m21hdIall.inp
          3 file(s)          15,125 bytes
```

Total files listed:

```
77 file(s)      612,301,569 bytes
18 dir(s)              0 bytes free
```

E.9 Contents of CD-ROM MES_SALI

Volume in drive F is MES_SALI

Volume Serial Number is 3B40-EEDE

Directory of F:\

CAT	<DIR>	05-27-98 11:54a	cat
WRKAD	<DIR>	05-27-98 11:54a	wrkAD
0 file(s)		0 bytes	

Directory of F:\cat

.	<DIR>	05-27-98 11:54a	.
..	<DIR>	05-27-98 11:54a	..
BATHY	<DIR>	05-27-98 11:54a	bathy
BOUND	<DIR>	05-27-98 11:54a	bound
SALI	<DIR>	05-27-98 11:54a	sali
WIND	<DIR>	05-27-98 11:54a	wind
0 file(s)		0 bytes	

Directory of F:\cat\bathy

.	<DIR>	05-27-98 11:54a	.
..	<DIR>	05-27-98 11:54a	..
BATHYFIN CT2	1,052	04-27-98 11:07a	bathyfin.ct2
BATHYFIN DT2	421,648	04-27-98 11:07a	bathyfin.dt2
BATHY~10 CT2	1,052	05-24-98 11:04a	bathyIall.ct2
BATHY~12 DT2	421,648	05-24-98 11:04a	bathyIall.dt2
BEDFRIC CT2	1,052	05-03-98 11:54a	bedfric.ct2
BEDFRIC DT2	421,648	04-21-98 3:40p	bedfric.dt2
6 file(s)		1,268,100 bytes	

Directory of F:\cat\bound

.	<DIR>	05-27-98 11:54a	.
..	<DIR>	05-27-98 11:54a	..
CHAN02~6 CT0	1,052	04-19-98 11:03a	chan0296PW.ct0
CHAN02~8 DT0	76,640	04-19-98 11:03a	chan0296PW.dt0
S96DRY CT1	1,052	05-03-98 12:08p	s96Dry.ct1
S96DRY DT1	2,129,432	03-07-98 12:11p	s96Dry.dt1
4 file(s)		2,208,176 bytes	

Directory of F:\cat\sali

.	<DIR>	05-27-98 11:54a	.
..	<DIR>	05-27-98 11:54a	..
AD CT2	1,052	05-27-98 4:04a	ad.ct2
AD DT2	324,668,960	05-27-98 4:04a	ad.dt2
AD0296A CT0	1,052	05-27-98 8:53a	ad0296A.ct0
AD0296A DT0	49,216	05-27-98 8:53a	ad0296A.dt0
AD0296B CT0	1,052	05-27-98 9:01a	ad0296B.ct0
AD0296B DT0	24,608	05-27-98 9:01a	ad0296B.dt0
ADI0296A CT0	1,052	05-26-98 11:33a	adi0296A.ct0
ADI0296A DT0	22,272	05-26-98 11:32a	adi0296A.dt0

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ADI0296B	CT0	1,052	05-26-98	11:38a	adI0296B.ct0
ADI0296B	DT0	11,136	05-26-98	11:38a	adI0296B.dt0
ADIALl	CT2	1,052	05-26-98	7:52a	adIall.ct2
ADIALl	DT2	147,155,152	05-26-98	7:52a	adIall.dt2
ADIMAX	CT2	1,052	05-26-98	9:00a	adImax.ct2
ADIMAX	DT2	843,296	05-26-98	9:00a	adImax.dt2
ADIMEAN	CT2	1,052	05-26-98	9:11a	adImean.ct2
ADIMEAN	DT2	843,296	05-26-98	9:11a	adImean.dt2
ADIMIN	CT2	1,052	05-26-98	9:06a	adImin.ct2
ADIMIN	DT2	843,296	05-26-98	9:06a	adImin.dt2
ADMAX	CT2	1,052	05-27-98	9:11a	admax.ct2
ADMAX	DT2	843,296	05-27-98	9:11a	admax.dt2
ADMEAN	CT2	1,052	05-27-98	9:18a	admean.ct2
ADMEAN	DT2	843,296	05-27-98	9:18a	admean.dt2
ADMIN	CT2	1,052	05-27-98	9:15a	admin.ct2
ADMIN	DT2	843,296	05-27-98	9:15a	admin.dt2
HD0296A	CT0	1,052	05-27-98	9:04a	hd0296A.ct0
HD0296A	DT0	22,272	05-27-98	9:04a	hd0296A.dt0
HD0296B	CT0	1,052	05-27-98	9:08a	hd0296B.ct0
HD0296B	DT0	11,136	05-27-98	9:08a	hd0296B.dt0
HDDIFF	CT2	1,052	05-27-98	10:23a	hddiff.ct2
HDDIFF	DT2	421,648	05-27-98	10:23a	hddiff.dt2
HDIO296A	CT0	1,052	05-26-98	11:42a	hdIO296A.ct0
HDIO296A	DT0	22,272	05-26-98	11:42a	hdIO296A.dt0
HDIO296B	CT0	1,052	05-26-98	11:43a	hdIO296B.ct0
HDIO296B	DT0	11,136	05-26-98	11:43a	hdIO296B.dt0
HDIDIFF	CT2	1,052	05-26-98	6:11p	hdIdiff.ct2
HDIDIFF	DT2	421,648	05-26-98	6:11p	hdIdiff.dt2
HDIMAX	CT2	1,052	05-26-98	10:52a	hdImax.ct2
HDIMAX	DT2	843,296	05-26-98	10:52a	hdImax.dt2
HDIMEAN	CT2	1,052	05-26-98	10:55a	hdImean.ct2
HDIMEAN	DT2	843,296	05-26-98	10:55a	hdImean.dt2
HDIMIN	CT2	1,052	05-26-98	10:58a	hdImin.ct2
HDIMIN	DT2	843,296	05-26-98	10:58a	hdImin.dt2
HDSMAX	CT2	1,052	05-27-98	9:26a	hdSmax.ct2
HDSMAX	DT2	843,296	05-27-98	9:26a	hdSmax.dt2
HDSMEAN	CT2	1,052	05-27-98	9:30a	hdSmean.ct2
HDSMEAN	DT2	843,296	05-27-98	9:30a	hdSmean.dt2
HDSMIN	CT2	1,052	05-27-98	9:22a	hdSmin.ct2
HDSMIN	DT2	843,296	05-27-98	9:22a	hdSmin.dt2
HDXMAX	CT2	1,052	05-25-98	1:21p	hdXmax.ct2
HDXMAX	DT2	843,296	05-25-98	1:21p	hdXmax.dt2
HDXMEAN	CT2	1,052	05-25-98	1:43p	hdXmean.ct2
HDXMEAN	DT2	843,296	05-25-98	1:43p	hdXmean.dt2
HDXMIN	CT2	1,052	05-25-98	1:31p	hdXmin.ct2
HDXMIN	DT2	843,296	05-25-98	1:31p	hdXmin.dt2
HDYMAX	CT2	1,052	05-26-98	11:11a	hdYmax.ct2
HDYMAX	DT2	843,296	05-26-98	11:11a	hdYmax.dt2
HDYMEAN	CT2	1,052	05-26-98	11:18a	hdYmean.ct2
HDYMEAN	DT2	843,296	05-26-98	11:18a	hdYmean.dt2
HDYMIN	CT2	1,052	05-26-98	11:25a	hdYmin.ct2
HDYMIN	DT2	843,296	05-26-98	11:25a	hdYmin.dt2
SALIINI	CT2	1,052	05-05-98	6:36p	saliini.ct2
SALIINI	DT2	421,648	05-05-98	6:36p	saliini.dt2
SBND	CT1	1,052	05-18-98	11:38a	sbnd.ct1
SBND	DT1	2,608	05-05-98	6:30p	sbnd.dt1

64 file(s) 488,478,704 bytes

Directory of F:\cat\wind

<DIR> 05-27-98 11:54a .

```
..          <DIR>          05-27-98 11:54a ..
HATIA0~6 CT0          1,052 04-23-98 12:37p hatia0296.ct0
HATIA0~8 DT0          1,792 04-23-98 12:37p hatia0296.dt0
      2 file(s)          2,844 bytes
```

Directory of F:\wrkAD

```
.          <DIR>          05-27-98 11:54a .
..          <DIR>          05-27-98 11:54a ..
M21AD      INP          6,818 05-26-98 12:06p m21ad.inp
M21ADI~8 INP          6,852 05-25-98 4:54p m21adIall.inp
      2 file(s)          13,670 bytes
```

Total files listed:

78 file(s)	491,971,494 bytes
18 dir(s)	0 bytes free

E.10 Contents of CD-ROM MES_OTHER

Volume in drive F is MES_OTHER

Volume Serial Number is 904C-4115

Directory of F:\

BATHYRAW	<DIR>	06-01-98	4:33p	bathyraw
CAT	<DIR>	06-01-98	4:33p	cat
SOURCE	<DIR>	06-01-98	4:33p	source
WORKNZ	<DIR>	06-01-98	4:33p	workNZ
WRKNSW	<DIR>	06-01-98	4:33p	wrkNSW
WRKST	<DIR>	06-01-98	4:33p	wrkST
0 file(s)		0 bytes		

Directory of F:\bathyraw

.	<DIR>	06-01-98	4:33p	.
..	<DIR>	06-01-98	4:33p	..
C18294	XYZ	7,727	10-30-97	3:26p c18294.xyz
C186_95	XYZ	37,768	11-16-97	12:11p c186_95.xyz
E169_96	XYZ	26,207	10-13-97	7:19p e169_96.xyz
ED182BP	XYZ	8,064	11-02-97	4:14p ed182bp.xyz
ED_14994	XYZ	6,615	10-28-97	9:16a ed_14994.xyz
MES200	XYZ	21,361,536	03-16-98	5:08p mes200.xyz
NIZ97	XYZ	12,988	03-16-98	12:00p niz97.xyz
ORIKMS	XYZ	69,116,892	02-12-98	3:21p orikms.xyz
WATER0	XYZ	2,370,816	03-16-98	2:17p water0.xyz
9 file(s)		92,948,613 bytes		

Directory of F:\cat

.	<DIR>	06-01-98	4:33p	.
..	<DIR>	06-01-98	4:33p	..
BATHY	<DIR>	06-01-98	4:33p	bathy
BATHYRAW	<DIR>	06-01-98	4:33p	bathyraw
BATLOC	<DIR>	06-01-98	4:33p	batLoc
BNDLOC	<DIR>	06-01-98	4:33p	bndLoc
MEAS0296	<DIR>	06-01-98	4:33p	meas0296
MEAS0297	<DIR>	06-01-98	4:33p	meas0297
MEAS0996	<DIR>	06-01-98	4:33p	meas0996
MEAS0997	<DIR>	06-01-98	4:33p	meas0997
MESWL	<DIR>	06-01-98	4:33p	meswl
SEDI	<DIR>	06-01-98	4:33p	sedi
TIDE0296	<DIR>	06-01-98	4:33p	tide0296
TIDE0297	<DIR>	06-01-98	4:33p	tide0297
TIDE0996	<DIR>	06-01-98	4:33p	tide0996
TIDE0997	<DIR>	06-01-98	4:33p	tide0997
WAVES	<DIR>	06-01-98	4:33p	waves
0 file(s)		0 bytes		

Directory of F:\cat\bathy


```

.          <DIR>          06-01-98  4:33p  .
..         <DIR>          06-01-98  4:33p  ..
BAT-MES   CT2             1,052  04-27-98 10:46a bat-MES.ct2
BAT-MES   DT2            421,648  04-27-98  9:58a bat-MES.dt2
BAT-NIZ   CT2             1,052  04-27-98 10:37a bat-niz.ct2
BAT-NIZ   DT2            421,648  04-27-98 10:37a bat-niz.dt2
BATHYBND  CT2             1,052  03-04-98  3:30p bathybnd.ct2
BATHYBND  DT2            421,648  03-04-98  3:30p bathybnd.dt2
BATHYFIN  CT2             1,052  04-27-98 11:07a bathyfin.ct2
BATHYFIN  DT2            421,648  04-27-98 11:07a bathyfin.dt2
BATHYNSW  CT2             1,052  05-04-98  9:29a bathyNSW.ct2
BATHYNSW  DT2           1,682,260  05-04-98  9:29a bathyNSW.dt2
BEDFRIC   CT2             1,052  05-03-98 11:54a bedfric.ct2
BEDFRIC   DT2            421,648  04-21-98  3:40p bedfric.dt2
FINAL~30  CT2             1,052  03-07-98 12:08p finaldhul.ct2
FINAL~32  DT2            421,648  03-07-98 12:08p finaldhul.dt2
14 file(s)          4,219,512 bytes

```

Directory of F:\cat\bathyraw

```

.          <DIR>          06-01-98  4:33p  .
..         <DIR>          06-01-98  4:33p  ..
BAT-CSPS  CT2             1,052  02-22-98  5:03p bat-csps.ct2
BAT-CSPS  DT2            490,960  02-22-98  5:03p bat-csps.dt2
BAT-KMS   CT2             1,052  03-12-98  5:10p bat-kms.ct2
BAT-KMS   DT2            516,952  03-12-98  5:10p bat-kms.dt2
BAT-LAND  CT2             1,052  02-22-98  4:49p bat-land.ct2
BAT-LAND  DT2            421,648  02-22-98  4:49p bat-land.dt2
BAT-SPOT  CT2             1,052  05-18-98 11:44a bat-spot.ct2
BAT-SPOT  DT2            503,956  05-18-98 11:44a bat-spot.dt2
BIWTA~22  CT2             1,052  02-19-98 11:10a biwta_pwd.ct2
BIWTA~24  DT2            503,956  02-19-98 11:10a biwta_pwd.dt2
10 file(s)          2,442,732 bytes

```

Directory of F:\cat\batLoc

```

.          <DIR>          06-01-98  4:33p  .
..         <DIR>          06-01-98  4:33p  ..
BATHYLOC  CT2             1,052  05-30-98 10:37a bathyLoc.ct2
BATHYLOC  DT2            84,056  05-26-98  9:24a bathyLoc.dt2
BATILOC   CT2             1,052  05-30-98 10:36a batILoc.ct2
BATILOC   DT2            84,056  05-27-98  5:40p batILoc.dt2
BATIL~14  CT2             1,052  06-02-98 10:06a batILoc13.ct2
BATIL~16  DT2            84,056  06-02-98 10:06a batILoc13.dt2
BEDFRIC   CT2             1,052  05-19-98  3:21p bedfric.ct2
BEDFRIC   DT2            84,056  05-19-98  3:21p bedfric.dt2
HDFLI~22  CT2             1,052  06-04-98 12:04p hdfliI13Sn.ct2
HDFLI~24  DT2           336,224  06-04-98 12:03p hdfliI13Sm.dt2
HDFLI~26  CT2             1,052  06-04-98 12:03p hdfliI13Sm.ct2
HDFLI~28  DT2           336,224  06-04-98 12:04p hdfliI13Sn.dt2
HDFLI~30  CT2             1,052  05-30-98  3:14p hdfliIallSn.ct2
HDFLI~32  DT2           336,224  05-30-98  3:13p hdfliIallSm.dt2
HDFLI~34  CT2             1,052  05-30-98  3:13p hdfliIallSm.ct2
HDFLI~36  DT2           336,224  05-30-98  3:14p hdfliIallSn.dt2
HDFLSM    CT2             1,052  05-30-98  3:09p hdf1Sm.ct2
HDFLSM    DT2           336,224  05-30-98  3:09p hdf1Sm.dt2
HDFLSN    CT2             1,052  05-30-98  3:10p hdf1Sn.ct2
HDFLSN    DT2           336,224  05-30-98  3:10p hdf1Sn.dt2
HDNZ      CT2             1,052  05-30-98 10:13a hdnZ.ct2
HDNZ      DT2          25,300,856  05-27-98  9:12p hdnZ.dt2
HDNZI13   CT2             1,052  06-03-98  7:03p hdnZI13.ct2

```

```

DHU0296C CT0      1,052  05-14-98 11:55a dhu0296C.ct0
DHU0296C DT0      5,568  05-14-98 11:55a dhu0296C.dt0
K100296C CT0      1,052  05-13-98  3:23p k100296C.ct0
K100296C DT0      2,780  05-13-98  3:23p k100296C.dt0
KHE0296C CT0      1,052  05-14-98  4:08p khe0296C.ct0
KHE0296C DT0      5,564  05-14-98  4:08p khe0296C.dt0
KOCHO~38 CT0      1,052  05-14-98 11:32a Kocho0296C.ct0
KOCHO~40 DT0      6,000  05-14-98 11:32a Kocho0296C.dt0
RAM0296C CT0      1,052  05-13-98  3:28p ram0296C.ct0
RAM0296C DT0      5,568  05-13-98  3:28p ram0296C.dt0
SAN0296C CT0      1,052  03-08-98  9:42a san0296C.ct0
SAN0296C DT0      5,568  03-08-98  9:42a san0296C.dt0
    22 file(s)          136,428 bytes

```

Directory of F:\cat\meas0297

```

.          <DIR>          06-01-98  4:33p .
..         <DIR>          06-01-98  4:33p ..
CHAND0~6 CT0      1,052  04-20-98  2:36p Chand0197C.ct0
CHAND0~8 DT0     11,328  04-20-98  2:36p Chand0197C.dt0
CHANG~10 CT0      1,052  05-13-98 11:17a Chang0197C.ct0
CHANG~12 DT0     11,328  05-13-98 11:17a Chang0197C.dt0
CHIT0~14 CT0      1,052  05-13-98 11:18a Chit0197C.ct0
CHIT0~16 DT0     11,328  05-13-98 11:18a Chit0197C.dt0
DAS0197C CT0      1,052  05-13-98 11:19a Das0197C.ct0
DAS0197C DT0     11,324  05-13-98 11:19a Das0197C.dt0
DAU0197C CT0      1,052  05-13-98 11:26a Dau0197C.ct0
DAU0197C DT0       440  05-13-98 11:26a Dau0197C.dt0
DHULI~26 CT0      1,052  05-14-98  1:10p Dhuli0197C.ct0
DHULI~28 DT0     11,332  05-14-98  1:10p Dhuli0197C.dt0
KH100~30 CT0      1,052  05-13-98 12:00p Kh100197C.ct0
KH100~32 DT0      5,664  05-13-98 12:00p Kh100197C.dt0
KHEP0~34 CT0      1,052  05-14-98  4:06p Khep0197C.ct0
KHEP0~36 DT0     11,328  05-14-98  4:06p Khep0197C.dt0
KOCHO~38 CT0      1,052  05-14-98 12:46p Koch0197C.ct0
KOCHO~40 DT0      5,664  05-14-98 12:46p Koch0197C.dt0
RAMDA~42 CT0      1,052  05-13-98 11:32a Ramda0197C.ct0
RAMDA~44 DT0     11,328  05-13-98 11:32a Ramda0197C.dt0
SAND0~46 CT0      1,052  05-14-98 12:27p Sand0197C.ct0
SAND0~48 DT0     11,328  05-14-98 12:27p Sand0197C.dt0
    22 file(s)          113,964 bytes

```

Directory of F:\cat\meas0996

```

.          <DIR>          06-01-98  4:33p .
..         <DIR>          06-01-98  4:33p ..
0809CH~6 CT0      1,052  05-14-98  9:35a 0809Char96.ct0
0809CH~8 DT0      3,188  05-14-98  9:35a 0809Char96.dt0
CHAR0~10 CT0      1,052  05-14-98  9:39a Char0996C.ct0
CHAR0~12 DT0      3,188  05-14-98  9:39a Char0996C.dt0
CHIT0~14 CT0      1,052  05-14-98  9:44a Chit0996C.ct0
CHIT0~16 DT0      3,072  05-14-98  9:44a Chit0996C.dt0
DAS0996C CT0      1,052  05-14-98  9:46a Das0996C.ct0
DAS0996C DT0      3,072  05-14-98  9:46a Das0996C.dt0
DAUL0~22 CT0      1,052  05-14-98 12:14p Daul0996C.ct0
DAUL0~24 DT0       800  05-14-98 12:14p Daul0996C.dt0
DHUL0~26 CT0      1,052  05-14-98 10:44a Dhul0996C.ct0
DHUL0~28 DT0      3,072  05-14-98 10:44a Dhul0996C.dt0
KH100~30 CT0      1,052  05-14-98  2:57p kh100996C.ct0
KH100~32 DT0      2,784  05-14-98  2:57p kh100996C.dt0
KHEP0~34 CT0      1,052  05-14-98  4:04p Khep0996C.ct0

```

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KHEP0~36 DT0	3,072	05-14-98	4:04p	Khep0996C.dt0
KOCH0~38 CT0	1,052	05-16-98	2:44p	Koch0996C.ct0
KOCH0~40 DT0	2,784	05-16-98	2:44p	Koch0996C.dt0
RAM0996C CT0	1,052	05-14-98	10:54a	Ram0996C.ct0
RAM0996C DT0	3,072	05-14-98	10:54a	Ram0996C.dt0
SAND0~46 CT0	1,052	05-14-98	11:13a	Sand0996C.ct0
SAND0~48 DT0	3,072	05-14-98	11:18a	Sand0996C.dt0
22 file(s)		42,748 bytes		

Directory of F:\cat\meas0997

.	<DIR>	06-01-98	4:33p	.
..	<DIR>	06-01-98	4:33p	..
CHAND0~6 CT0	1,052	04-26-98	9:07a	Chand0897.ct0
CHAND0~8 DT0	11,712	04-26-98	9:07a	Chand0897.dt0
CHANG~10 CT0	1,052	05-13-98	3:00p	Chang0997C.ct0
CHANG~12 DT0	11,712	05-13-98	3:00p	Chang0997C.dt0
CHIT0~14 CT0	1,052	05-13-98	2:58p	Chit0997C.ct0
CHIT0~16 DT0	11,712	05-13-98	2:58p	Chit0997C.dt0
DAS0997C CT0	1,052	05-13-98	2:34p	Das0997C.ct0
DAS0997C DT0	11,712	05-13-98	2:34p	Das0997C.dt0
DAU0997C CT0	1,052	05-13-98	2:48p	Dau0997C.ct0
DAU0997C DT0	1,088	05-13-98	2:48p	Dau0997C.dt0
DHULI~26 CT0	1,052	05-14-98	1:41p	Dhuli0997C.ct0
DHULI~28 DT0	11,712	05-14-98	1:41p	Dhuli0997C.dt0
K100997C CT0	1,052	05-13-98	2:31p	K100997C.ct0
K100997C DT0	5,856	05-13-98	2:31p	K100997C.dt0
KHEP0~34 CT0	1,052	05-14-98	4:06p	Khep0997C.ct0
KHEP0~36 DT0	11,712	05-14-98	4:06p	Khep0997C.dt0
RAM0997C CT0	1,052	05-13-98	2:44p	Ram0997C.ct0
RAM0997C DT0	11,712	05-13-98	2:44p	Ram0997C.dt0
SAND0~42 CT0	1,052	05-14-98	1:54p	Sand0997C.ct0
SAND0~44 DT0	11,712	05-14-98	1:54p	Sand0997C.dt0
20 file(s)		111,160 bytes		

Directory of F:\cat\meswl

.	<DIR>	06-01-98	4:33p	.
..	<DIR>	06-01-98	4:33p	..
MES1C CT0	1,052	05-13-98	12:34p	mes1C.ct0
MES1C DT0	6,612	05-13-98	12:34p	mes1C.dt0
MES2C CT0	1,052	05-13-98	12:47p	mes2C.ct0
MES2C DT0	4,748	05-13-98	12:47p	mes2C.dt0
MES4C CT0	1,052	05-13-98	12:48p	mes4C.ct0
MES4C DT0	6,044	05-13-98	12:48p	mes4C.dt0
MES5C CT0	1,052	05-13-98	12:51p	mes5C.ct0
MES5C DT0	6,124	05-13-98	12:51p	mes5C.dt0
MES6C CT0	1,052	05-13-98	12:52p	mes6C.ct0
MES6C DT0	5,812	05-13-98	12:52p	mes6C.dt0
SEC CT0	1,052	05-13-98	12:53p	seC.ct0
SEC DT0	4,596	05-13-98	12:53p	seC.dt0
12 file(s)		40,248 bytes		

Directory of F:\cat\sedi

.	<DIR>	06-01-98	4:33p	.
..	<DIR>	06-01-98	4:33p	..
DRYSNN~6 CT2	1,052	05-28-98	3:56p	drySNnowT.ct2
DRYSNN~8 DT2	1,686,592	05-28-98	3:56p	drySNnowT.dt2
DRYSP~10 CT2	1,052	05-28-98	4:33p	drySPnowT.ct2
DRYSP~12 DT2	1,686,592	05-28-98	4:33p	drySPnowT.dt2

MONSN-14	CT2	1,052	05-28-98	7:18p	monSNnowT.ct2
MONSN-16	DT2	1,686,592	05-28-98	7:18p	monSNnowT.dt2
MONSN-18	CT2	1,052	05-28-98	5:48p	monSNSseT.ct2
MONSN-20	DT2	1,686,592	05-28-98	5:48p	monSNSseT.dt2
MONSN-22	CT2	1,052	05-28-98	4:56p	monSNsswT.ct2
MONSN-24	DT2	1,686,592	05-28-98	4:56p	monSNsswT.dt2
MONSP-26	CT2	1,052	05-16-98	6:01p	monSPnowT.ct2
MONSP-28	DT2	1,686,592	05-16-98	6:01p	monSPnowT.dt2
MONSP-30	CT2	1,052	05-16-98	5:02p	monSPsseT.ct2
MONSP-32	DT2	1,686,592	05-16-98	12:37p	monSPsswT.dt2
MONSP-34	CT2	1,052	05-16-98	12:37p	monSPsswT.ct2
MONSP-36	DT2	1,686,592	05-16-98	5:02p	monSPsseT.dt2
		16 file(s)	13,501,152 bytes		

Directory of F:\cat\tide0296

.	<DIR>		06-01-98	4:33p	.
..	<DIR>		06-01-98	4:33p	..
4502N	CT0	1,052	05-31-98	8:57a	4502N.ct0
4502N	DT0	11,524	05-31-98	8:57a	4502N.dt0
4503N	CT0	1,052	05-31-98	9:23a	4503N.ct0
4503N	DT0	11,524	05-31-98	9:23a	4503N.dt0
4506N	CT0	1,052	05-31-98	9:14a	4506N.ct0
4506N	DT0	11,524	05-31-98	9:14a	4506N.dt0
4507AN	CT0	1,052	05-31-98	9:24a	4507aN.ct0
4507AN	DT0	11,524	05-31-98	9:24a	4507aN.dt0
4507C	CT0	1,052	05-31-98	12:37p	4507C.ct0
4507C	DT0	11,524	05-31-98	12:37p	4507C.dt0
4510N	CT0	1,052	05-31-98	9:20a	4510N.ct0
4510N	DT0	11,524	05-31-98	9:20a	4510N.dt0
4511N	CT0	1,052	05-31-98	9:16a	4511N.ct0
4511N	DT0	11,524	05-31-98	9:16a	4511N.dt0
4514N	CT0	1,052	05-31-98	9:18a	4514N.ct0
4514N	DT0	11,524	05-31-98	9:18a	4514N.dt0
		16 file(s)	100,608 bytes		

Directory of F:\cat\tide0297

.	<DIR>		06-01-98	4:33p	.
..	<DIR>		06-01-98	4:33p	..
4502N	CT0	1,052	05-31-98	10:24a	4502N.ct0
4502N	DT0	1,924	05-31-98	10:24a	4502N.dt0
4503N	CT0	1,052	05-31-98	10:37a	4503N.ct0
4503N	DT0	1,924	05-31-98	10:37a	4503N.dt0
4506N	CT0	1,052	05-31-98	10:27a	4506N.ct0
4506N	DT0	1,924	05-31-98	10:27a	4506N.dt0
4507AN	CT0	1,052	05-31-98	10:38a	4507aN.ct0
4507AN	DT0	1,924	05-31-98	10:38a	4507aN.dt0
4507C	CT0	1,052	05-31-98	12:38p	4507C.ct0
4507C	DT0	1,924	05-31-98	12:38p	4507C.dt0
4510N	CT0	1,052	05-31-98	10:36a	4510N.ct0
4510N	DT0	1,924	05-31-98	10:36a	4510N.dt0
4511N	CT0	1,052	05-31-98	10:34a	4511N.ct0
4511N	DT0	1,924	05-31-98	10:34a	4511N.dt0
4514N	CT0	1,052	05-31-98	10:35a	4514N.ct0
4514N	DT0	1,924	05-31-98	10:35a	4514N.dt0
		16 file(s)	23,808 bytes		

Directory of F:\cat\tide0996

.	<DIR>		06-01-98	4:33p	.
---	-------	--	----------	-------	---

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<DIR>          06-01-98  4:33p  ..
4502N  CT0      1,052  05-31-98  9:53a 4502N.ct0
4502N  DT0      3,076  05-31-98  9:53a 4502N.dt0
4503N  CT0      1,052  05-31-98 10:00a 4503N.ct0
4503N  DT0      3,076  05-31-98 10:00a 4503N.dt0
4506N  CT0      1,052  05-31-98  9:54a 4506N.ct0
4506N  DT0      2,884  05-31-98  9:54a 4506N.dt0
4507AN CT0      1,052  05-31-98 10:02a 4507aN.ct0
4507AN DT0      2,884  05-31-98 10:02a 4507aN.dt0
4507C  CT0      1,052  05-31-98 10:00a 4507C.ct0
4507C  DT0      2,884  05-31-98 10:00a 4507C.dt0
4510N  CT0      1,052  05-31-98  9:59a 4510N.ct0
4510N  DT0      2,884  05-31-98  9:59a 4510N.dt0
4511N  CT0      1,052  05-31-98  9:55a 4511N.ct0
4511N  DT0      2,884  05-31-98  9:55a 4511N.dt0
4514N  CT0      1,052  05-31-98  9:57a 4514N.ct0
4514N  DT0      1,540  05-31-98  9:57a 4514N.dt0
16 file(s)          30,528 bytes

```

Directory of F:\cat\tide0997

```

<DIR>          06-01-98  4:33p  .
..             <DIR>          06-01-98  4:33p  ..
4502N  CT0      1,052  05-31-98 10:40a 4502N.ct0
4502N  DT0      2,500  05-31-98 10:40a 4502N.dt0
4503N  CT0      1,052  05-31-98 10:44a 4503N.ct0
4503N  DT0      2,500  05-31-98 10:44a 4503N.dt0
4506N  CT0      1,052  05-31-98 10:41a 4506N.ct0
4506N  DT0      2,500  05-31-98 10:41a 4506N.dt0
4507AN CT0      1,052  05-31-98 10:46a 4507aN.ct0
4507AN DT0      2,500  05-31-98 10:46a 4507aN.dt0
4507C  CT0      1,052  05-31-98 12:33p 4507C.ct0
4507C  DT0      2,500  05-31-98 12:33p 4507C.dt0
4510N  CT0      1,052  05-31-98 10:44a 4510N.ct0
4510N  DT0      2,500  05-31-98 10:44a 4510N.dt0
4511N  CT0      1,052  05-31-98 10:42a 4511N.ct0
4511N  DT0      2,500  05-31-98 10:42a 4511N.dt0
4514N  CT0      1,052  05-31-98 10:43a 4514N.ct0
4514N  DT0      2,500  05-31-98 10:43a 4514N.dt0
16 file(s)          28,416 bytes

```

Directory of F:\cat\waves

```

<DIR>          06-01-98  4:33p  .
..             <DIR>          06-01-98  4:33p  ..
BND157 CT1      1,052  05-04-98 10:48a bnd157.ct1
BND157 DT1      7,220  05-04-98 10:48a bnd157.dt1
BND202 CT1      1,052  05-04-98 10:49a bnd202.ct1
BND202 DT1      7,220  05-04-98 10:49a bnd202.dt1
HDMEA~14 CT2      1,052  05-04-98  9:21a hdmeanNSW.ct2
HDMEA~16 DT2    3,364,520 05-04-98  9:21a hdmeanNSW.dt2
NOW0T  CT2      1,052  05-16-98  4:11p now0t.ct2
NOW0T  DT2    2,951,536 05-16-98  4:11p now0t.dt2
NOW0TN96 CT2      1,052  05-28-98  2:21p now0tN96.ct2
NOW0TN96 DT2    2,951,536 05-28-98  2:19p now0tN96.dt2
NOW0TN97 CT2      1,052  05-28-98  2:21p now0tN97.ct2
NOW0TN97 DT2    2,951,536 05-28-98  2:16p now0tN97.dt2
NOW0TS96 CT2      1,052  05-28-98  2:22p now0tS96.ct2
NOW0TS96 DT2    2,951,536 05-28-98  2:19p now0tS96.dt2
SSE8   CT2      1,052  05-04-98 11:26a sse8.ct2
SSE8   DT2    2,951,536 05-04-98 11:26a sse8.dt2

```

```

SSE8T      CT2      1,052  05-05-98  8:38a  sse8t.ct2
SSE8T      DT2      2,951,536  05-04-98  11:42a  sse8t.dt2
SSE8TN97   CT2      1,052  05-28-98  2:22p  sse8tN97.ct2
SSE8TN97   DT2      2,951,536  05-28-98  2:17p  sse8tN97.dt2
SSW8       CT2      1,052  05-04-98  11:11a  ssw8.ct2
SSW8       DT2      2,951,536  05-04-98  11:11a  ssw8.dt2
SSW8T      CT2      1,052  05-05-98  8:38a  ssw8t.ct2
SSW8T      DT2      2,951,536  05-04-98  11:19a  ssw8t.dt2
SSW8TN97   CT2      1,052  05-28-98  2:23p  ssw8tN97.ct2
SSW8TN97   DT2      2,951,536  05-28-98  2:18p  ssw8tN97.dt2
          26 file(s)      32,907,996 bytes

```

Directory of F:\source

```

.           <DIR>      06-01-98  4:33p  .
..          <DIR>      06-01-98  4:33p  ..
HDFLOW      <DIR>      06-01-98  4:33p  hdfLOW
HTMBND      <DIR>      06-01-98  4:33p  htmbnd
          0 file(s)      0 bytes

```

Directory of F:\source\hdfLOW

```

.           <DIR>      06-01-98  4:33p  .
..          <DIR>      06-01-98  4:33p  ..
CAT         CHC      2,754  03-05-98  10:57a  cat.chc
CHCMEM      I        513  03-05-98  10:57a  chcmem.i
CMPUTE      F      4,074  05-16-98  2:08p  cmpute.f
HDFLOW      F      3,727  05-13-98  11:25a  hdfLOW.f
HDFLOW      I      1,119  03-05-98  12:38p  hdfLOW.i
HPQ2UV      F      1,438  05-13-98  11:36a  hpq2uv.f
INPUT       F      4,365  05-13-98  11:23a  input.f
MAKEFILE    745      05-13-98  10:34a  makefile
PRO         INC      319  03-05-98  10:57a  pro.inc
          9 file(s)      19,054 bytes

```

Directory of F:\source\htmbnd

```

.           <DIR>      06-01-98  4:33p  .
..          <DIR>      06-01-98  4:33p  ..
HTMBND      F      1,715  05-04-98  10:36a  htmbnd.f
          1 file(s)      1,715 bytes

```

Directory of F:\workNZ

```

.           <DIR>      06-01-98  4:33p  .
..          <DIR>      06-01-98  4:33p  ..
HDFLI1~6   INP      297  06-04-98  12:03p  hdfLI13Sn.inp
HDFLI1~8   INP      296  06-04-98  12:02p  hdfLI13Sm.inp
M21HDI13   INP      4,082  06-04-98  12:22p  m21hdi13.inp
M21HDSF    INP      4,050  05-30-98  10:17a  m21hdsf.inp
M21HD~12   INP      4,081  05-30-98  10:18a  m21hdi1all.inp
M21TRN-E   INP      566  05-19-98  1:33p  m21trn-e.inp
M21TRN-S   INP      569  05-19-98  3:19p  m21trn-s.inp
M21TR~20   INP      565  05-19-98  2:46p  m21trn-w2.inp
M21TR~22   INP      576  05-28-98  11:30a  m21trn-Ie.inp
M21TR~24   INP      582  05-27-98  5:04p  m21trn-In1.inp
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M21TR~28   INP      579  05-27-98  5:26p  m21trn-Is.inp
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M21TR~32   INP      575  05-27-98  5:24p  m21trn-Iw2.inp
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276

M21TR-36 INP	570	05-19-98	1:18p	m21trn-n2.inp
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2 file(s)					6,594 bytes

Directory of F:\wrkST

.	<DIR>		06-01-98	4:33p	.
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M21D96~8 INP	2,202	05-28-98	2:33p	m21D96Nnow.inp	
M21M9~10 INP	2,189	05-16-98	11:22a	m21M97Sssw.inp	
M21M9~12 INP	2,192	05-28-98	5:12p	m21M97Nnow.inp	
M21M9~14 INP	2,202	05-28-98	2:30p	m21M97Nsse.inp	
M21M9~16 INP	2,206	05-28-98	2:31p	m21M97Nssw.inp	
M21M9~18 INP	2,197	05-16-98	4:12p	m21M97Snow.inp	
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8 file(s)					17,581 bytes

Total files listed:

336 file(s)	226,480,887 bytes
69 dir(s)	0 bytes free

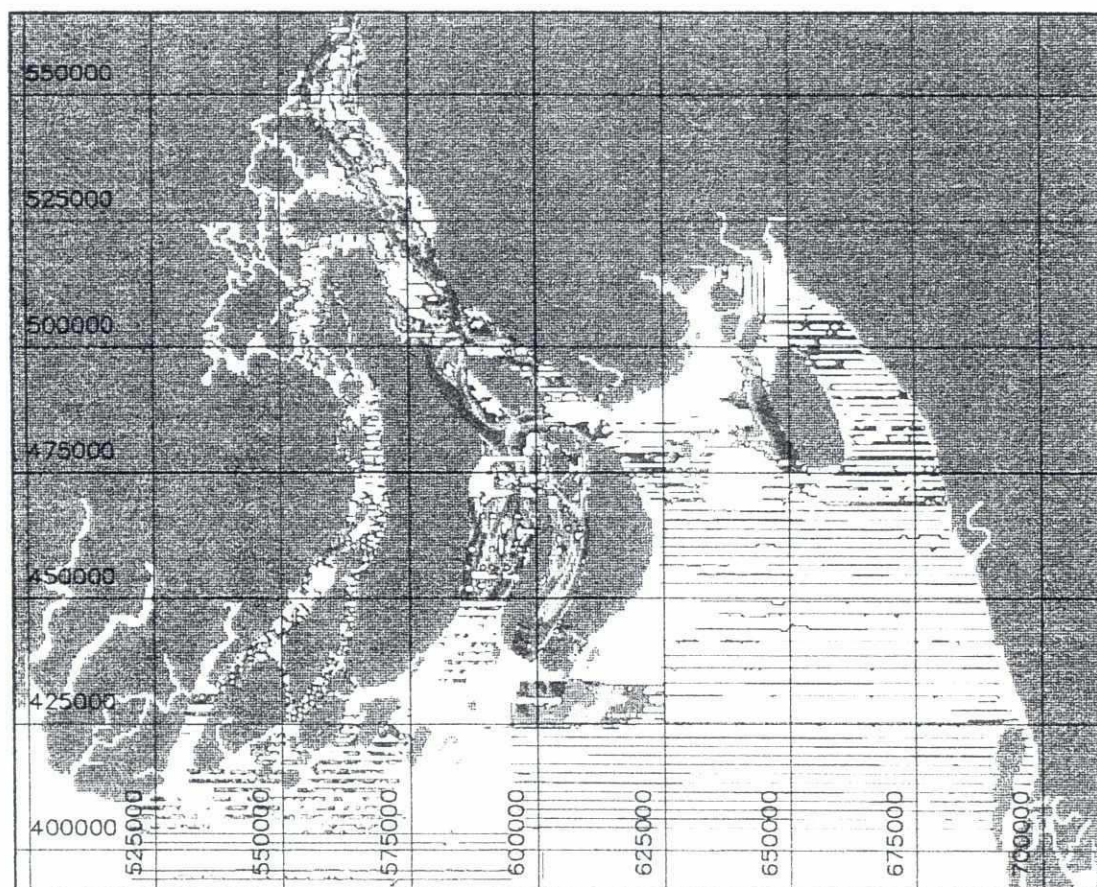
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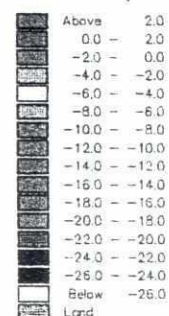
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529

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04/09/98 10:41:10



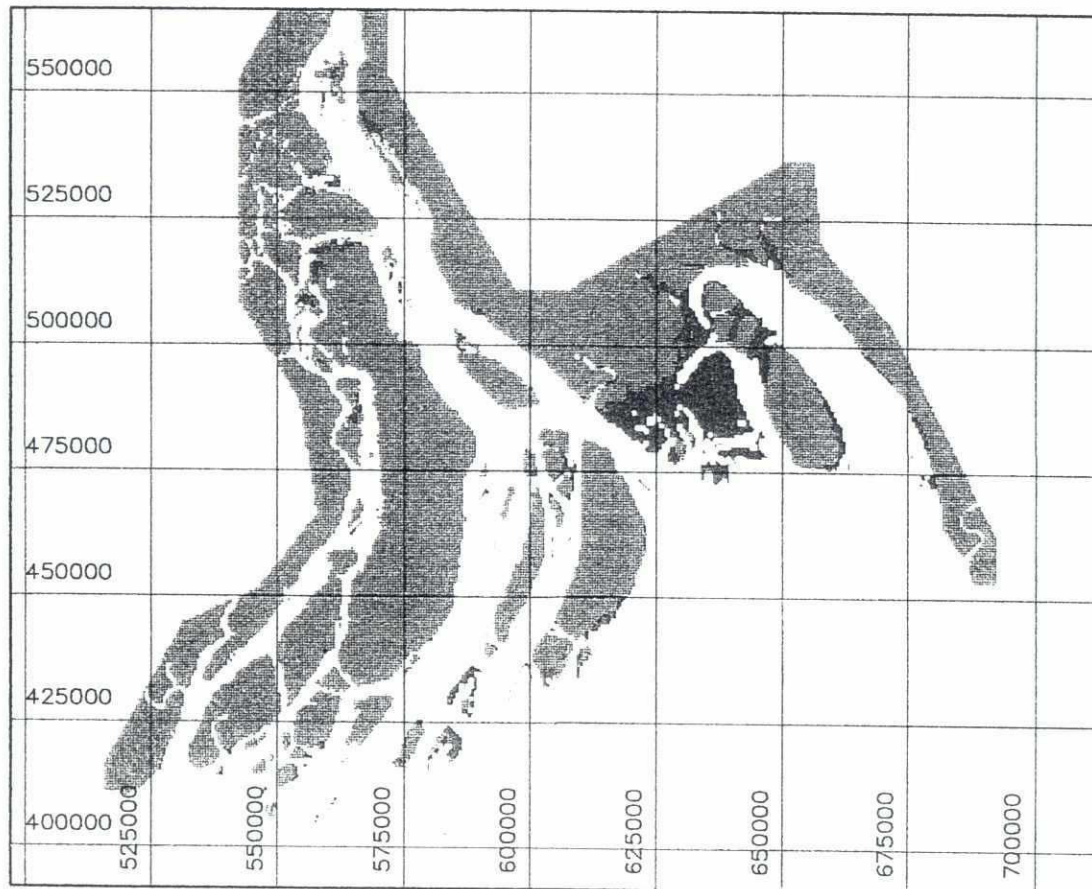
Elevation (m PWD)



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		Project:	Meghna Estuary Study	
File:	Date: Mon Jun 8 1998	Bathymetry data coverage MES bathymetric survey		Drawing no. 3.1
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326

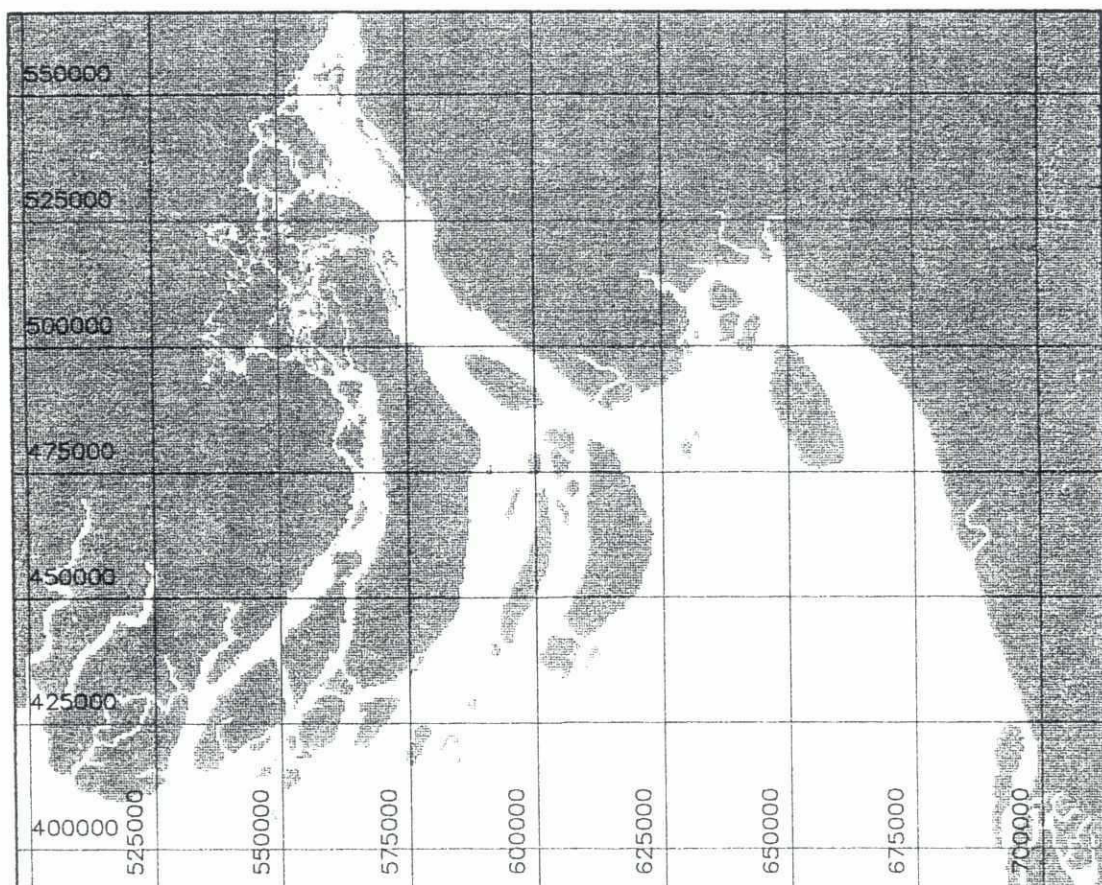
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Elevation (m PWD)

Above	2.0
1.0 -	2.0
0.0 -	1.0
-1.0 -	0.0
-2.0 -	-1.0
-3.0 -	-2.0
-4.0 -	-3.0
Below	-4.0
Land	

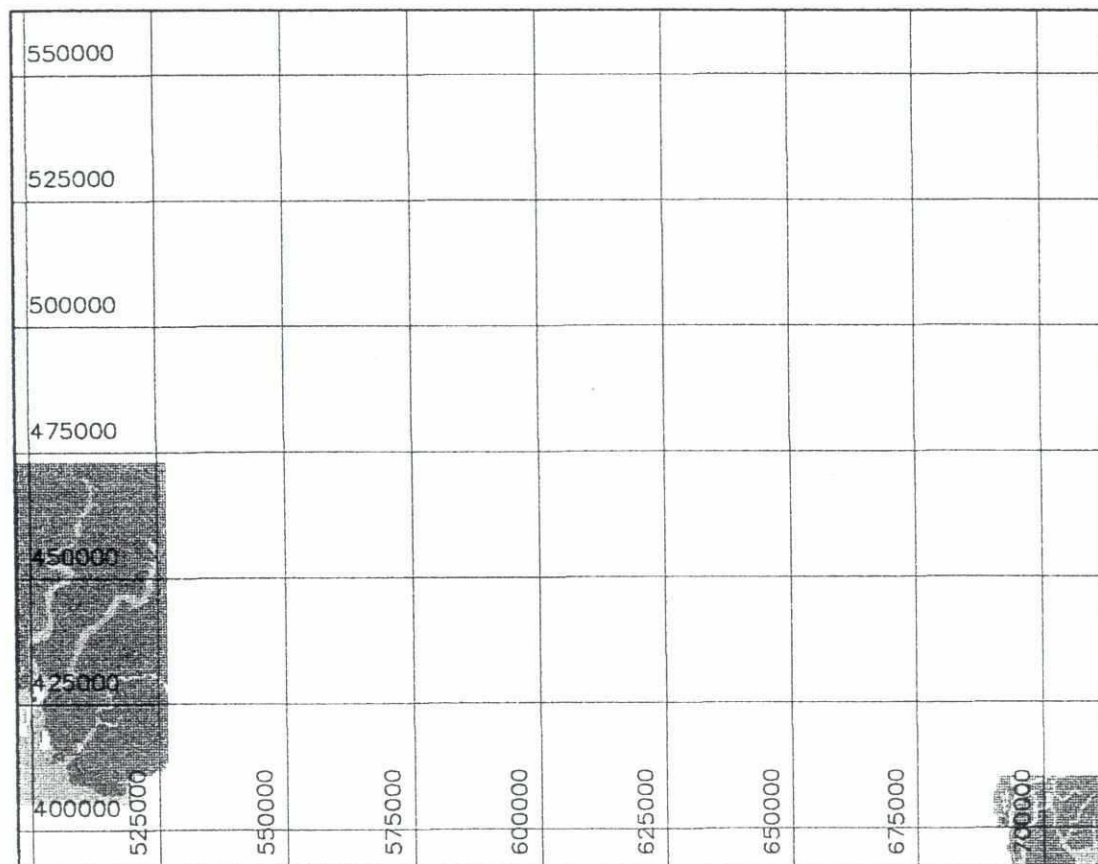
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File:	Date: Mon Jun 8 1998	Bathymetry data coverage Landsat image, February 1996		Drawing no. 3.2
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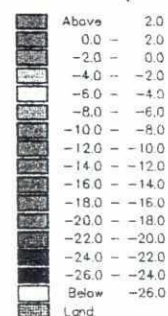
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File:	Date: Mon Jun 8 1998	Bathymetry data coverage BIWTA sea charts		Drawing no.
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220

SW-103 10/1/98

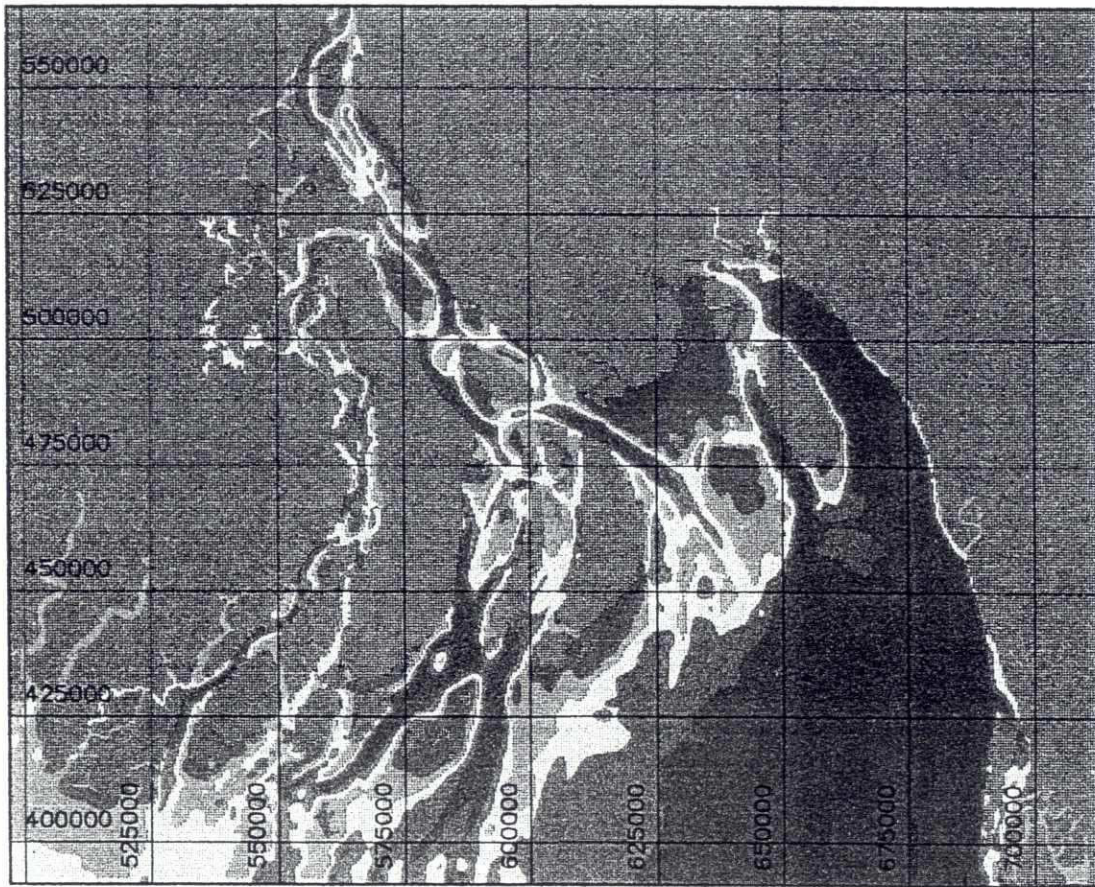


Elevation (m PWD)

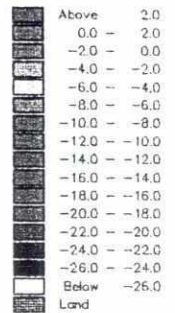


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		Project:	Meghna Estuary Study	
File:	Date: Mon Jun 8 1998	Bathymetry data coverage British Admiralty Charts (CSPS)		Drawing no.
Scale: 1:1500000	Init: p5011			3.4

২২



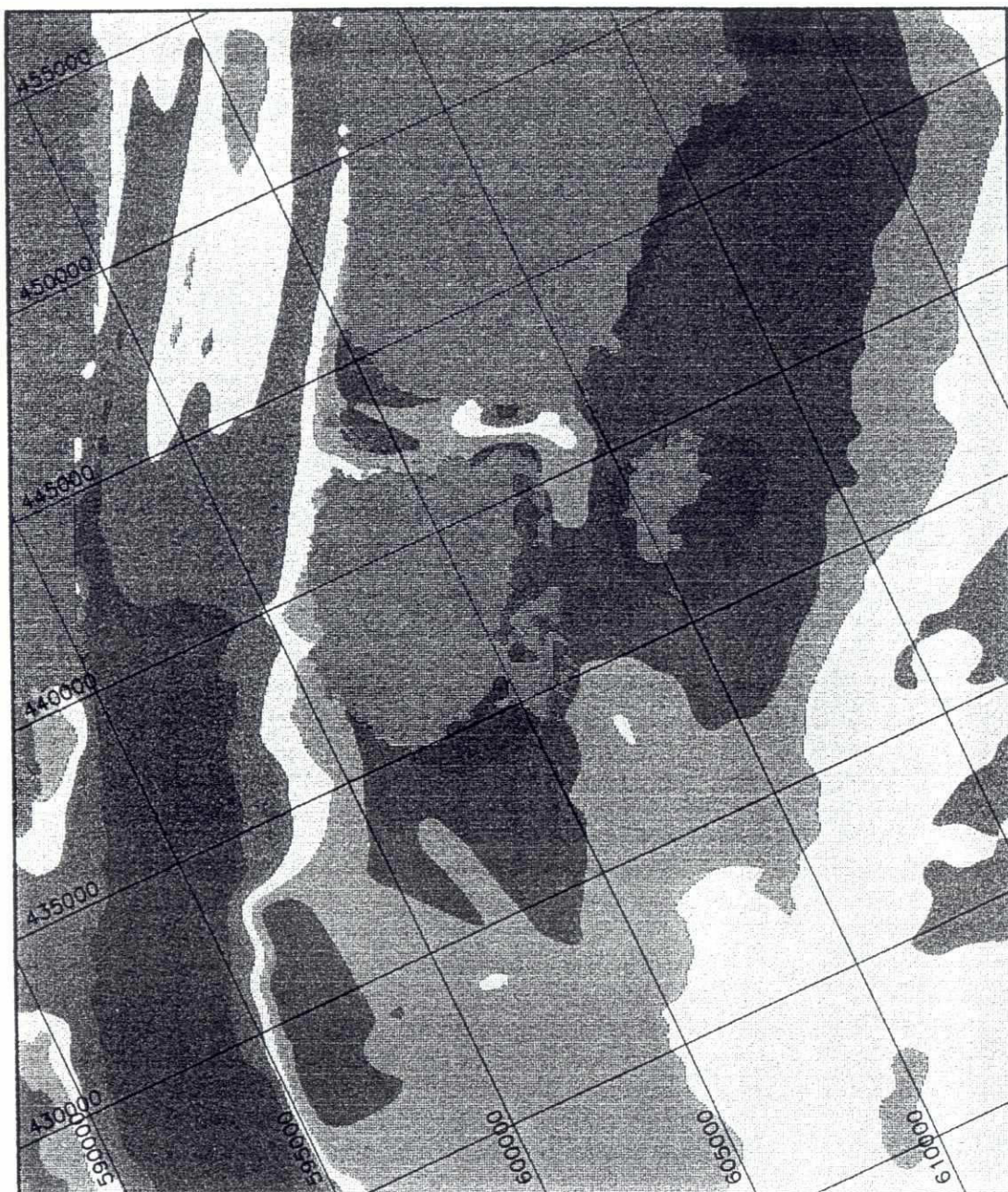
Elevation (m PWD)



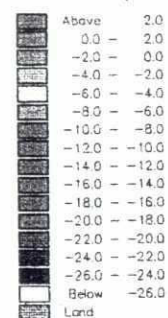
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File:	Date: Mon Jun 8 1998	Model bathymetry Meghna Estuary Model			Drawing no. 3.5
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222

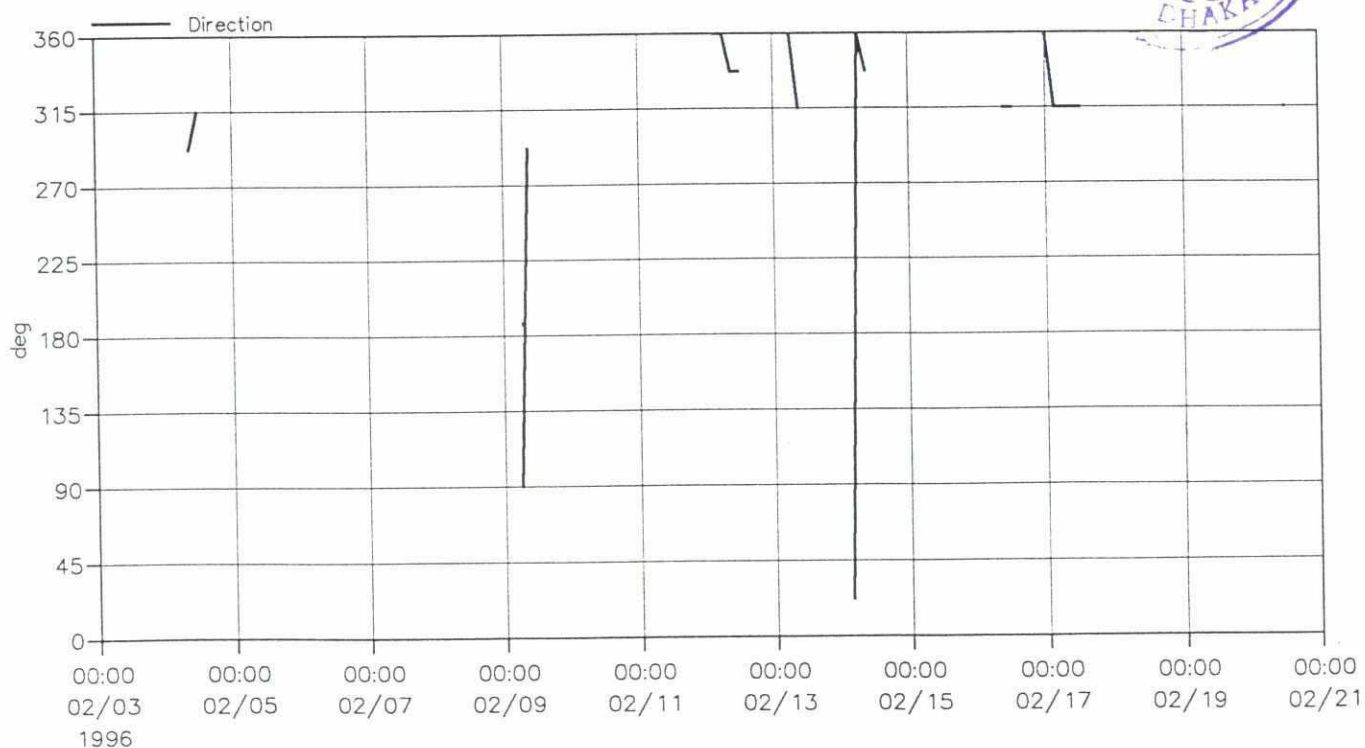
ofc bathy/lev



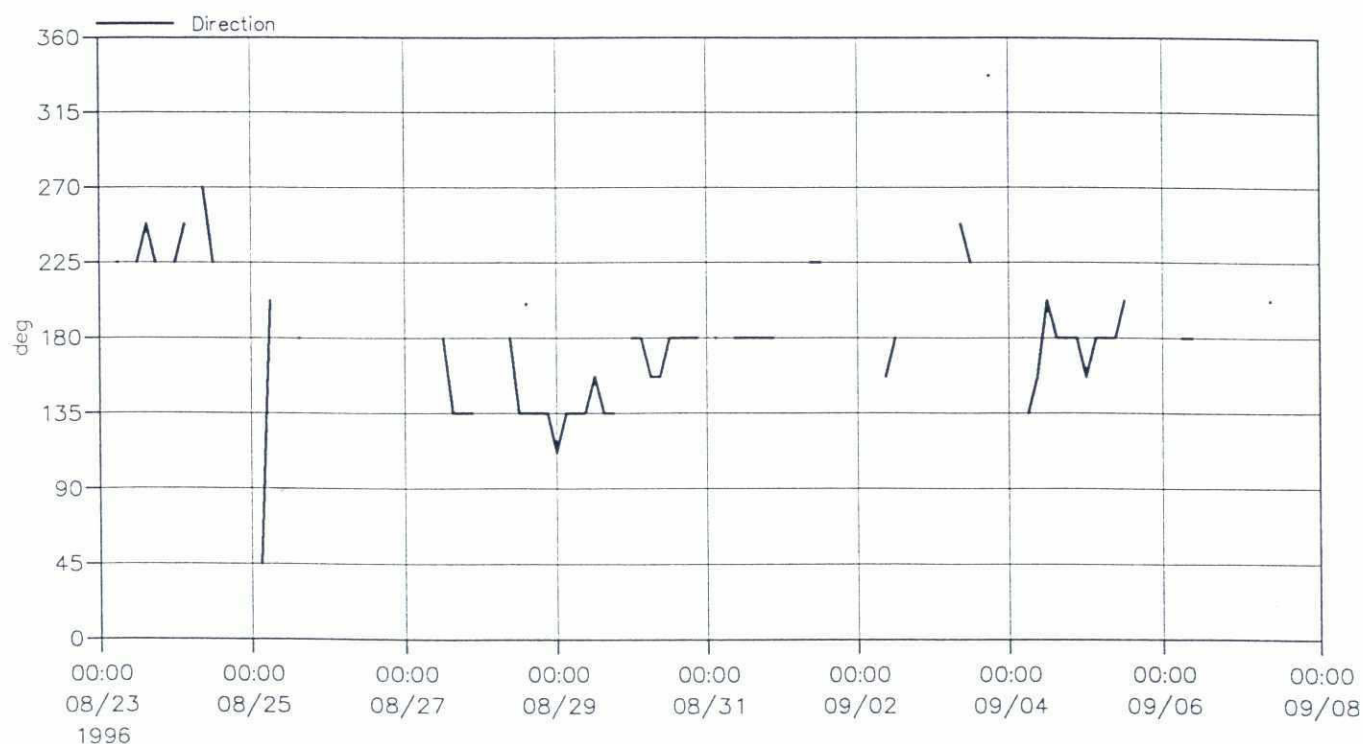
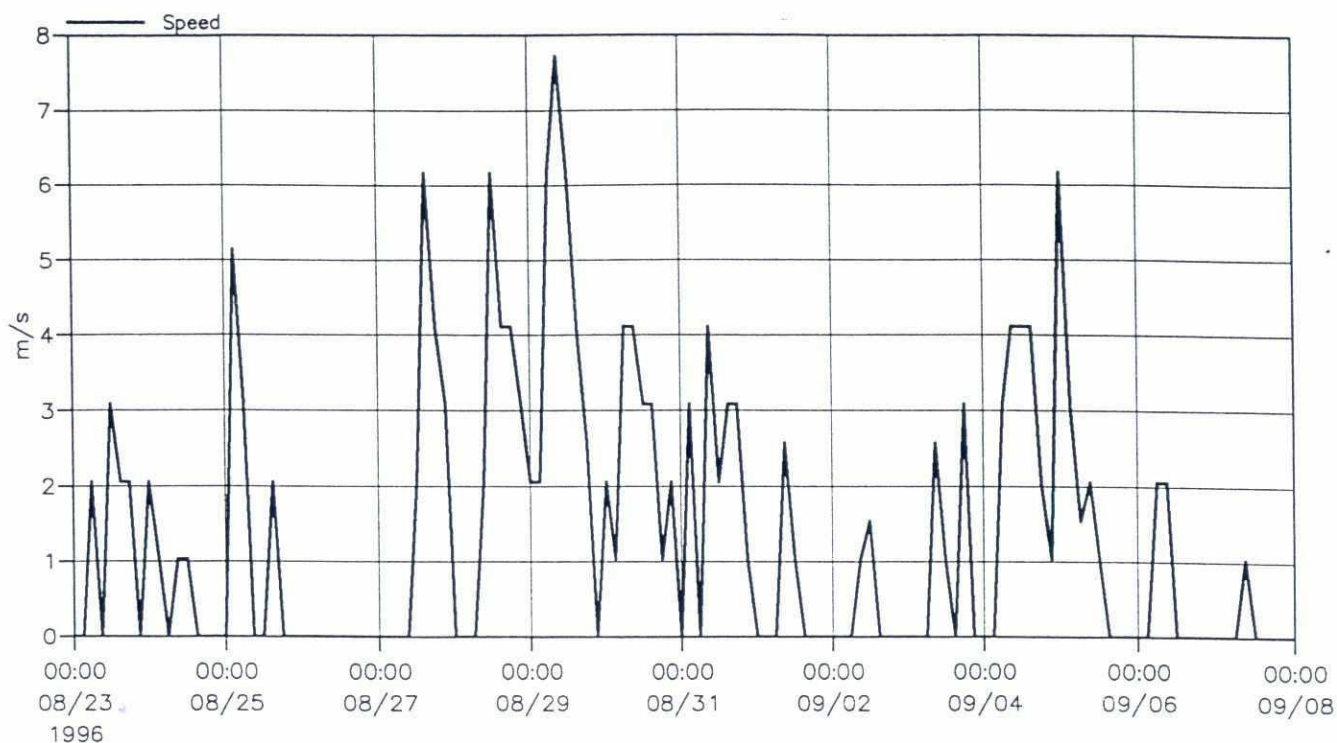
Elevation (m PWD)



SWMC		Client:	Bangladesh Water Development Board	MIKE 21
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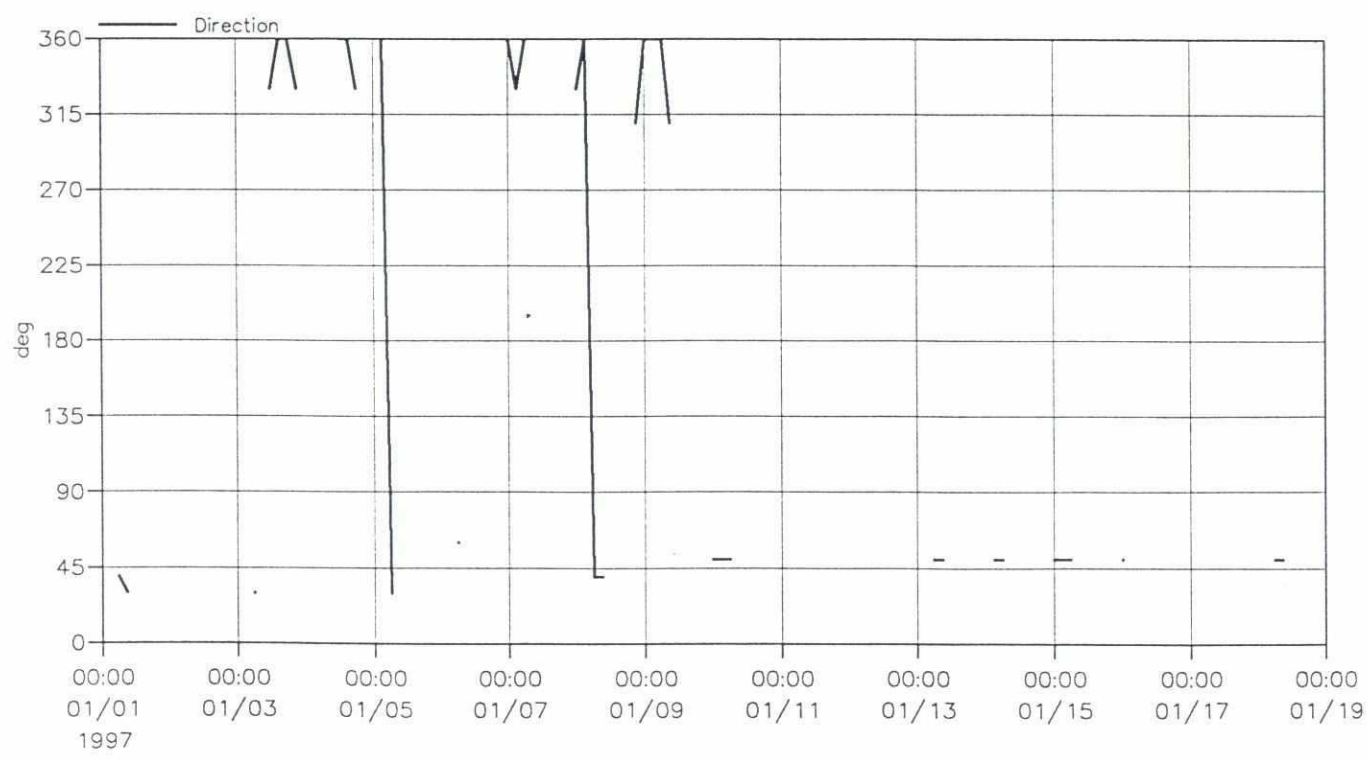
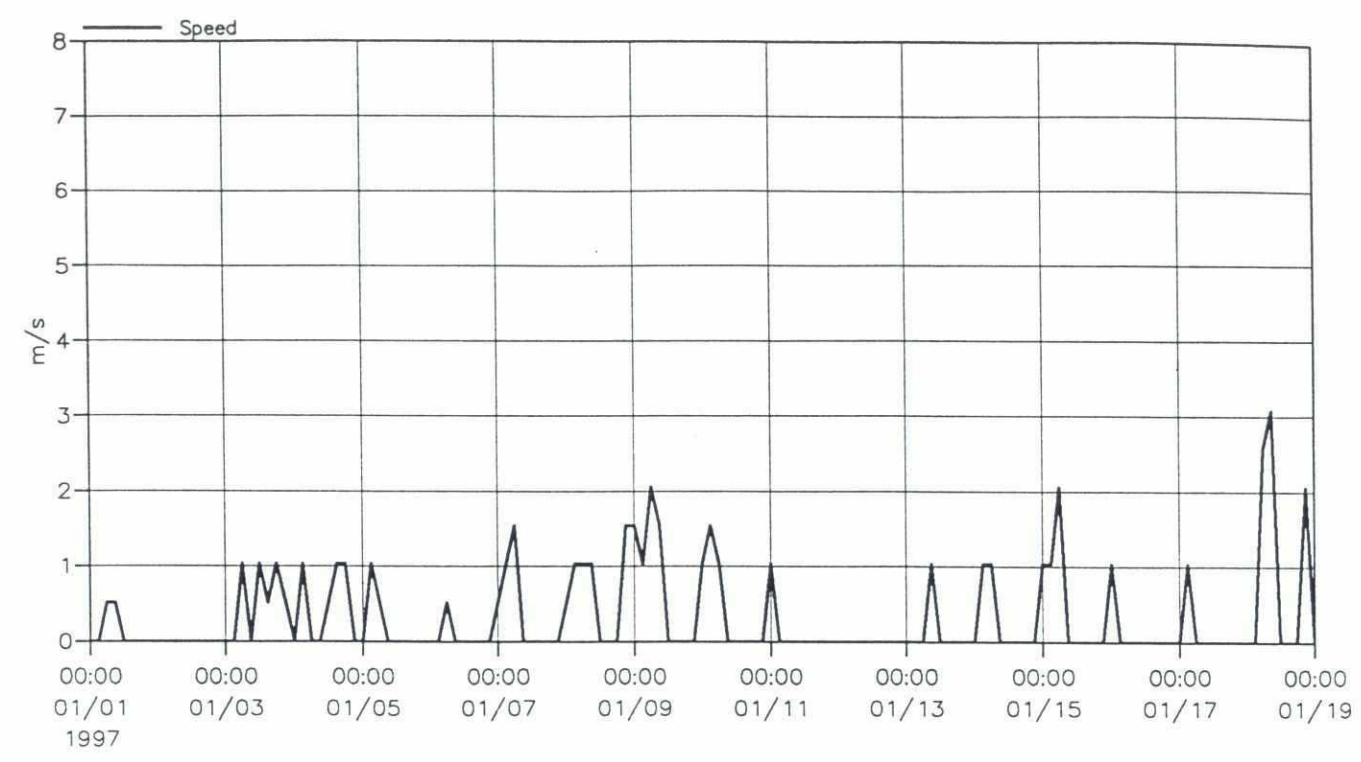
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File:	Date: Thu Apr 23 1998	<div style="text-align: center;"> Hatia Wind data for Dry Period Run 1996 </div>		<div style="font-weight: bold;">4.1</div>
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SWMC		Client: Bangladesh Water Development Board		MIKE 21
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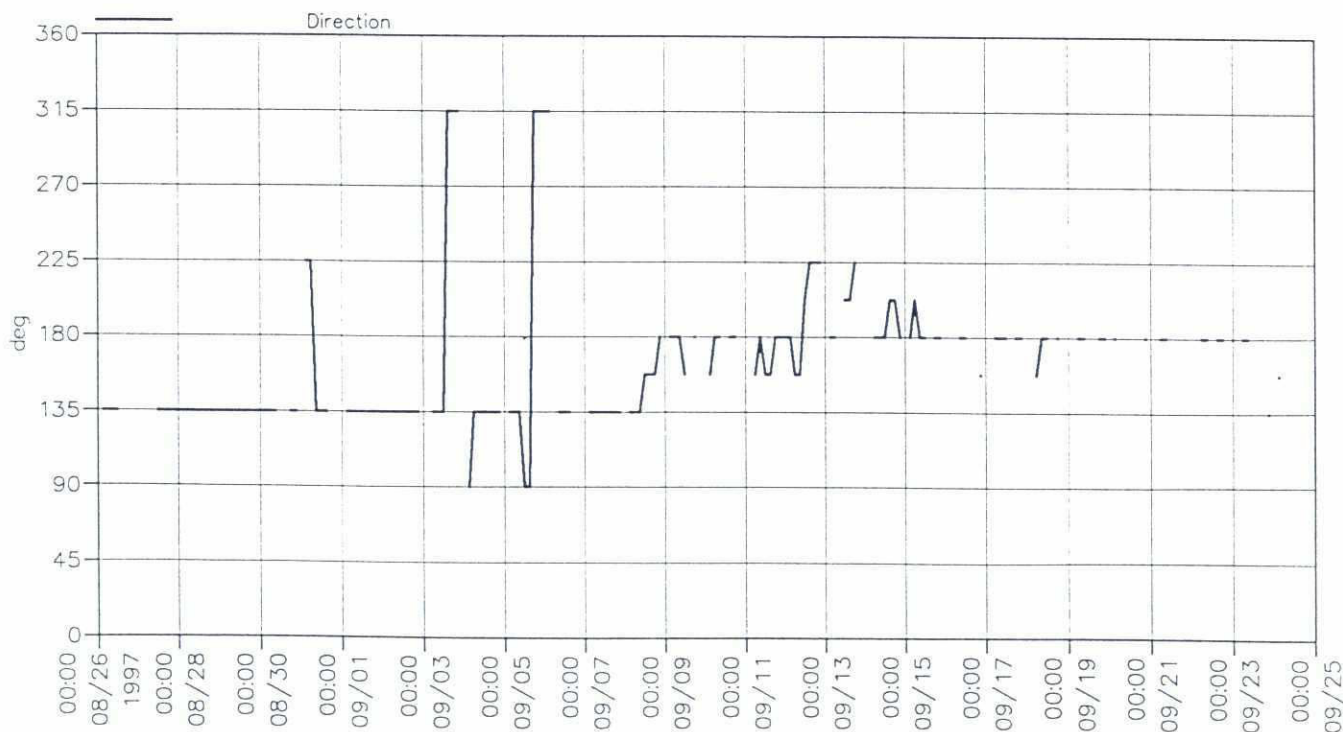
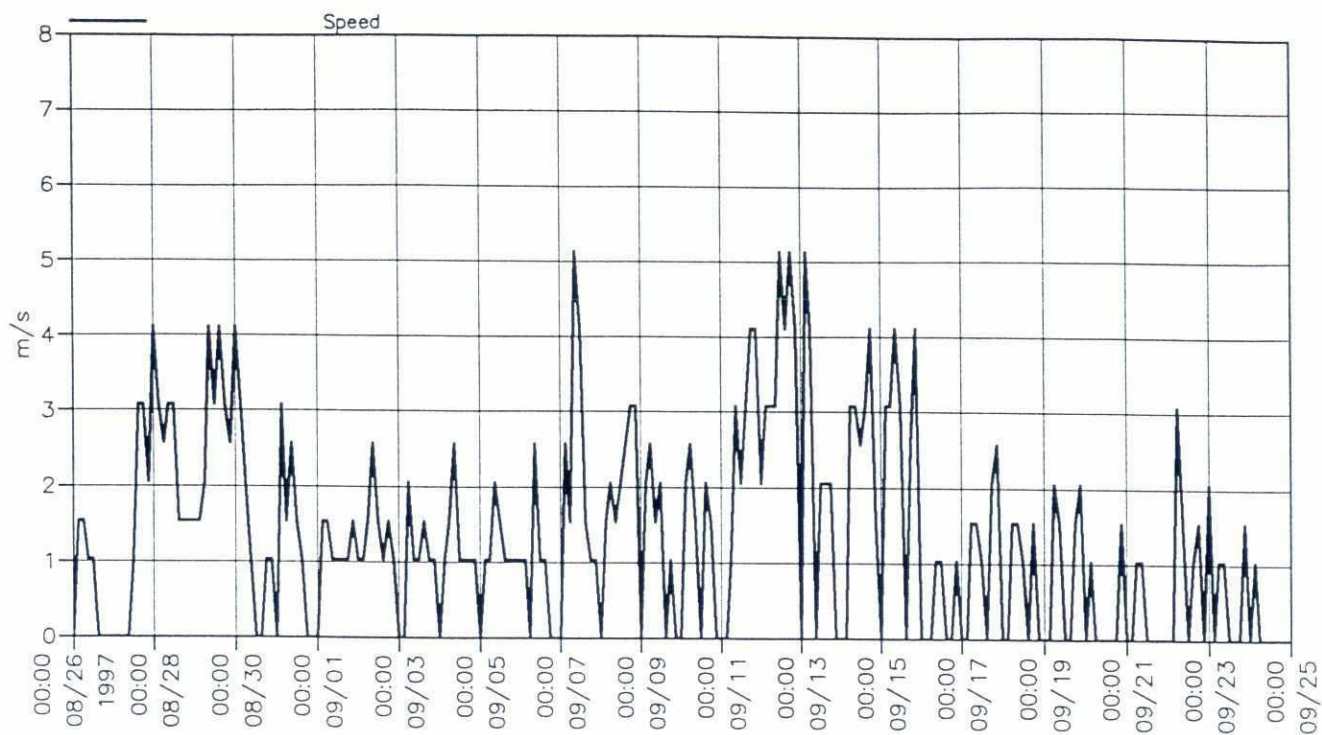
224

Windmeter Model 197

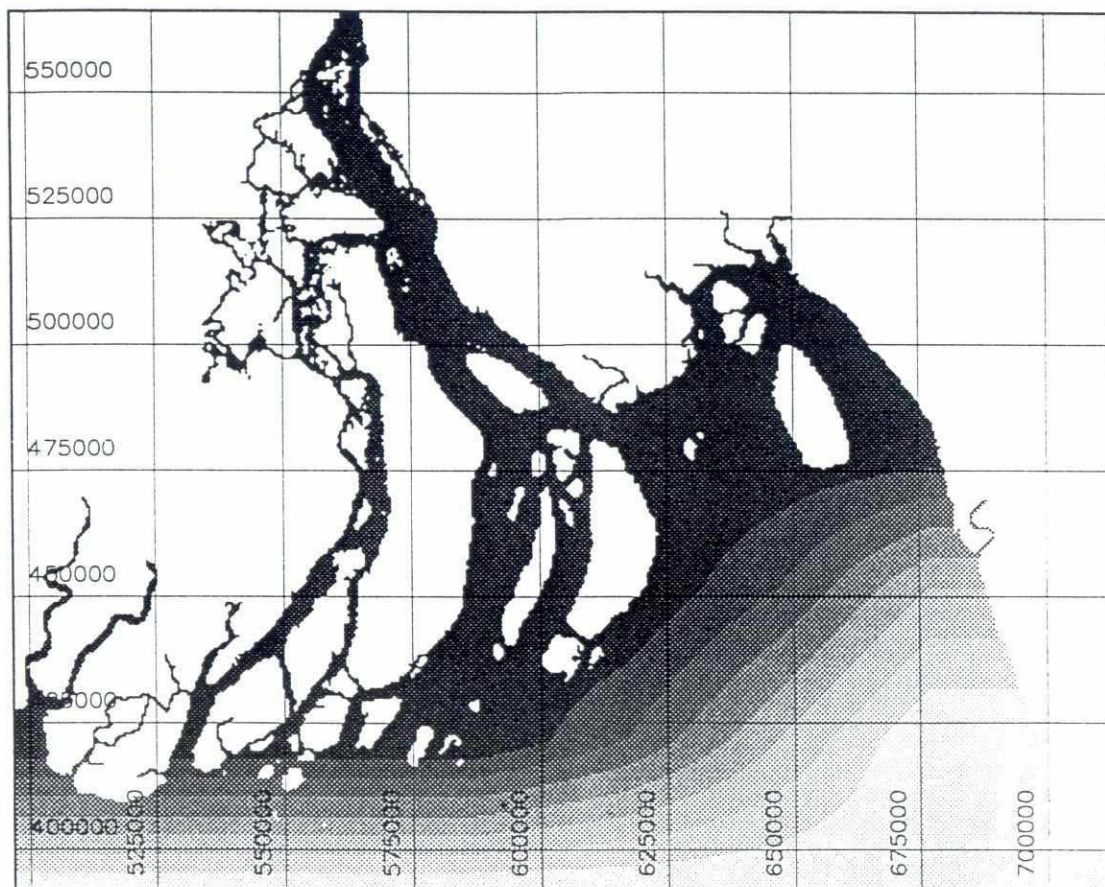


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File:	Date: Thu Apr 23 1998	Hatia Wind data for Dry Period Run 1997		Drawing no. 4.3
Scale:	Init: p5011			

22



SWMC		Client:	Bangladesh Water Development Board	MIKE 21
		Project:	Meghna Estuary Study	
File:	Date:	Hatia Wind data for Monsoon 1997		Drawing no. 4.4
Scale:	Init:			
	Thu Apr 23 1998			
	p5011			

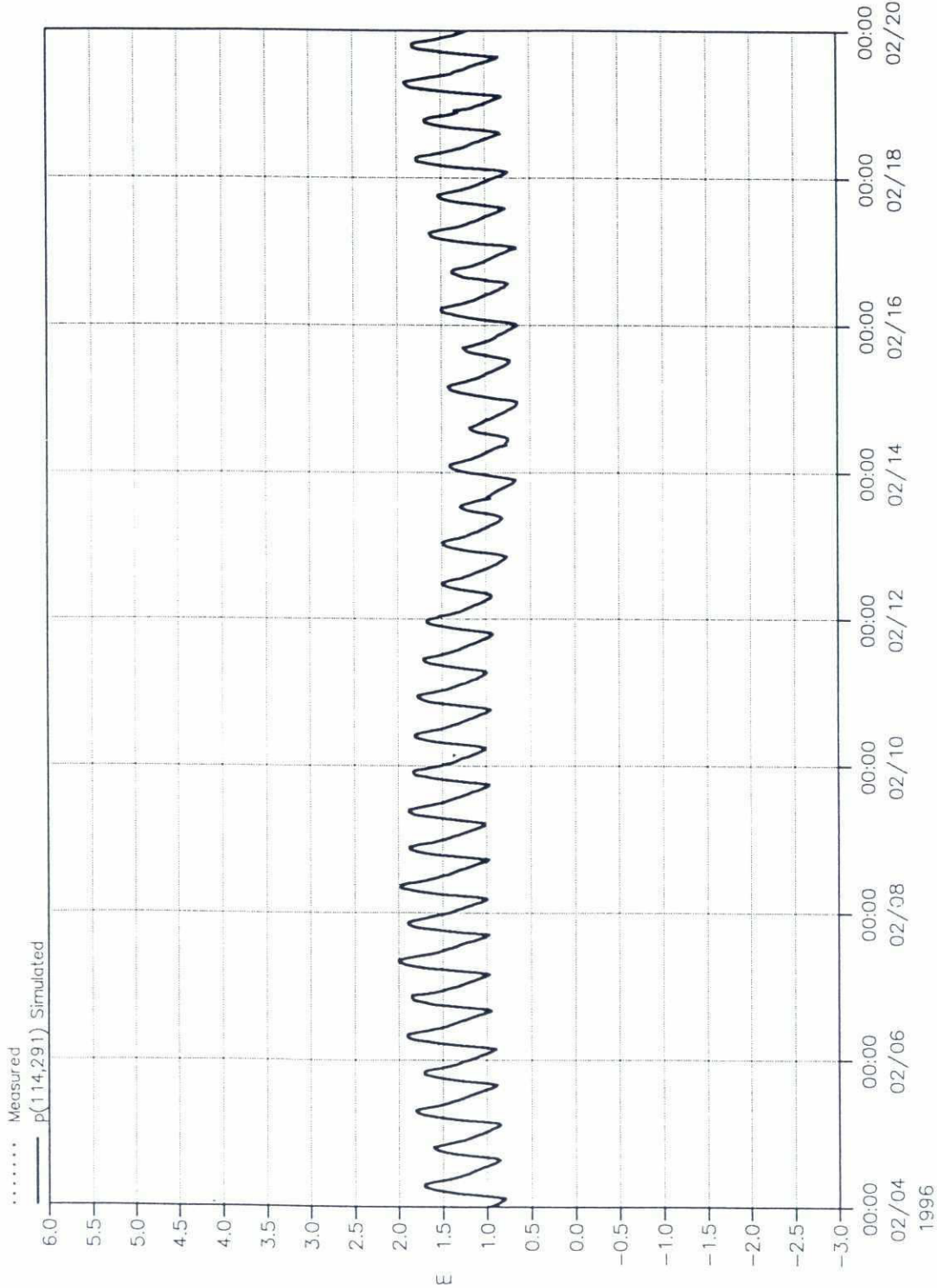


Manning Number

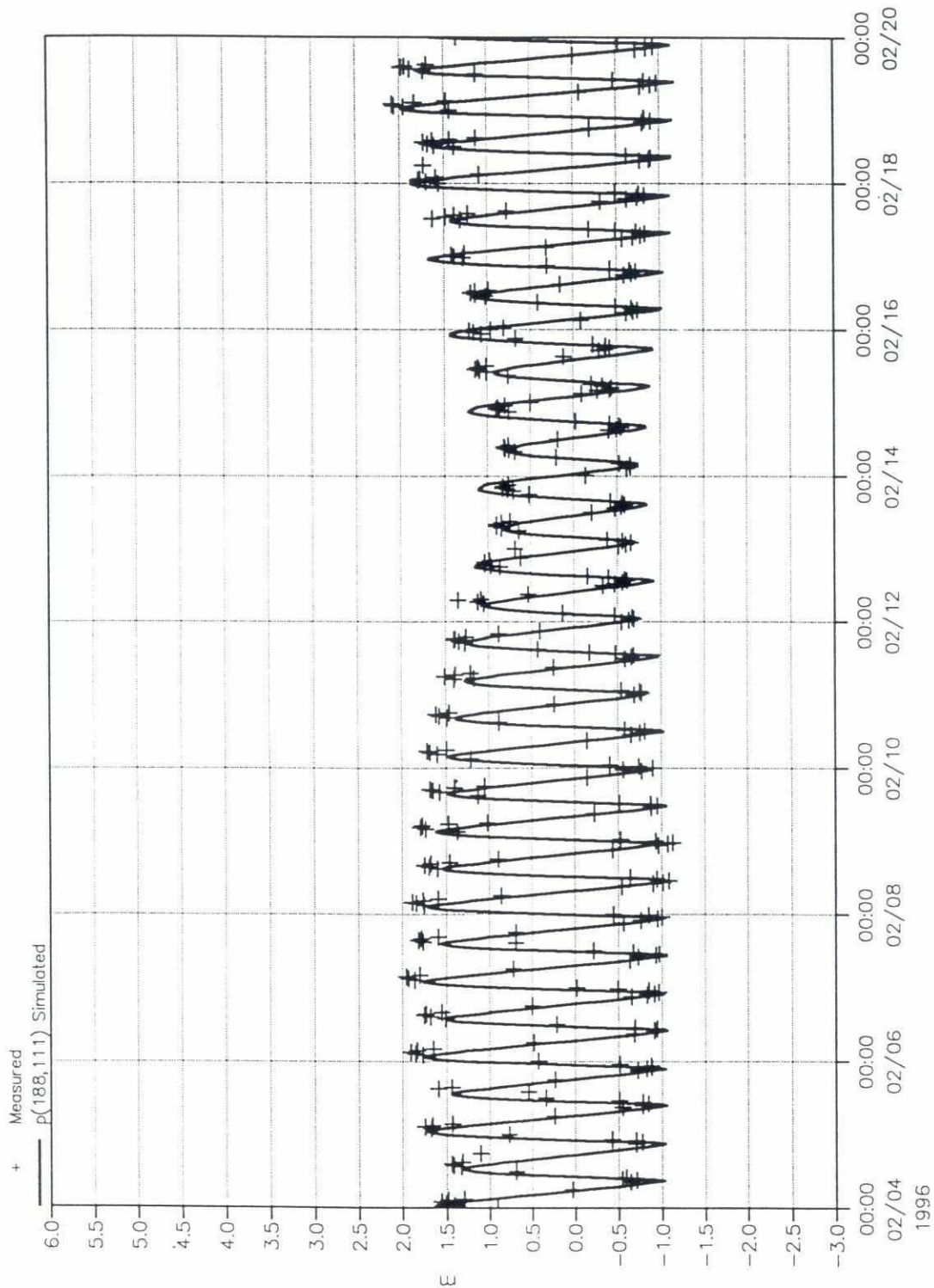
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	90	90
	85	85
	80	80
	75	75
	70	70
	65	65
	Below	65
	Land	

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		Project:	Meghna Estuary Study	
File:	Date: Mon Jun 8 1998	Bed friction coefficients Manning Numbers (m 1/3 / s)		Drawing no. 4.5
Scale: 1:1500000	Init: p5011			

28



SWMC		Client: Bangladesh Water Development Board		MIKE 21
		Project: Meghna Estuary Study		
File:	Date: Sun May 31 1998	Measured and simulated water level at Chandpur (PWD)		Drawing no. 4.6
Scale:	Init: p5011	Dry Season 1996		



SWMC		Client: Bangladesh Water Development Board		MIKE 21
Date: Sun May 31 1998		Project: Meghna Estuary Study		
File:		Measured and simulated water level at Char Chenga (PWD)		Drawing no.
Scale:	Init: p5011	Dry Season 1996		4.7

SWMC

Client:

Bangladesh Water Development Board

Project:

Meghna Estuary Study

Date: Sun May 31 1998

Measured and simulated water level at Char Chenga (PWD)

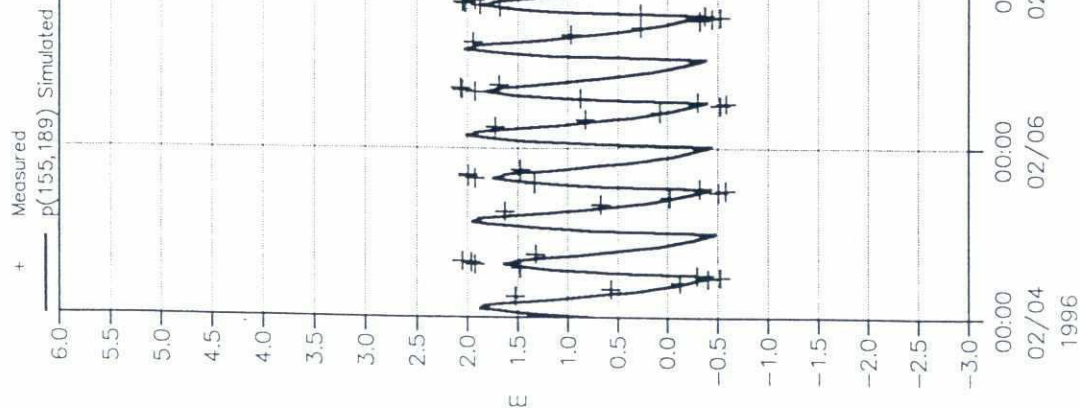
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4.7

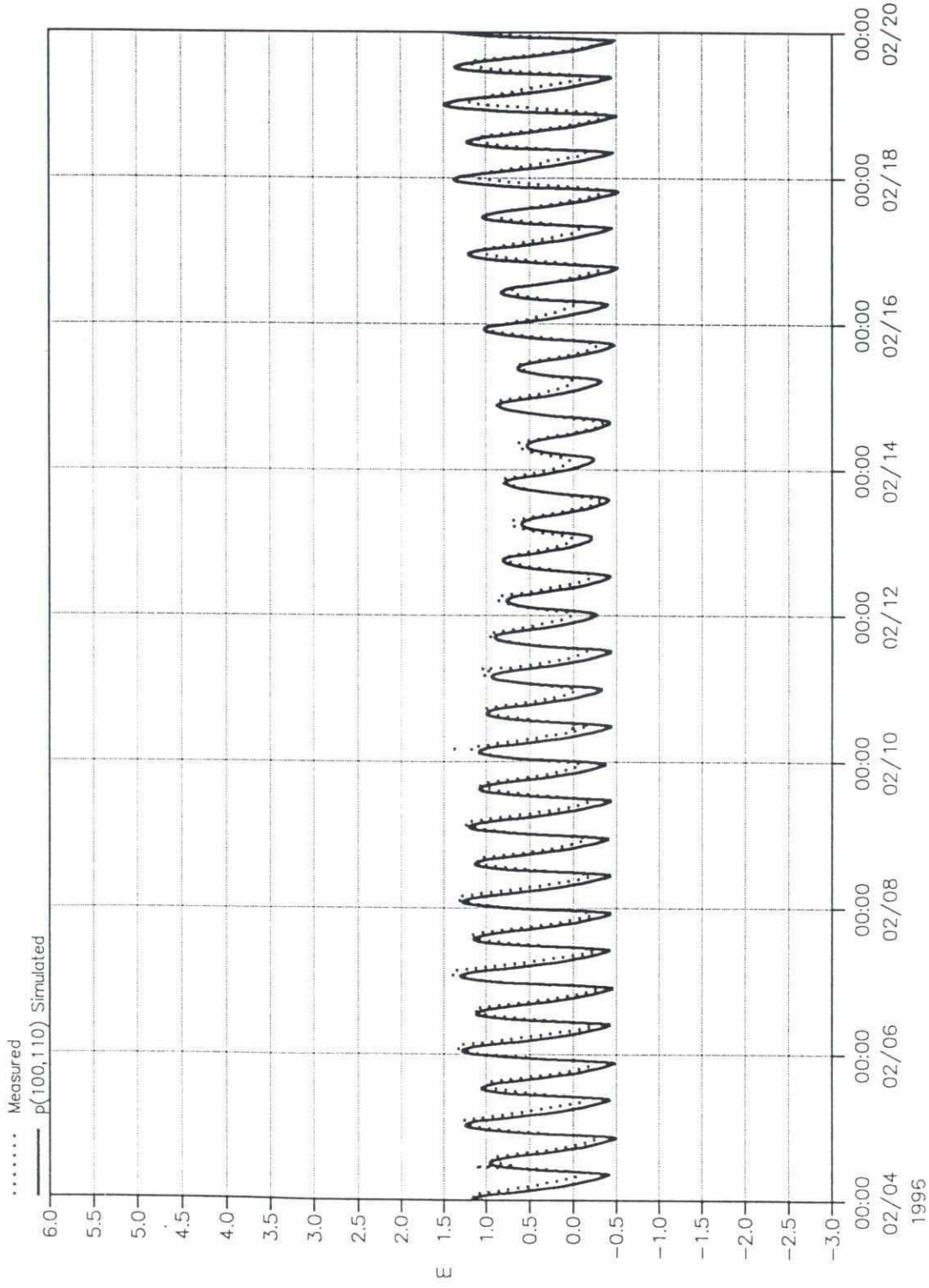
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Dry Season 1996

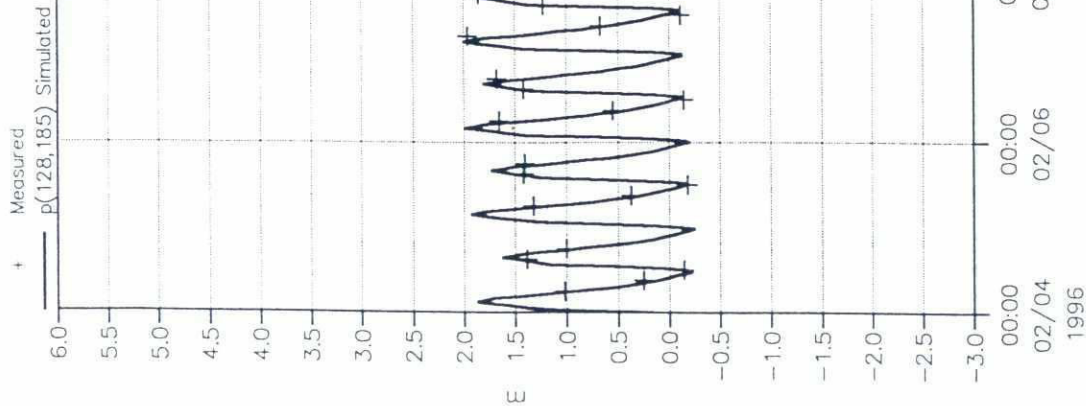


SWMC		Client: Bangladesh Water Development Board		MIKE 21
		Project: Meghna Estuary Study		
File:	Date: Sun May 31 1998	Measured and simulated water level at Chitalkhali (PWD)		Drawing no.
Scale:	Init: p5011	Dry Season 1996		4.8

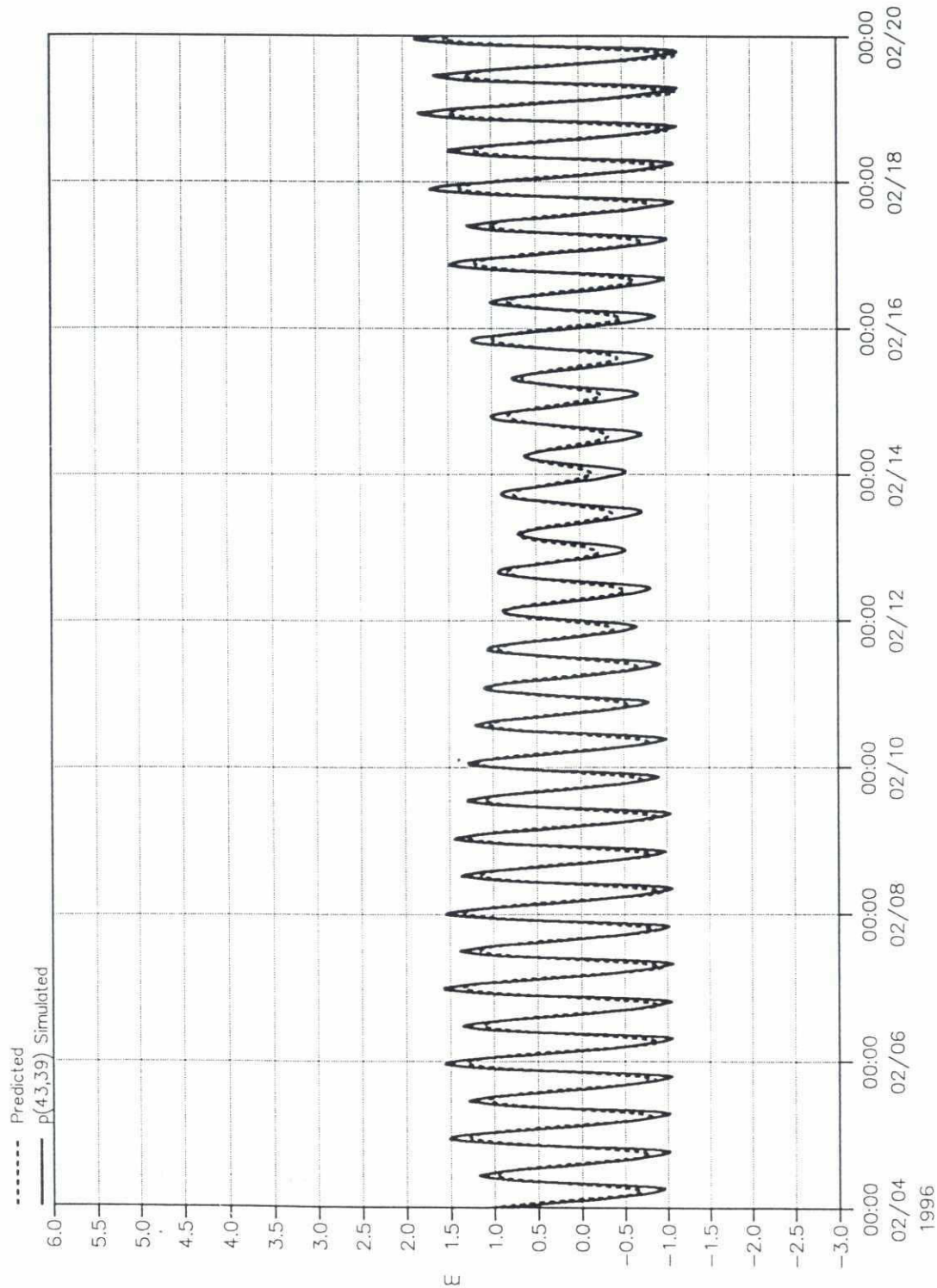


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		Project: Meghna Estuary Study		
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Scale:	Init: p5011			

220

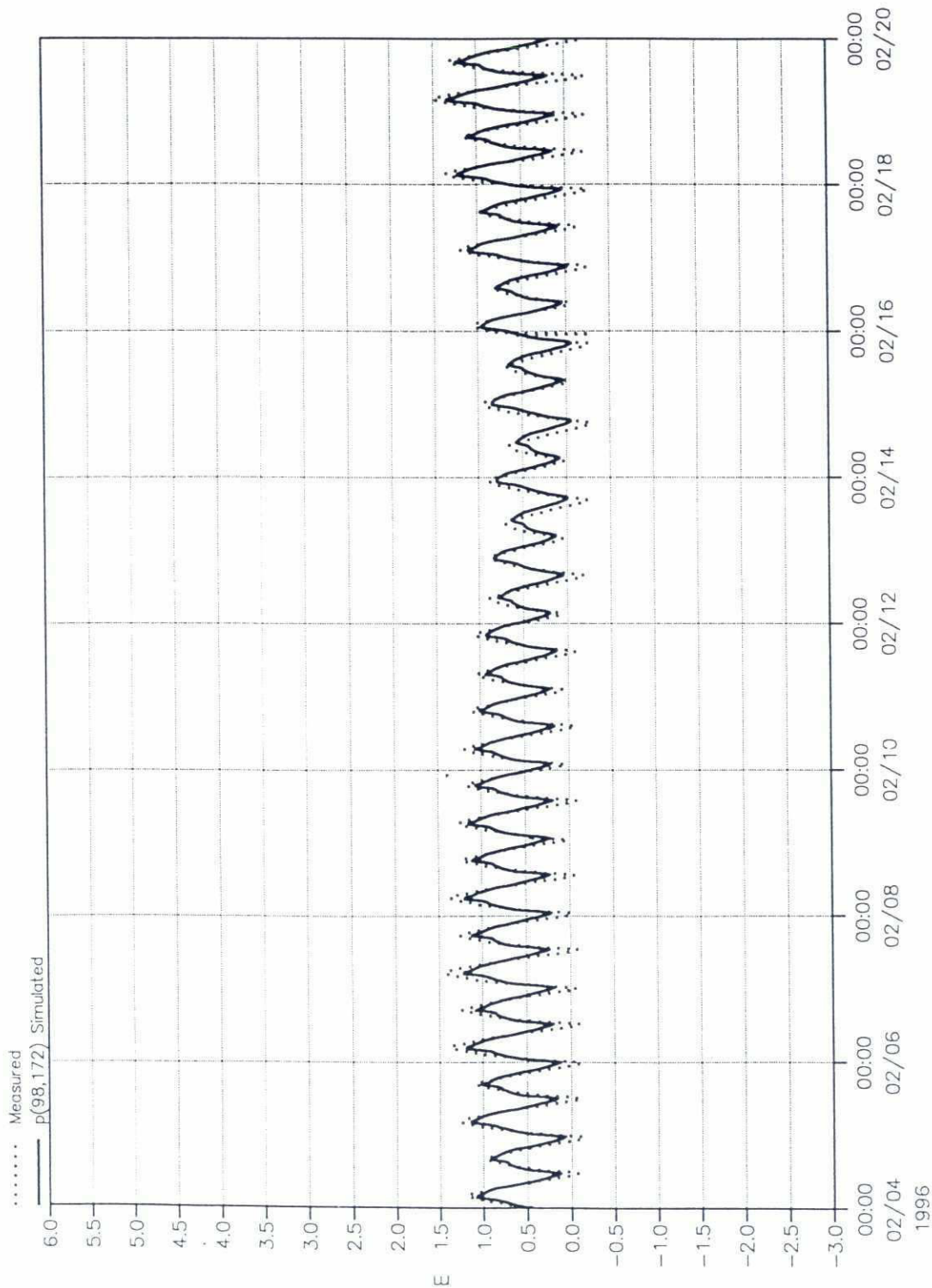


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		Project: Meghna Estuary Study		
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Scale:	Init: p5011	Dry Season 1996		

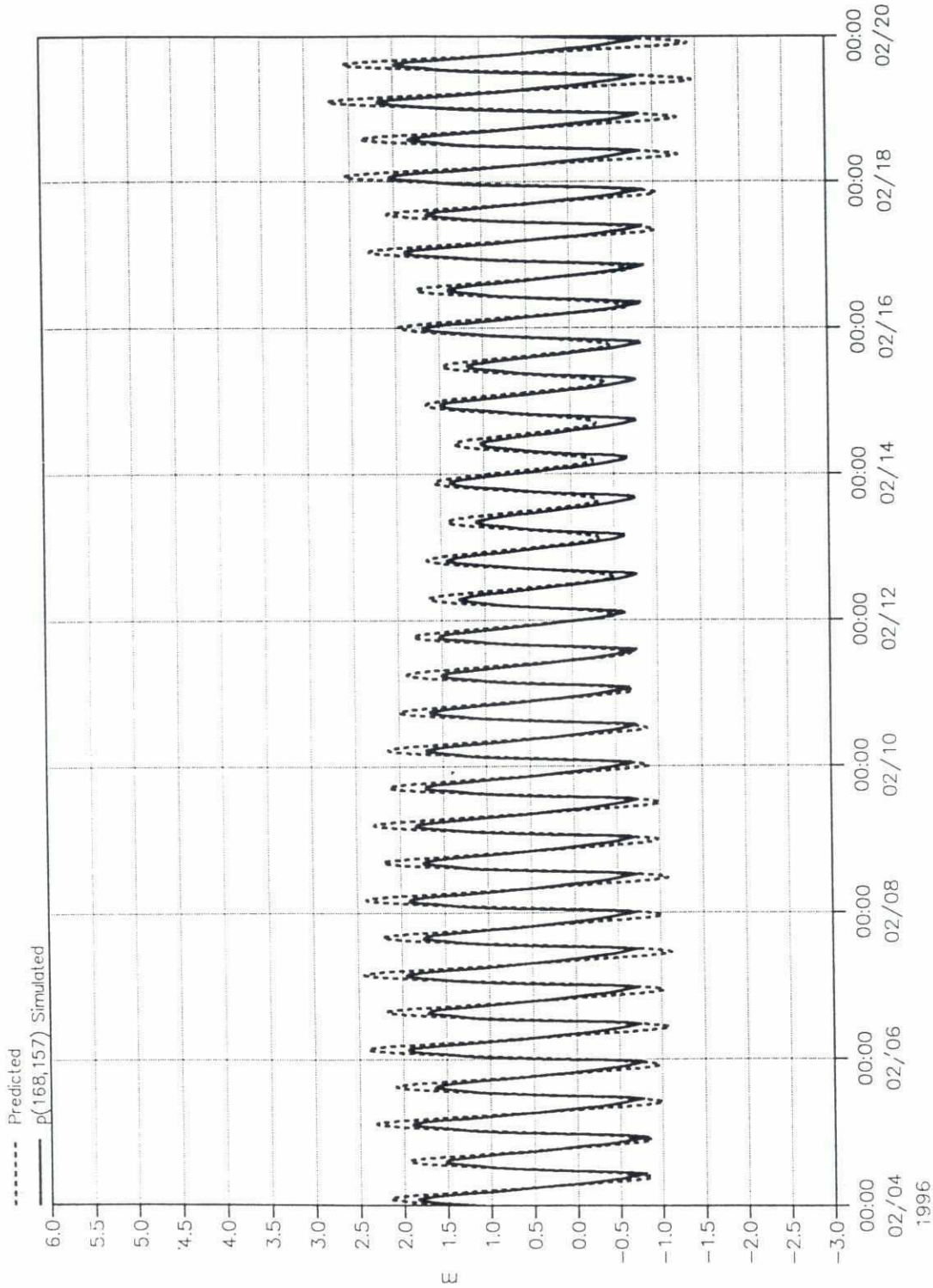


SWMC		Client: Bangladesh Water Development Board		MIKE 21
		Project: Meghna Estuary Study		
File:	Date: Sun May 31 1998	Measured and predicted water level at Dhulasar (PWD) Dry Season 1996		Drawing no.
Scale:	Init: p5011			4.11

268

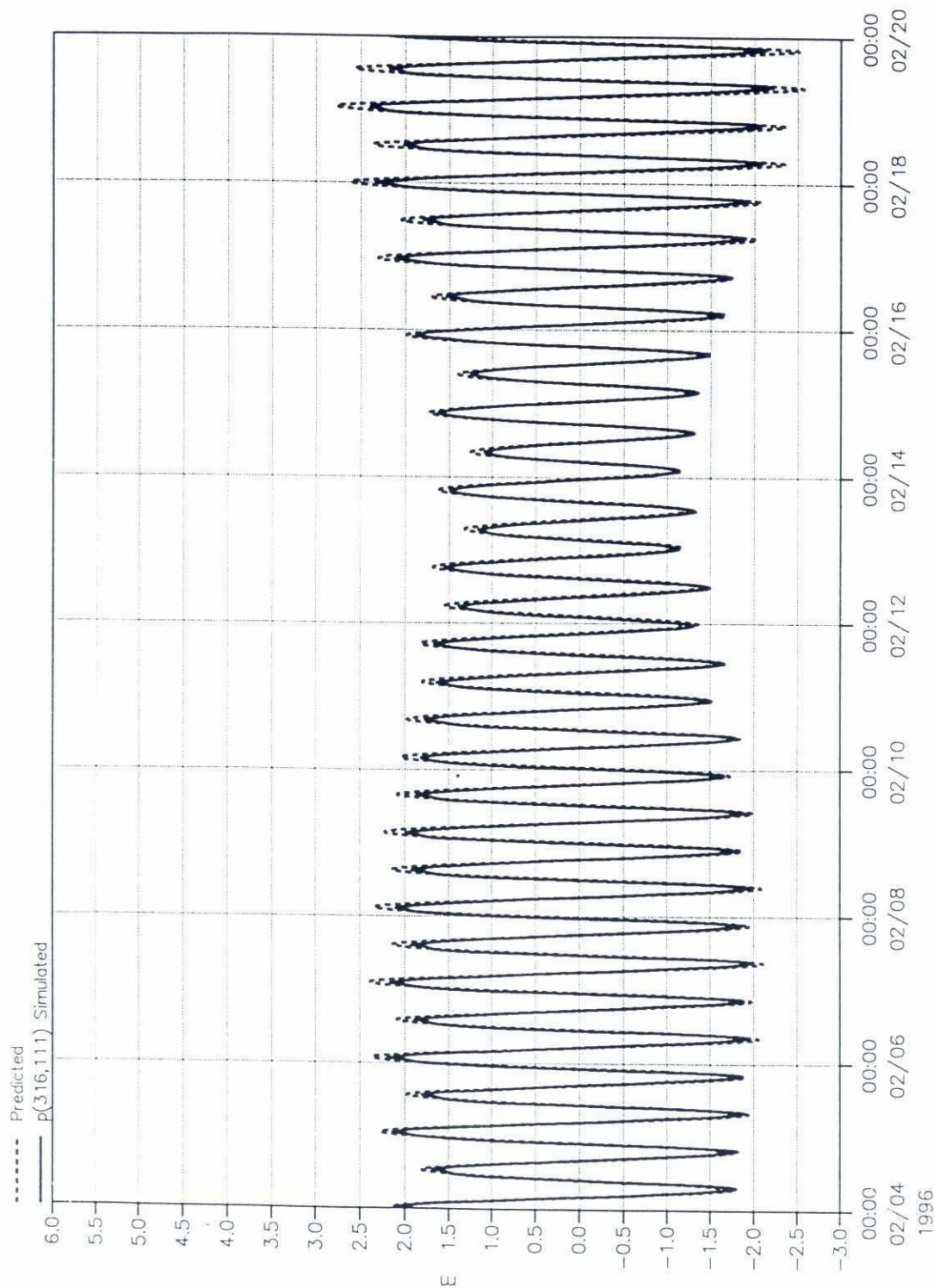


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		Project: Meghna Estuary Study		
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Scale:	Init: p5011			

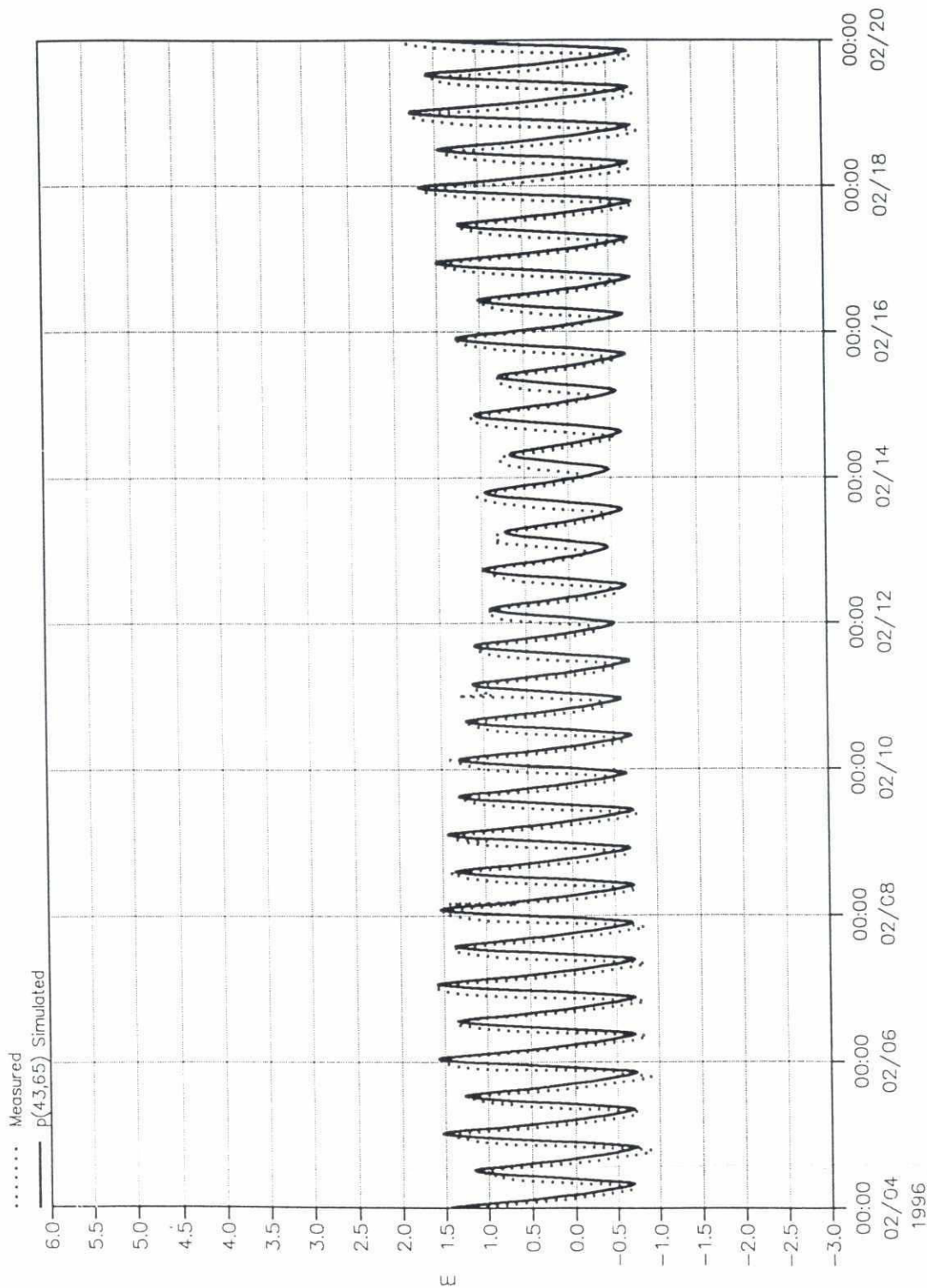


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Date: Sun May 31 1998		Project: Meghna Estuary Study		Drawing no.	
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Scale:		Hatia Bar (PWD)			
		Init: p5011		Dry Season 1996	

267



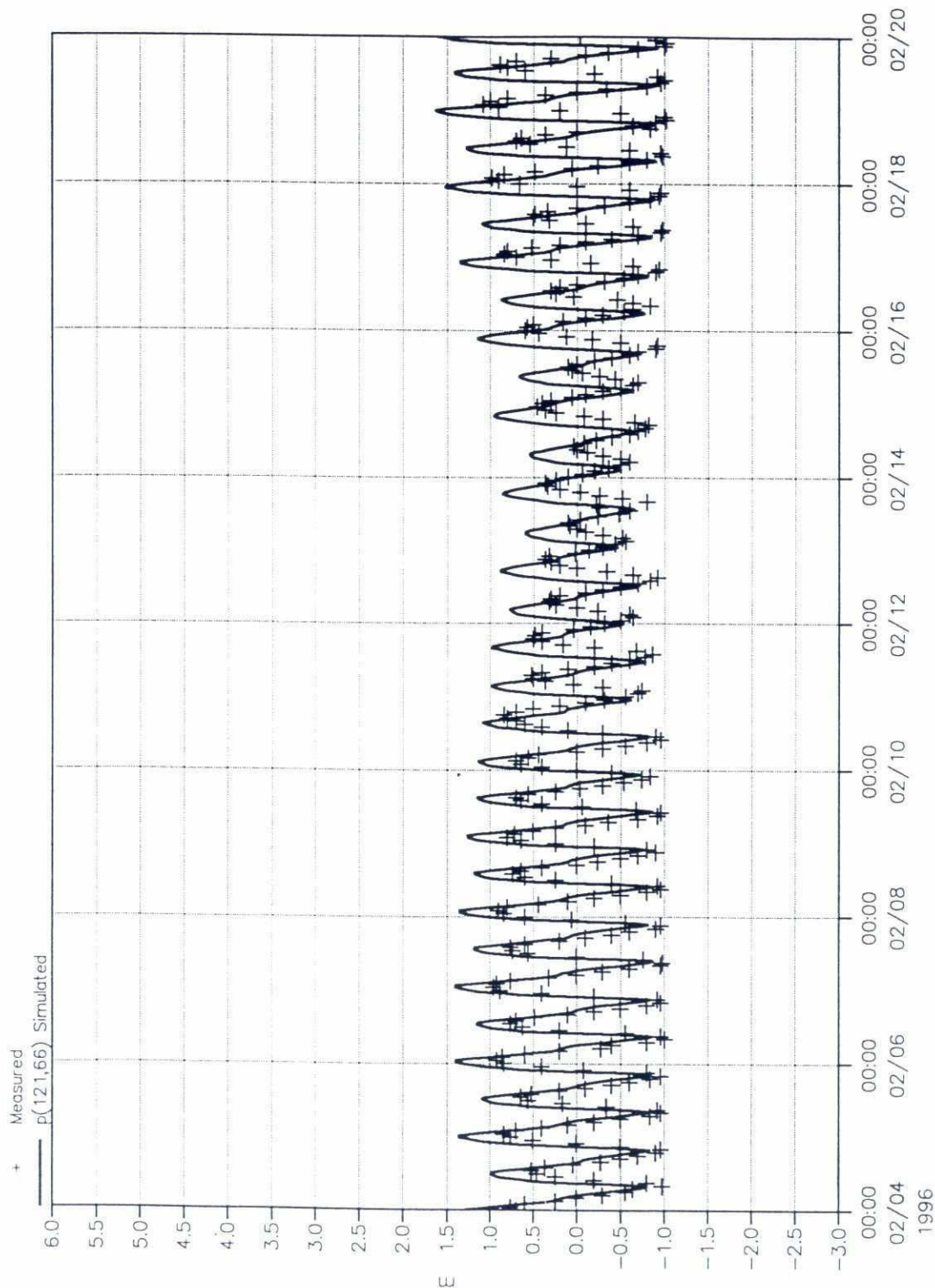
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File:	Date: Sun May 31 1998	Measured and predicted water level at Khal No. 18 (PWD) Dry Season 1996		Drawing no. 4.14
Scale:	Init: p5011			



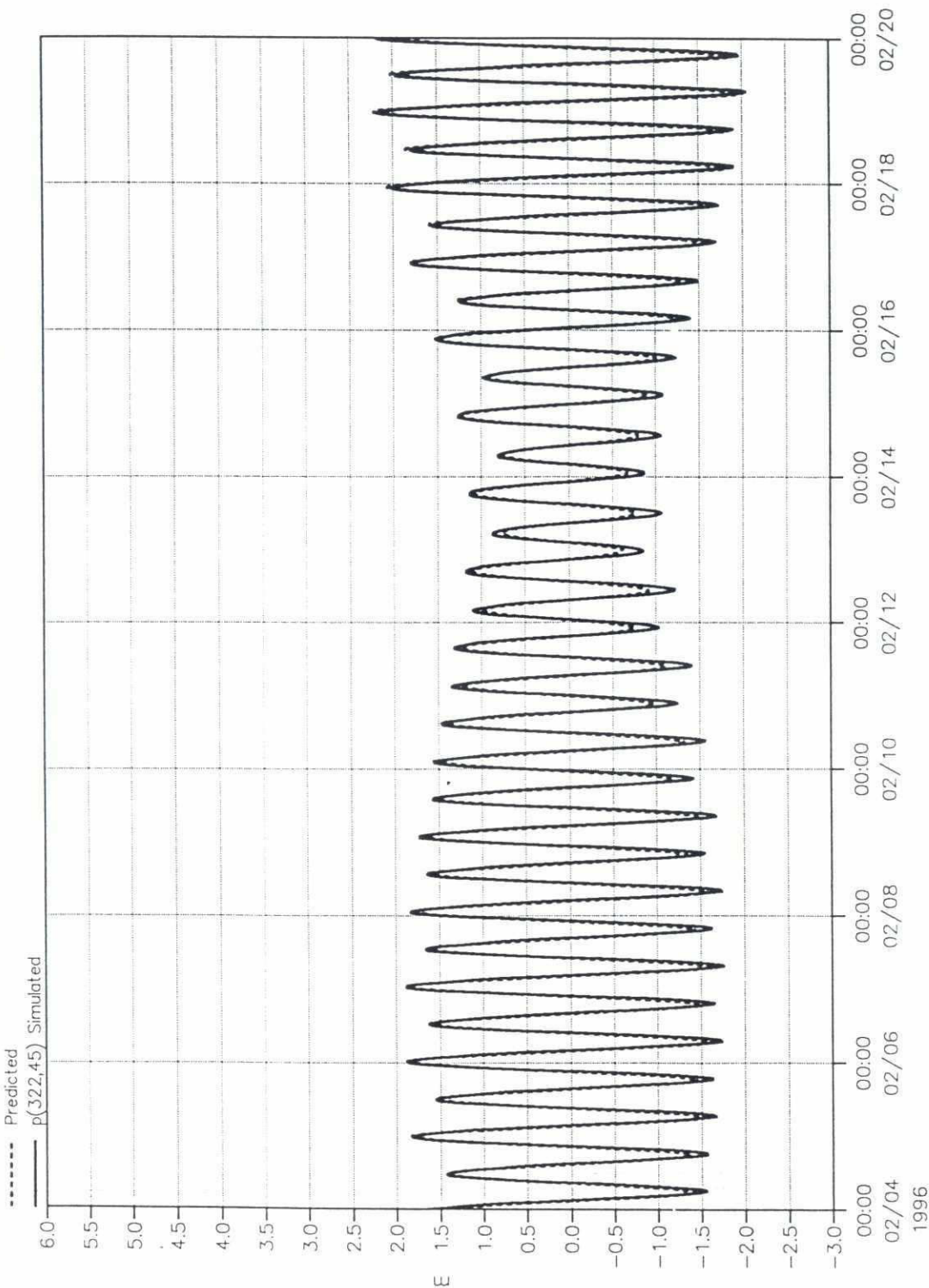
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269

261



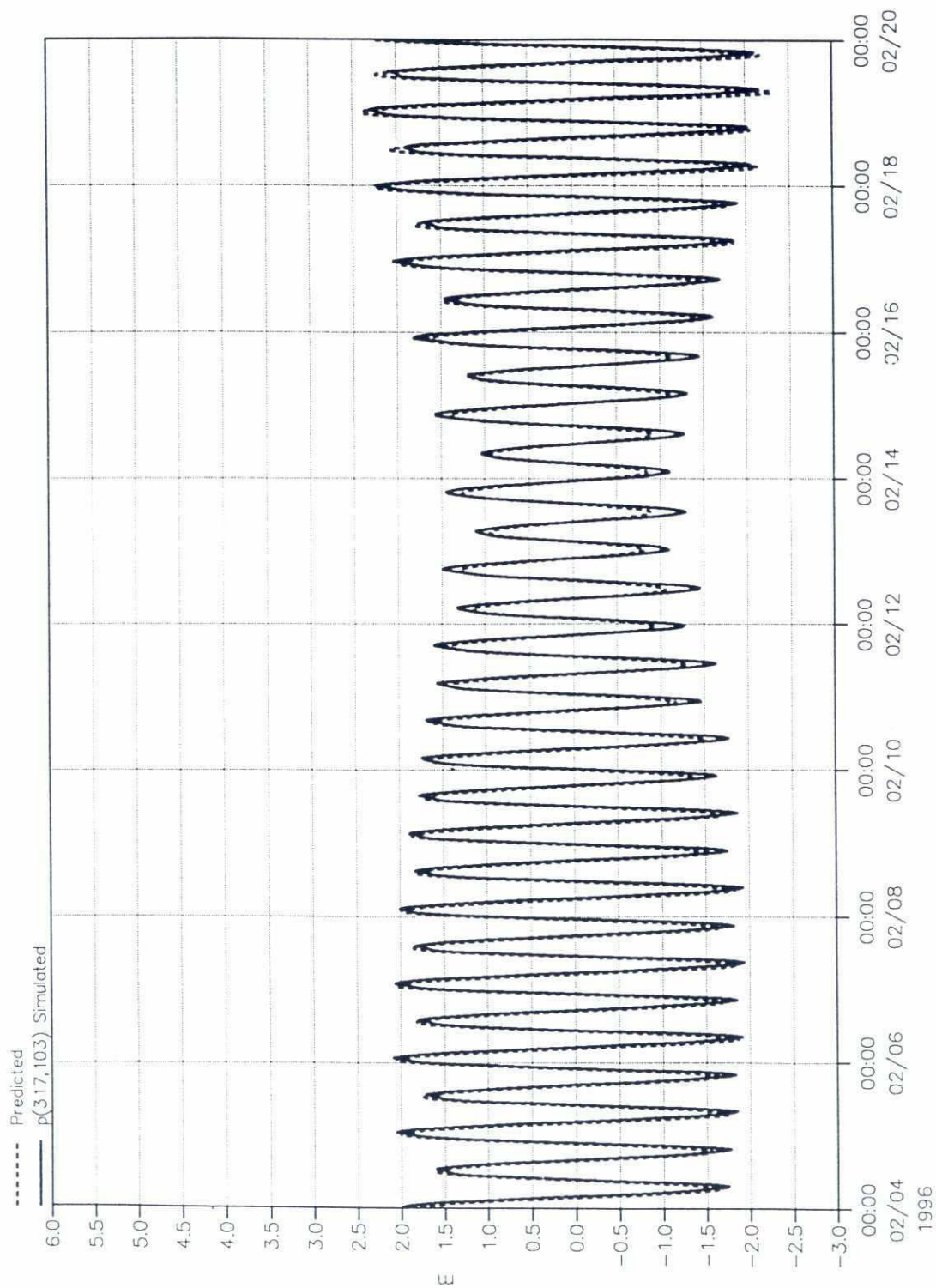
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File:	Date: Sun May 31 1998	Measured and simulated water level at Kochopia (PWD)		Drawing no. 4.16
Scale:	Unit: p5011	Dry Season 1996		



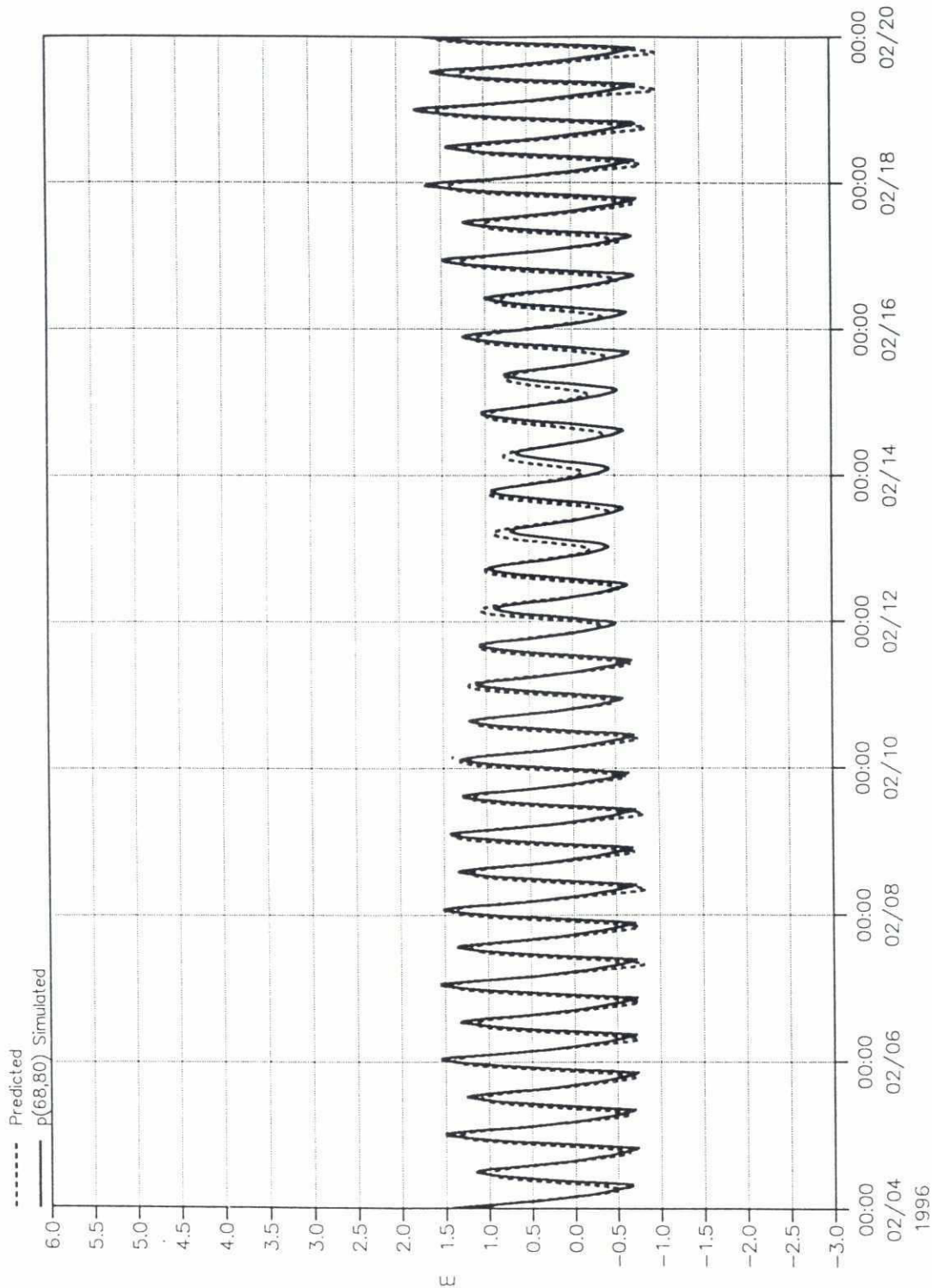
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SWMC		Client: Bangladesh Water Development Board		MIKE 21
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Scale:	Init: p5011			4.17

280

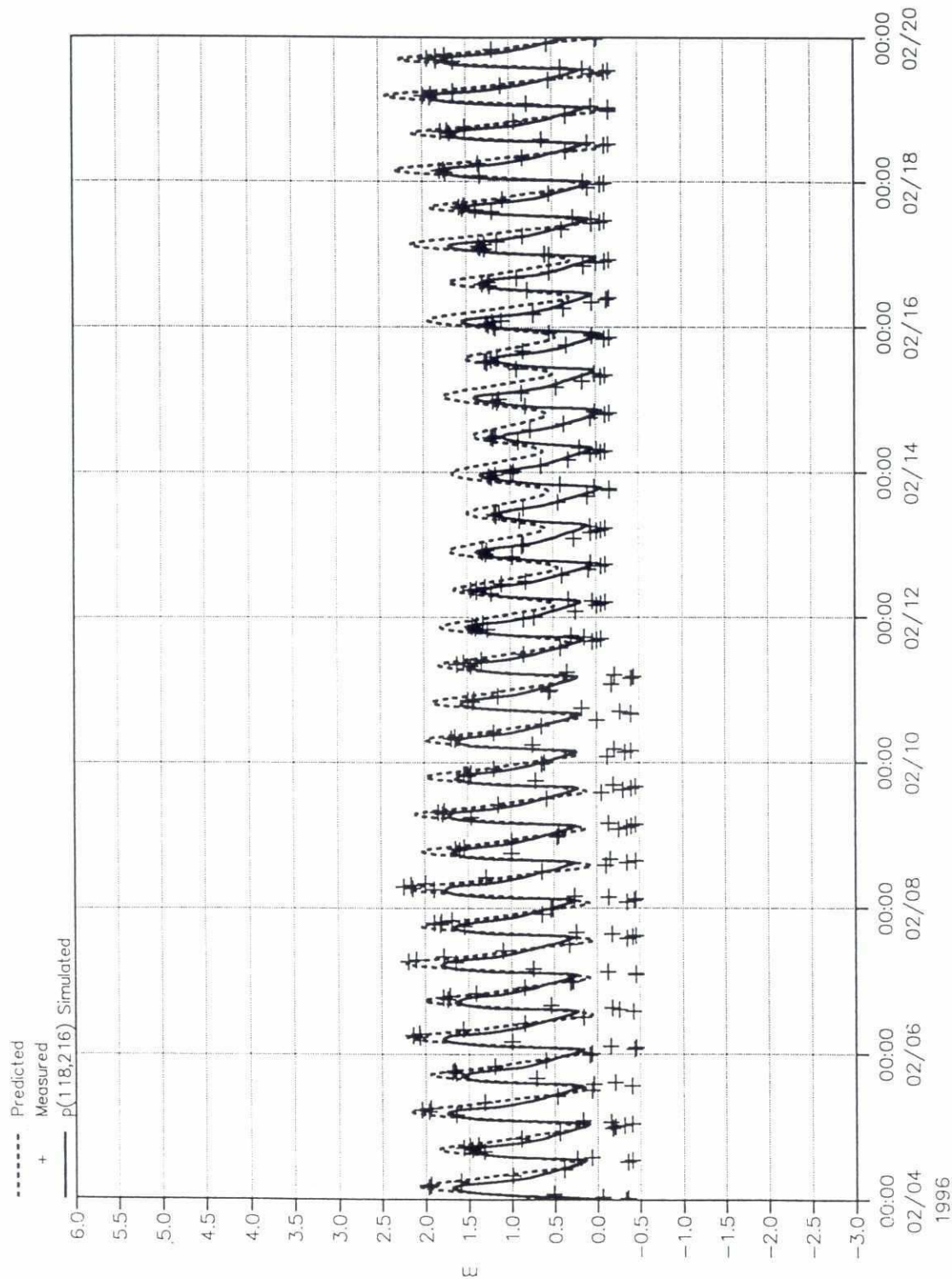


SVMC		Client: Bangladesh Water Development Board		MIKE 21
		Project: Meghna Estuary Study		
File:	Date: Sun May 31 1998	Measured and predicted water level at Normans Point (PWD) Dry Season 1996		Drawing no. 4.18
Scale:	Init: p5011			



SWMC		Client:	Bangladesh Water Development Board		MIKE 21
		Project:	Meghna Estuary Study		
File:	Date: Sun May 31 1998	Measured and predicted water level at Rabnabad Channel (PWD) Dry Season 1996		Drawing no.	
Scale:	Init: p5011			4.19	

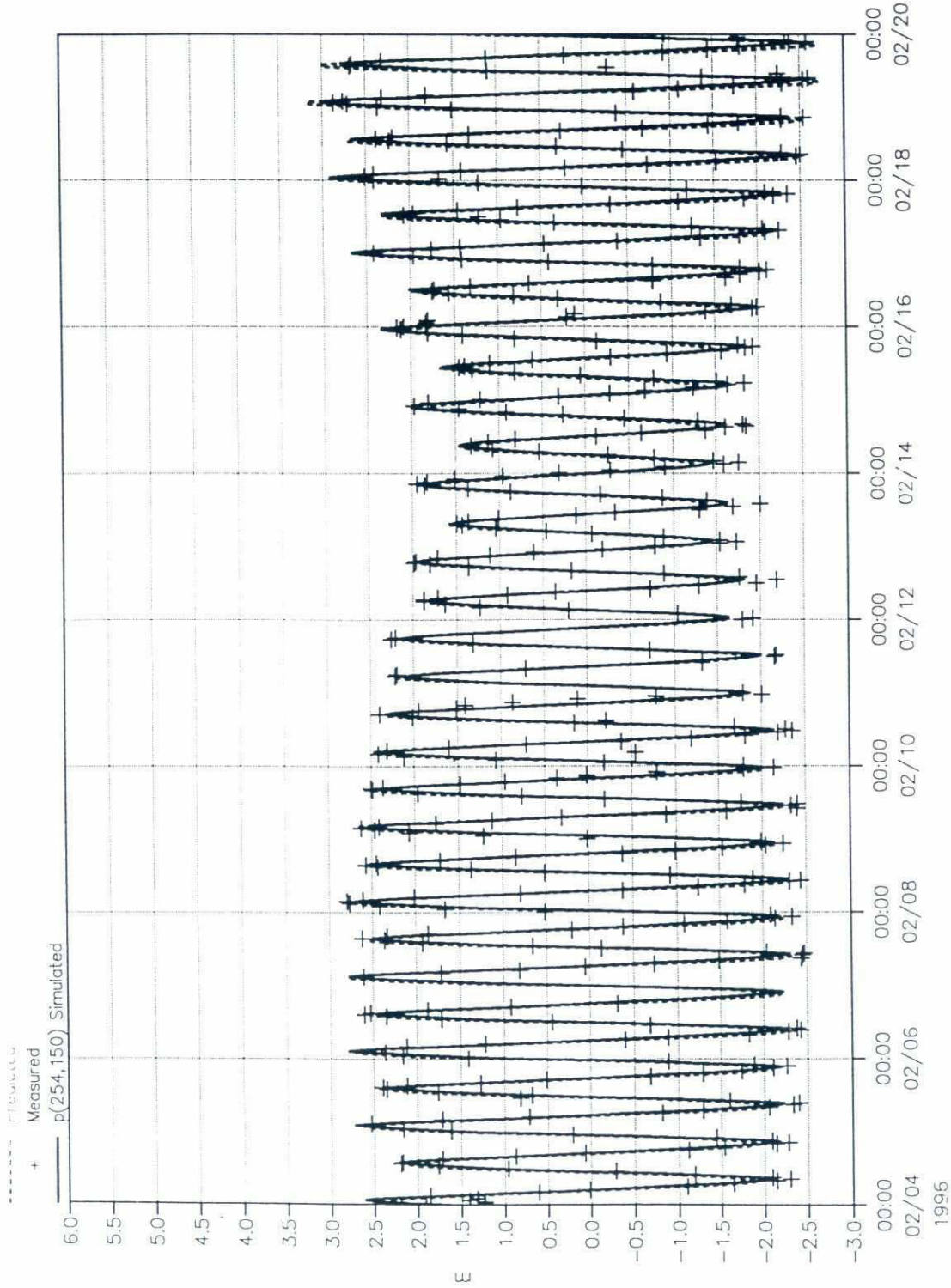
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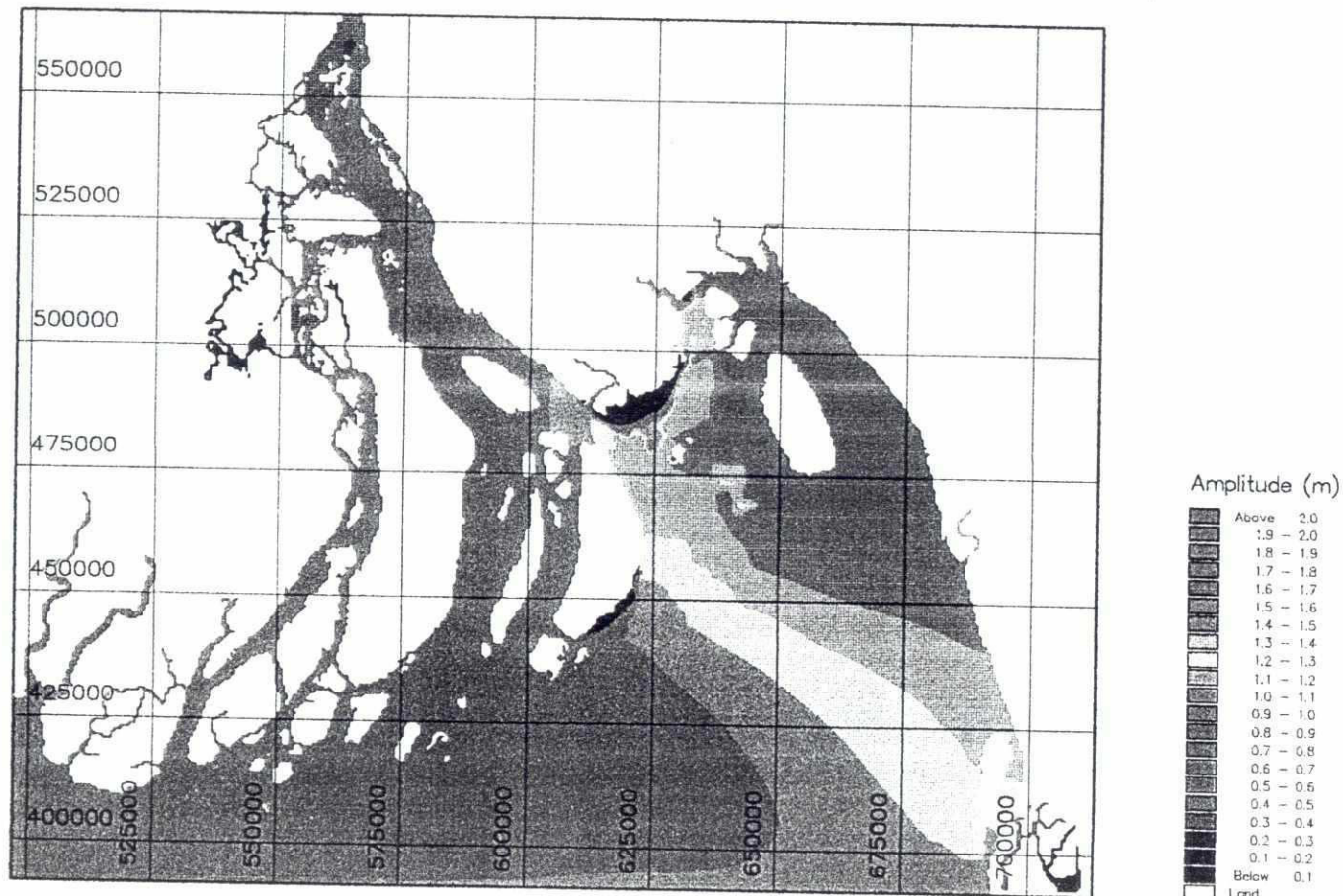
282

SWMC		Client: Bangladesh Water Development Board		Drawing no. 4.20
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File:	Date: Sun May 31 1998	Measured, simulated and predicted water level at Ramdaspur (PWD) Dry Season 1996		
Scale:	Unit: p5011			

286



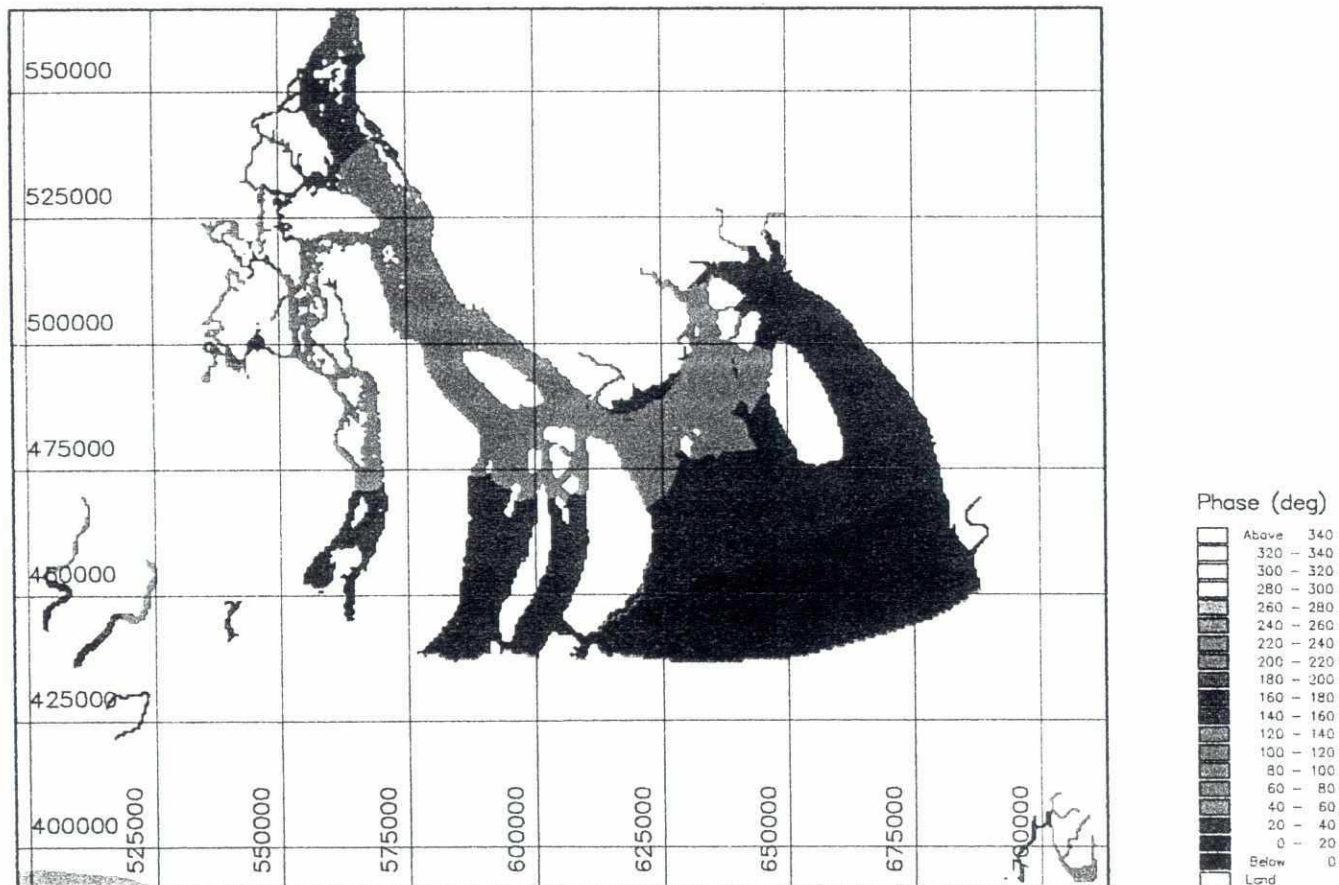
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File:	Date: Sun May 31 1998	Measured, simulated and predicted water level at Sandwip (PWD) Dry Season 1996		
Scale:	Init: p5011			
		Drawing no. 4.21		



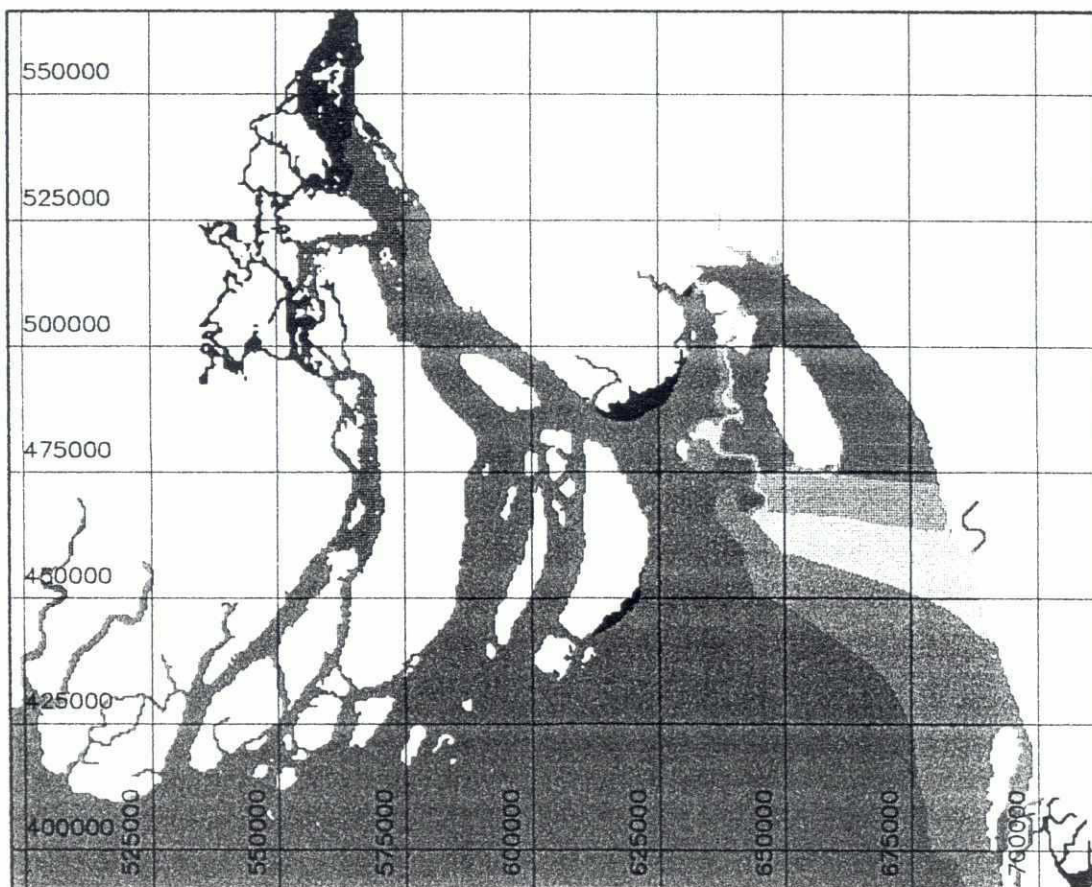
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288

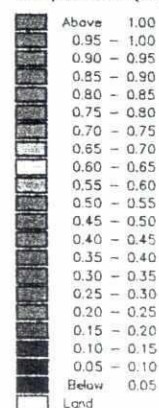
00001 36/4



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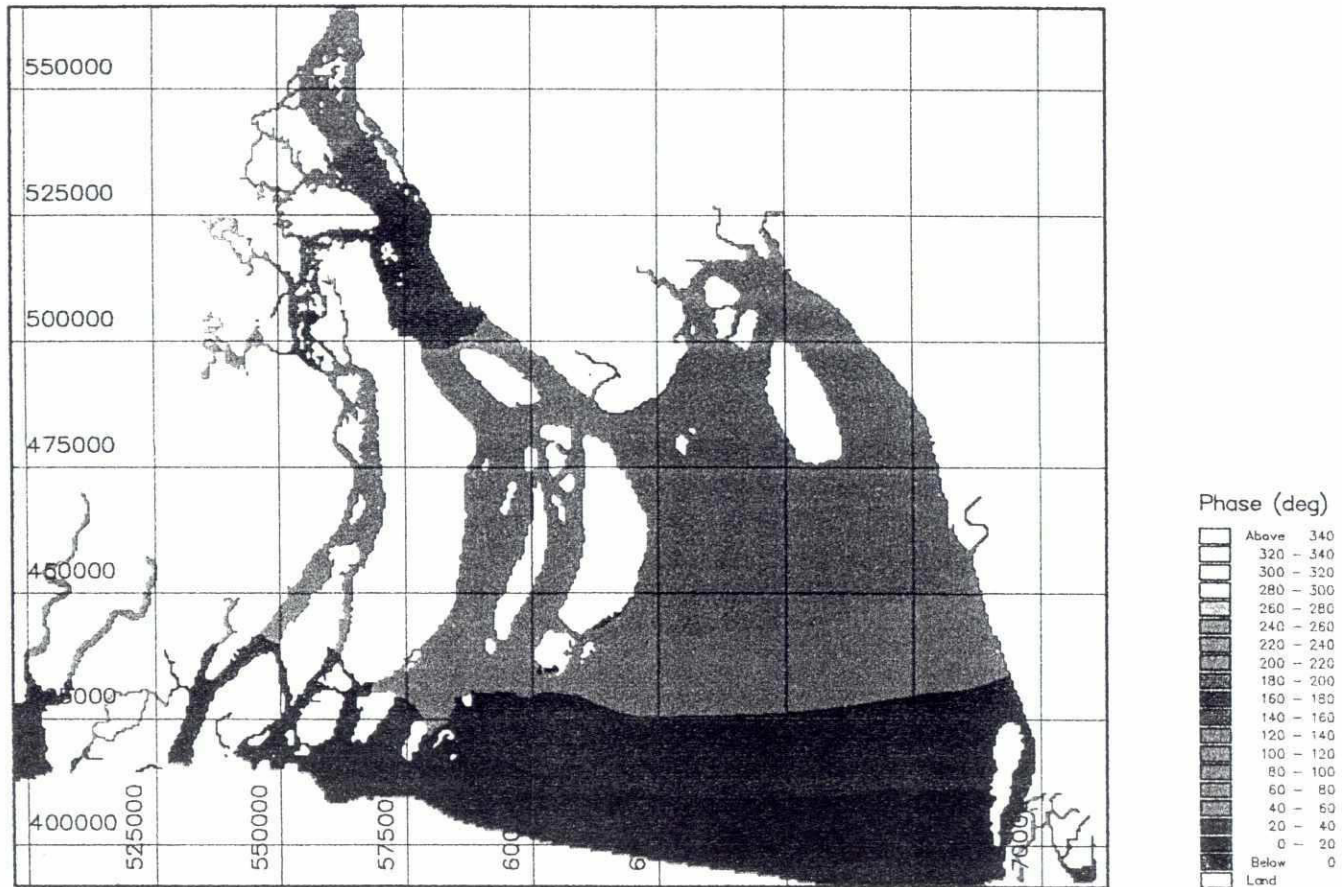
Amplitude (m)



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289

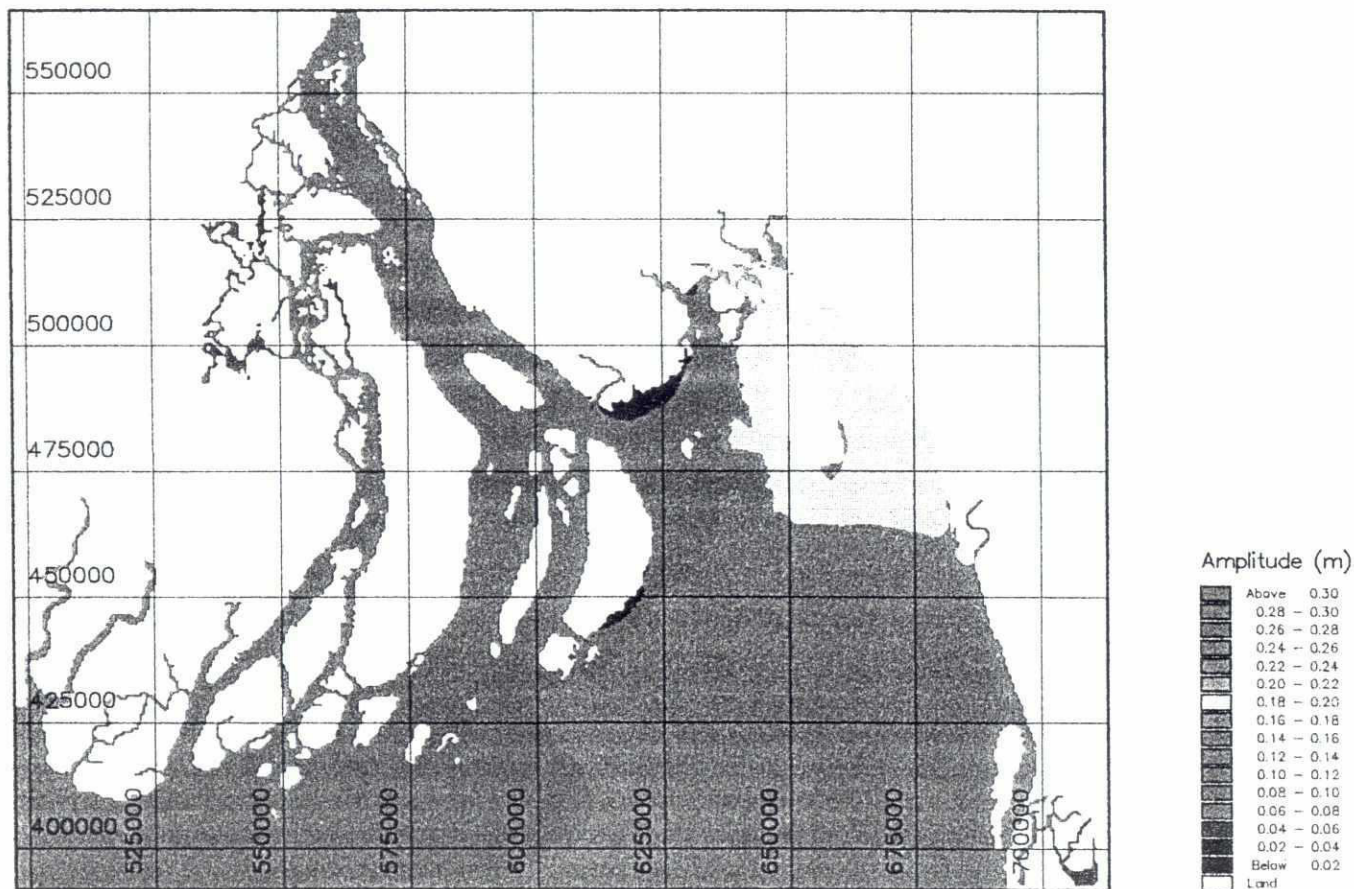
00001 96/4



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		Project:	Meghna Estuary Study	
File:	Date: Mon Jun 8 1998	Tidal analysis, Dry season 1996 S2 phase		Drawing no. 4.25
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286

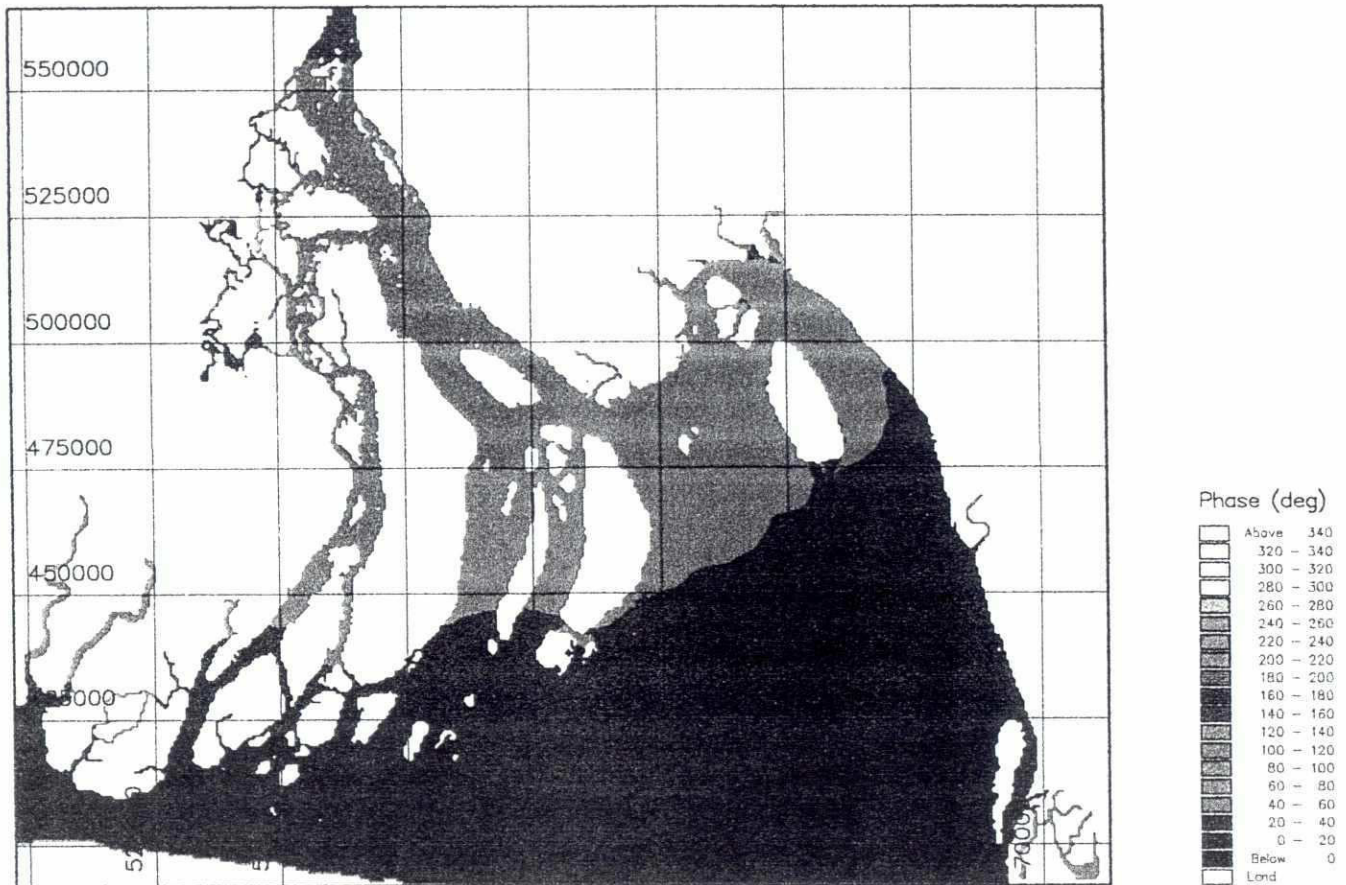
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		Project:	Meghna Estuary Study		
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280

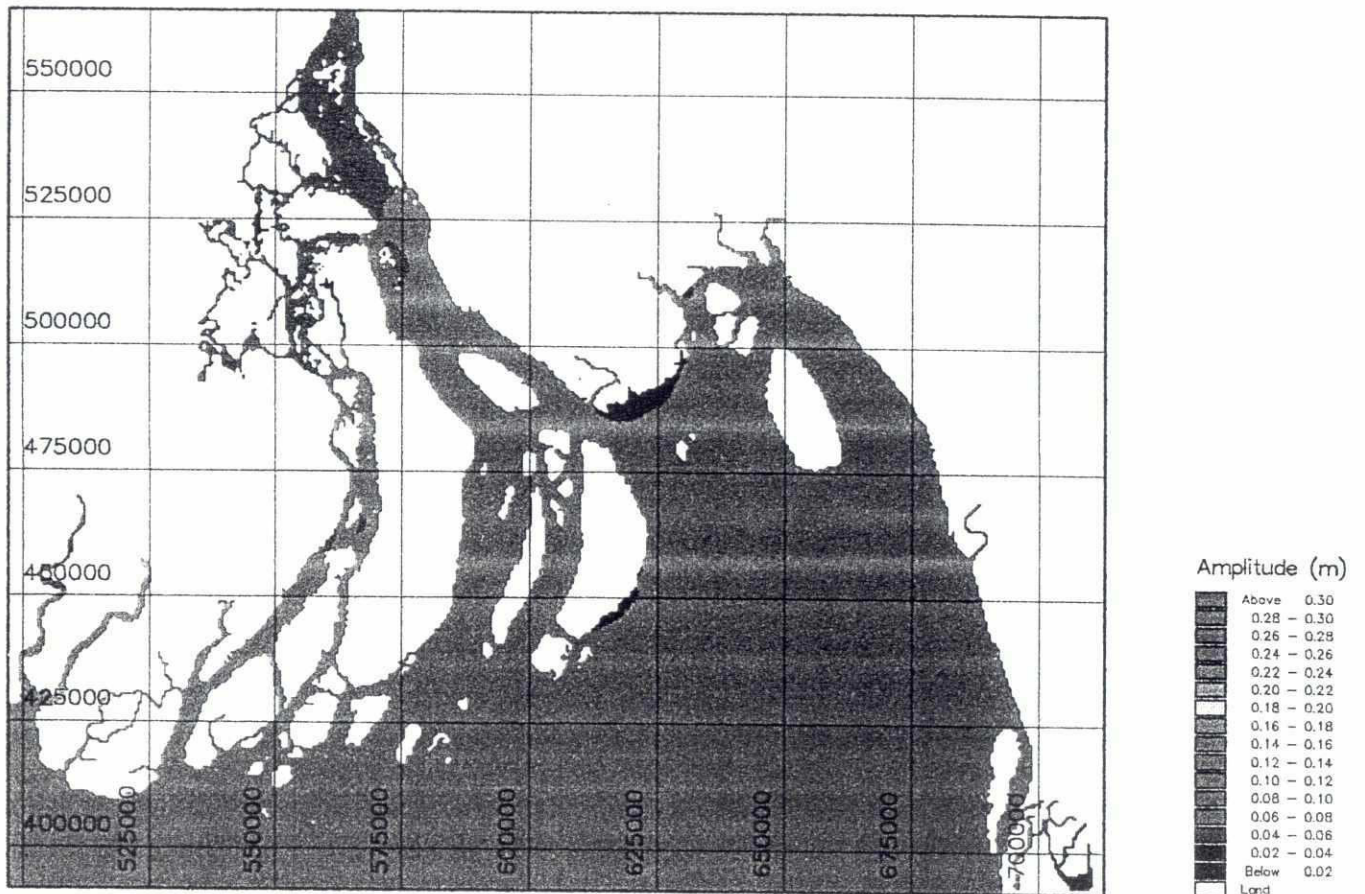
sheet 98/4



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280

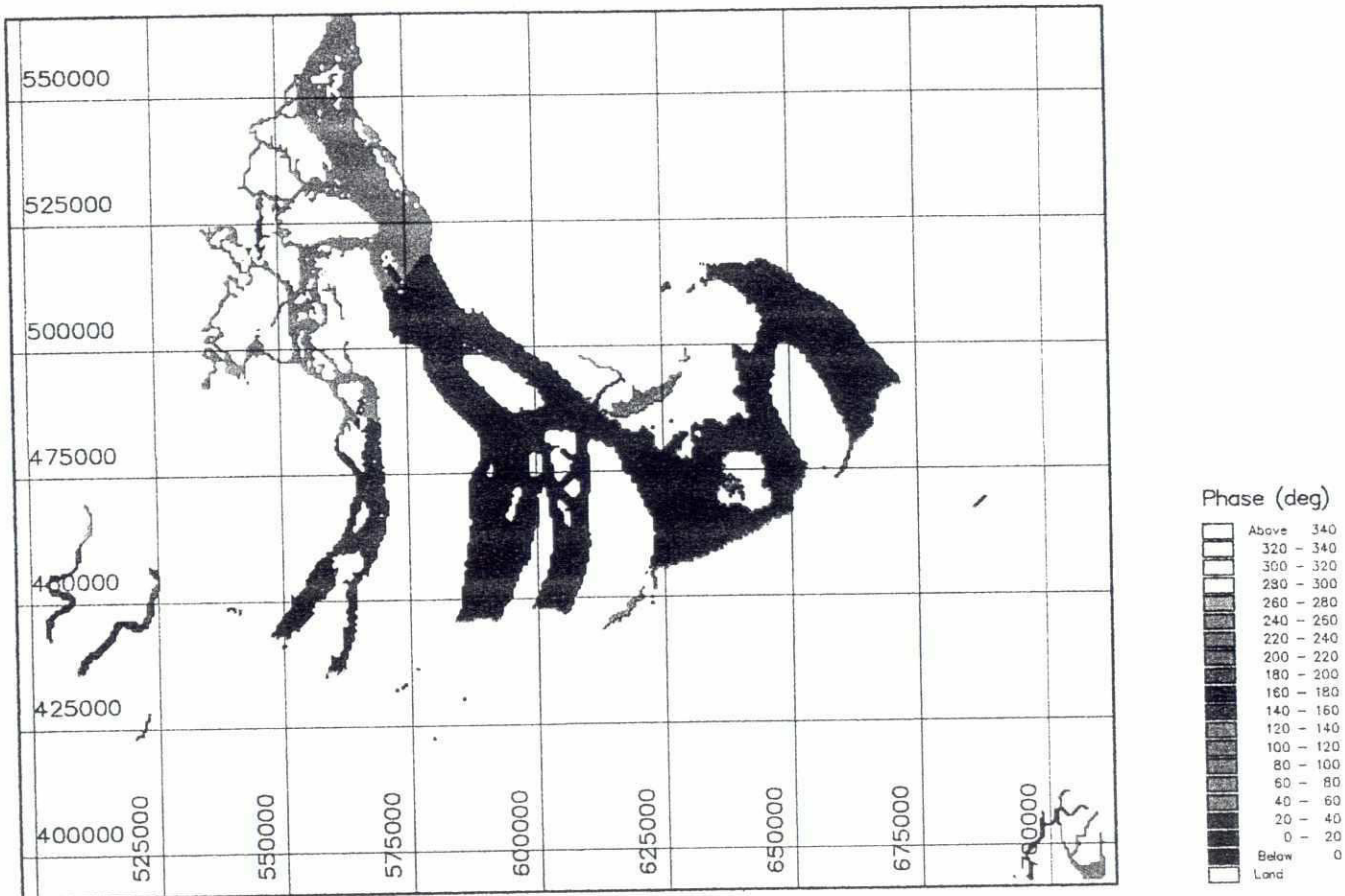
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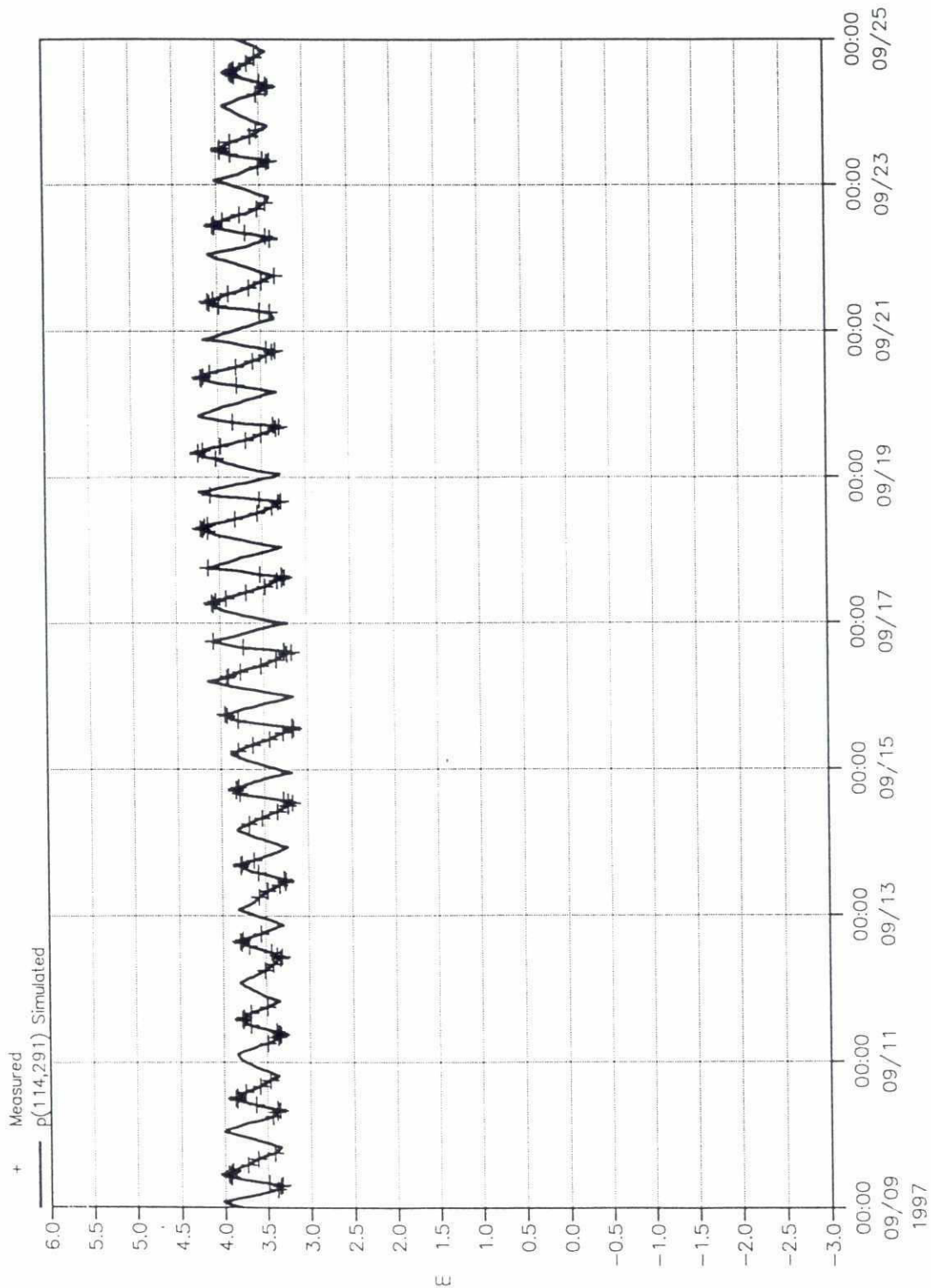
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202

U:\proj\96\44

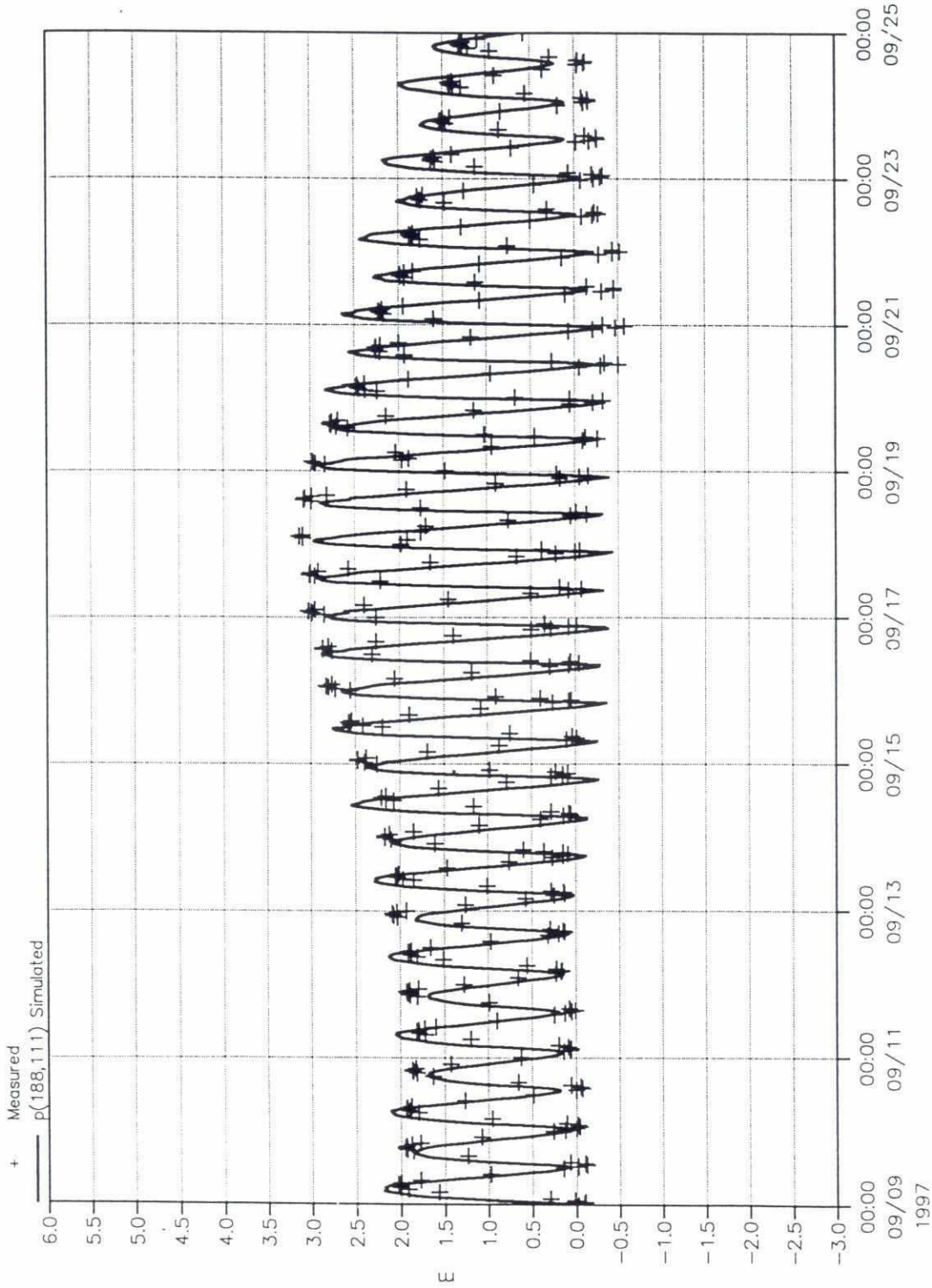


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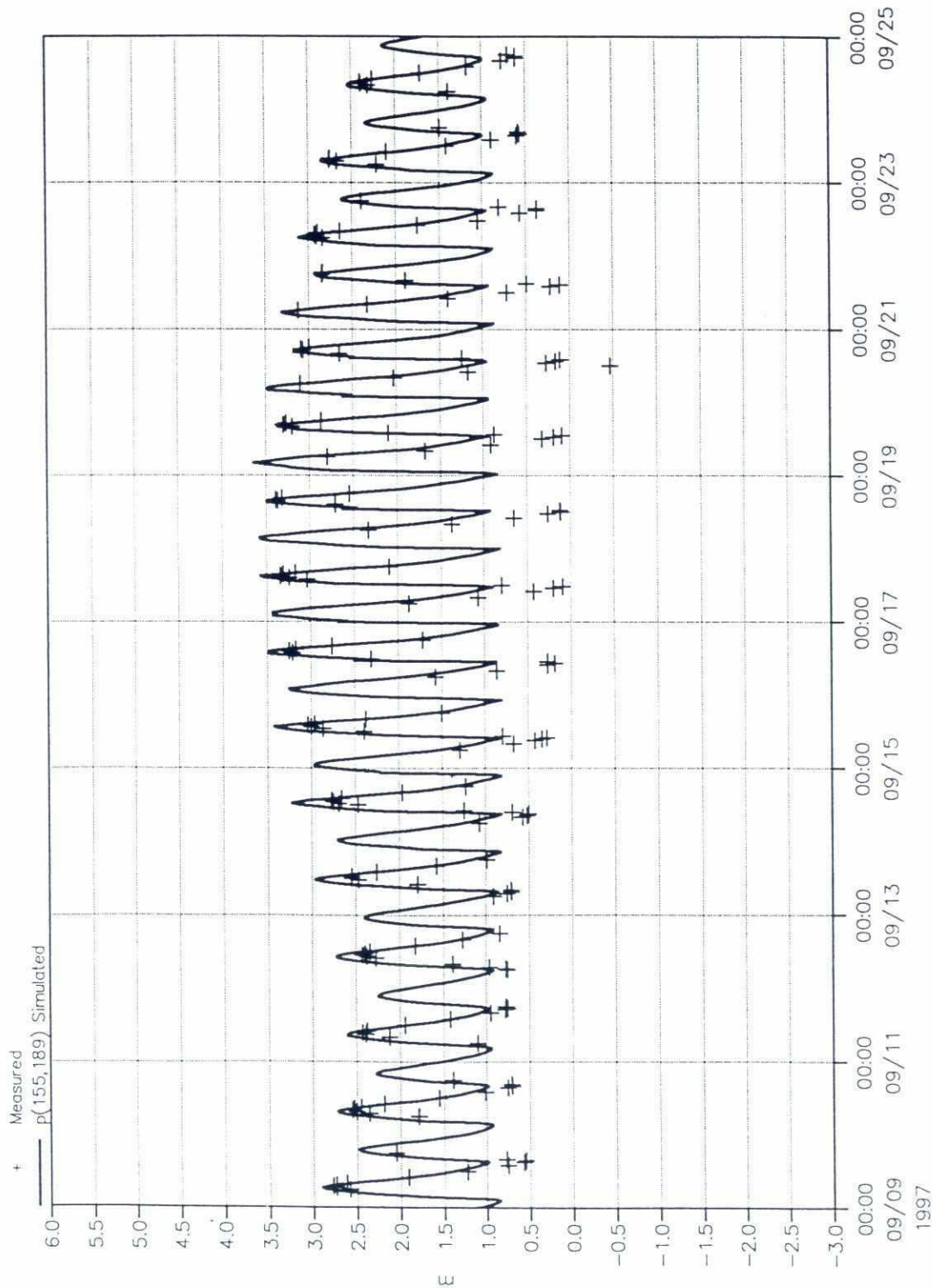
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		Project: Meghna Estuary Study	
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202

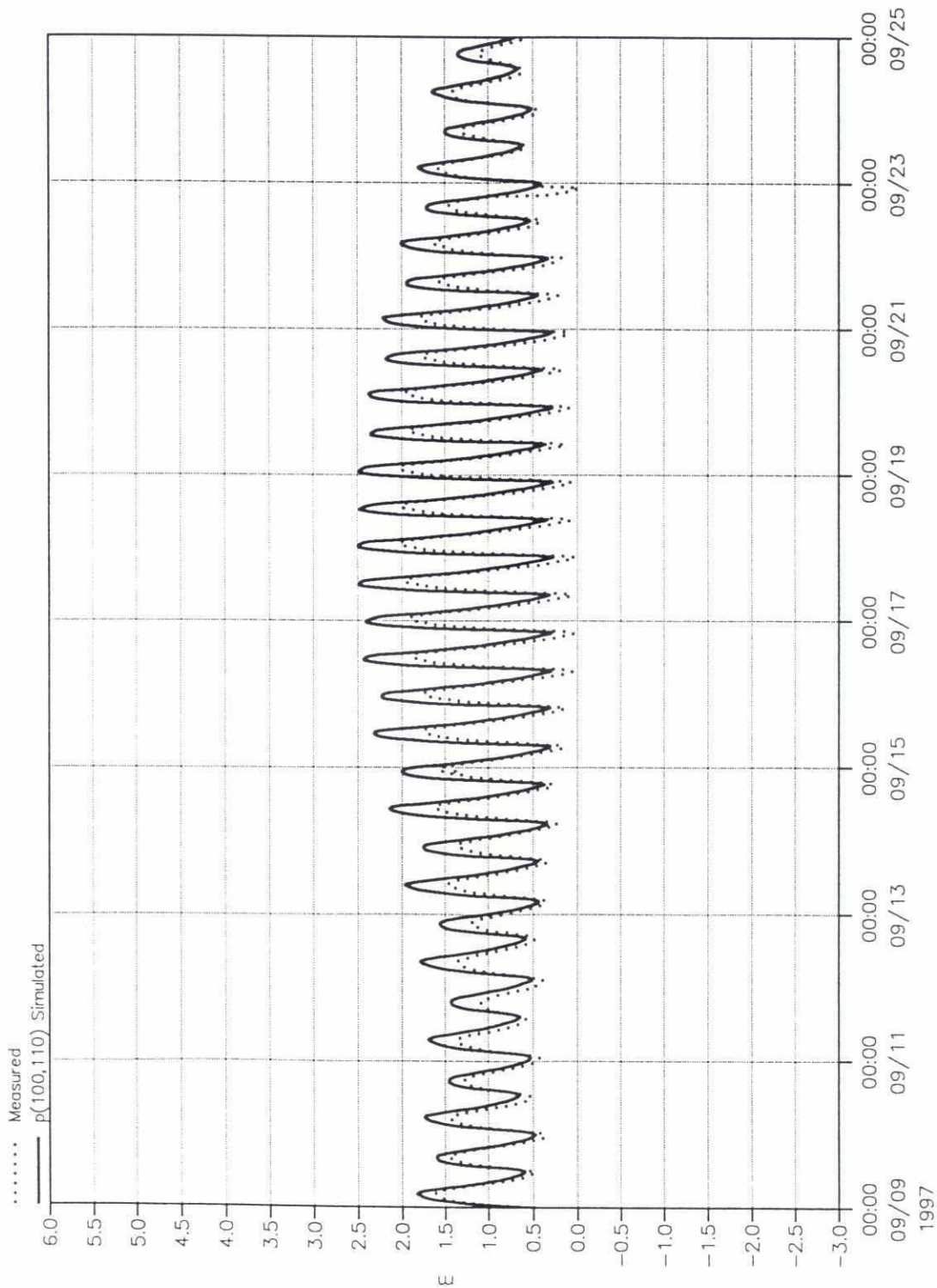


SVMC		Client: Bangladesh Water Development Board		MIKE 21
		Project: Meghna Estuary Study		
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Scale:	Init: p5011			

22



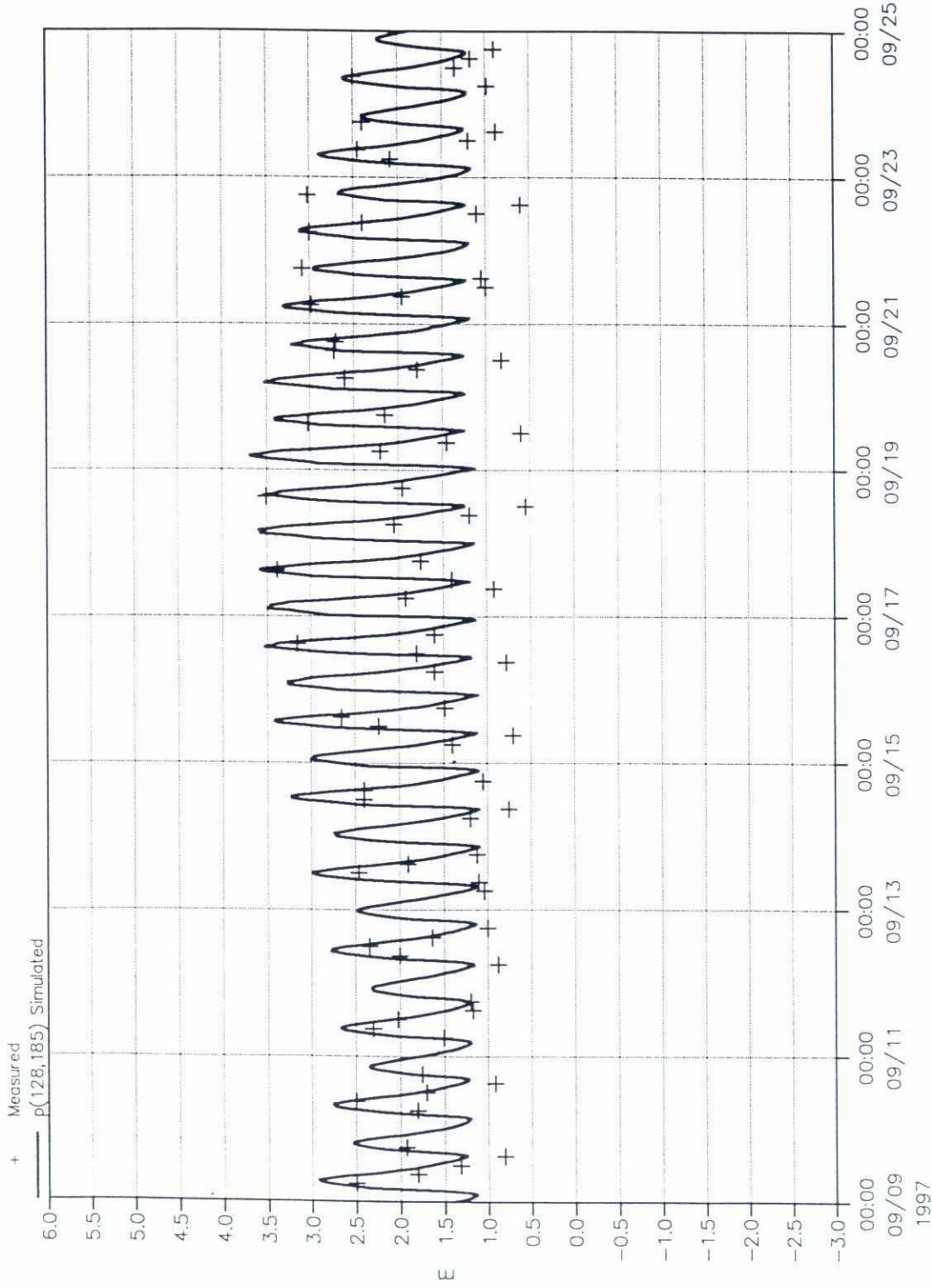
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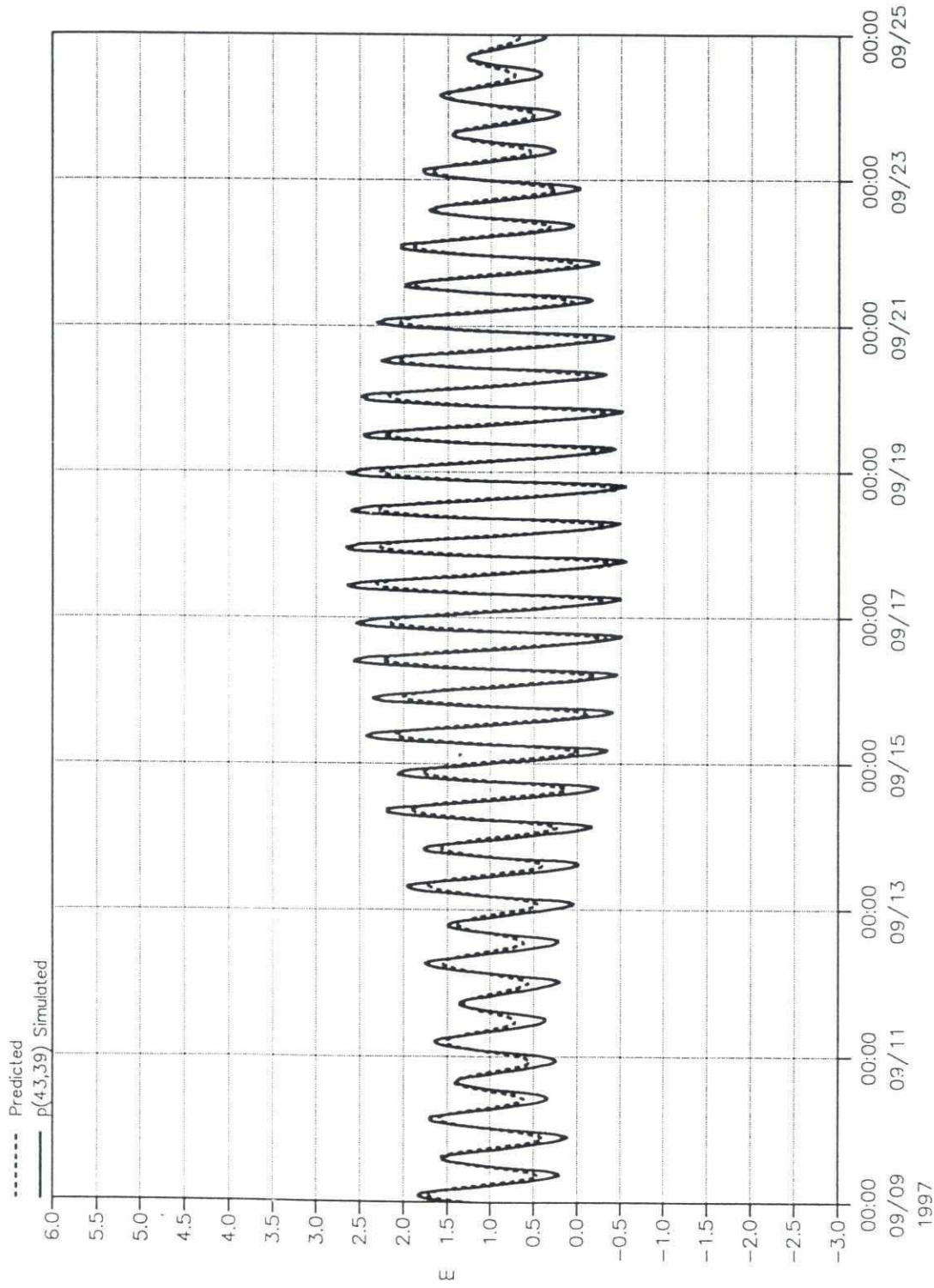
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22

203



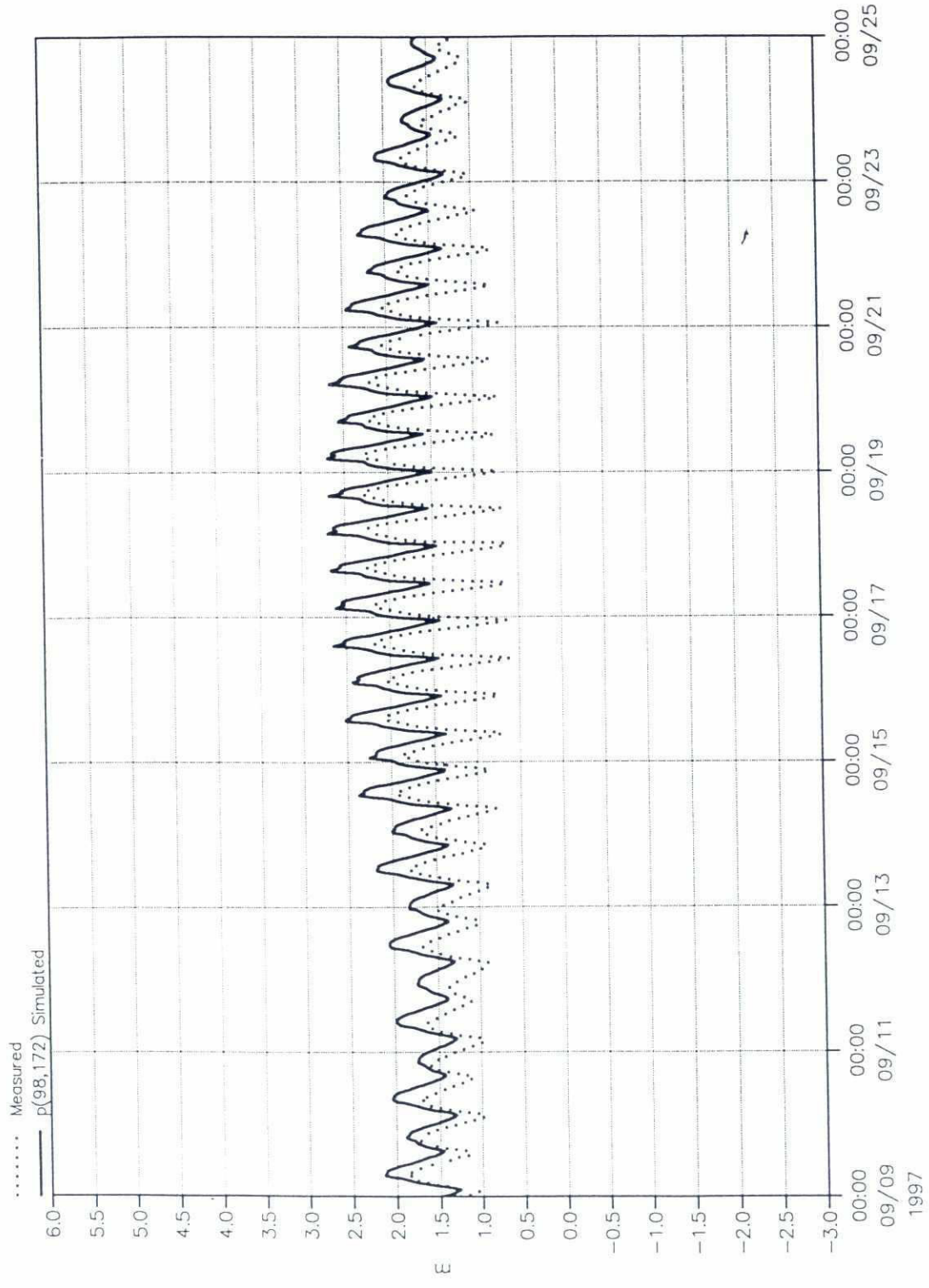
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		Project: Meghna Estuary Study		
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Scale:	Init: p5011			



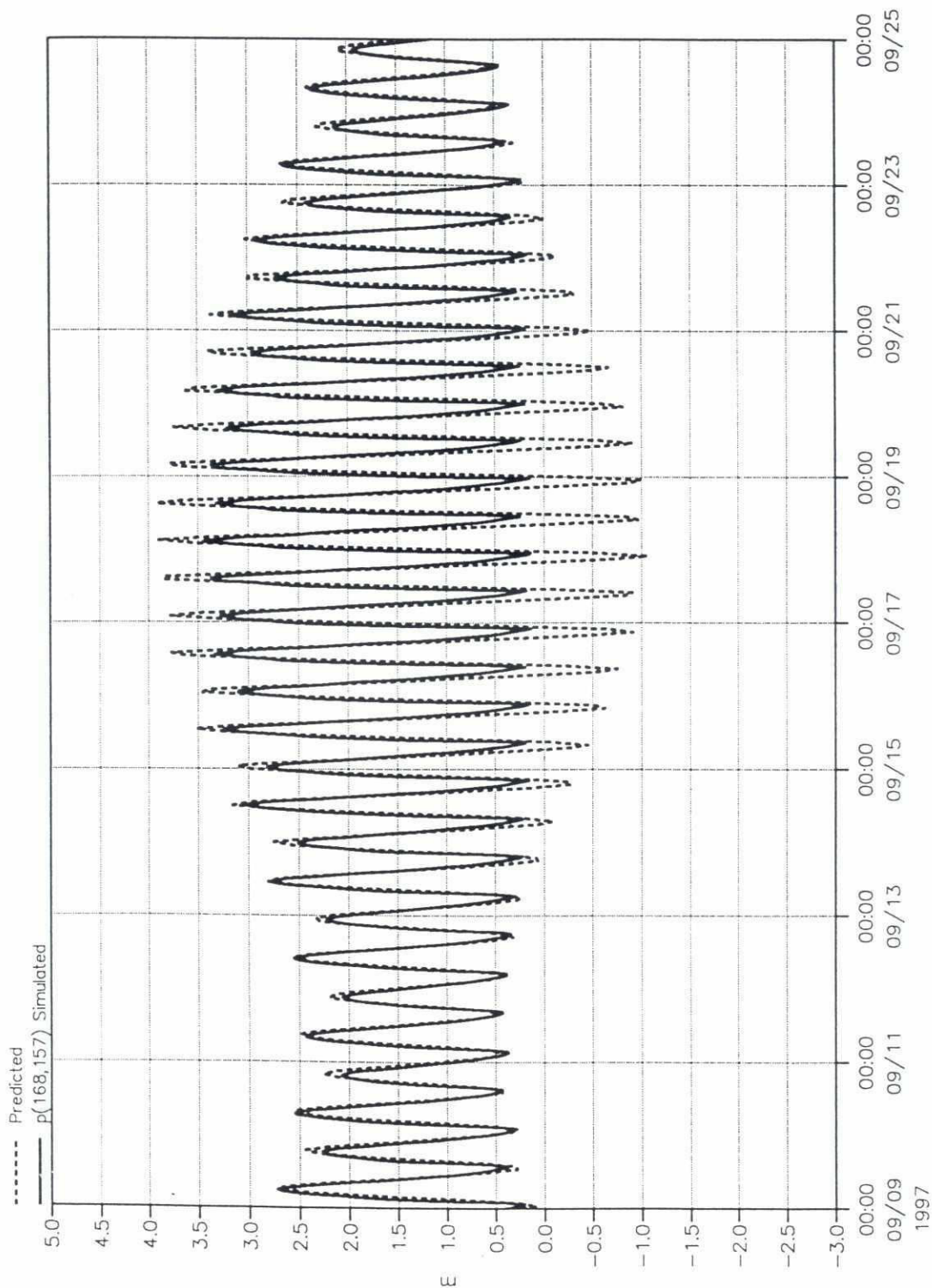
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		Project: Meghna Estuary Study		
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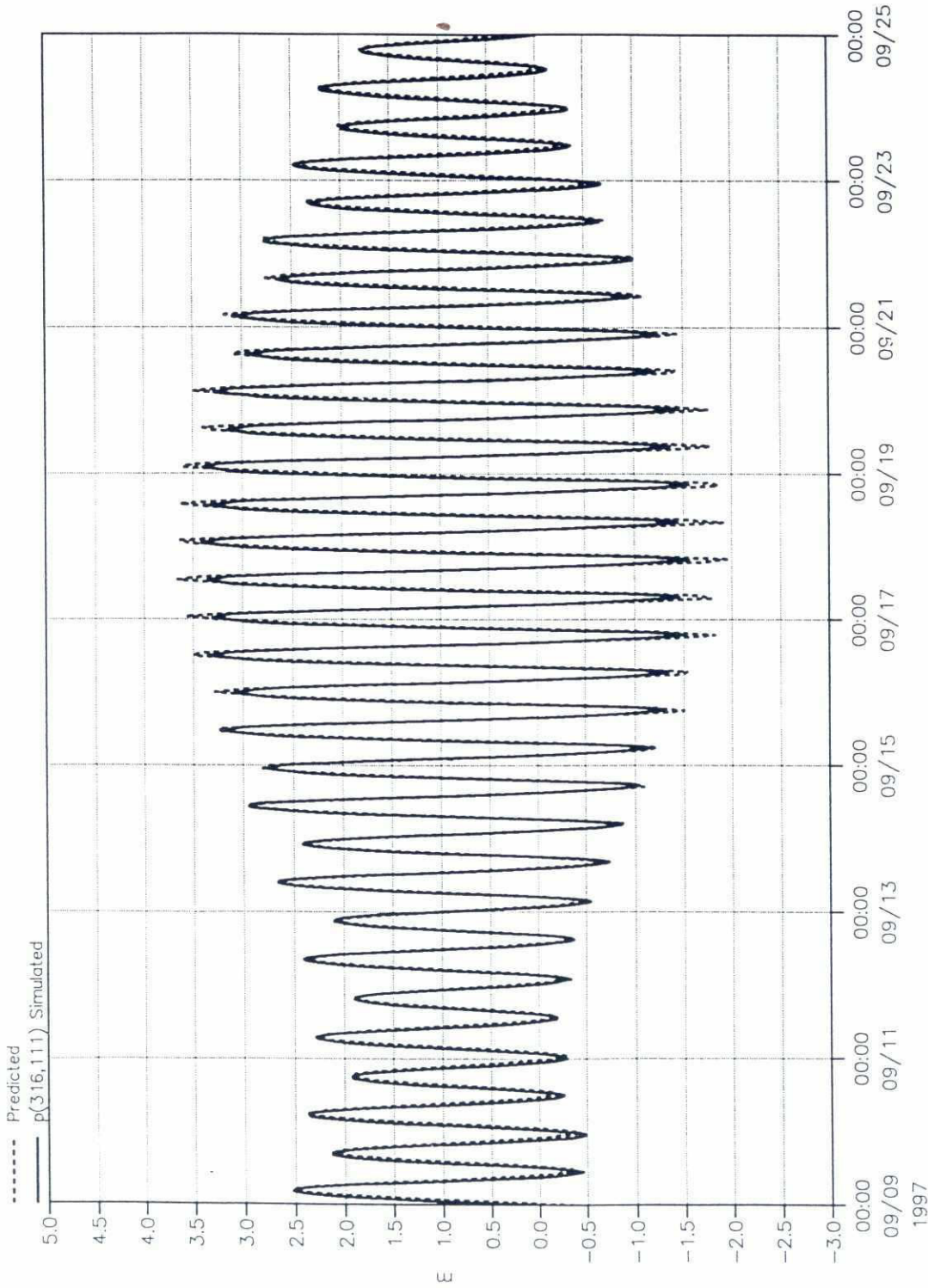
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		Project: Meghna Estuary Study		
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Scale:	Init: p5011			



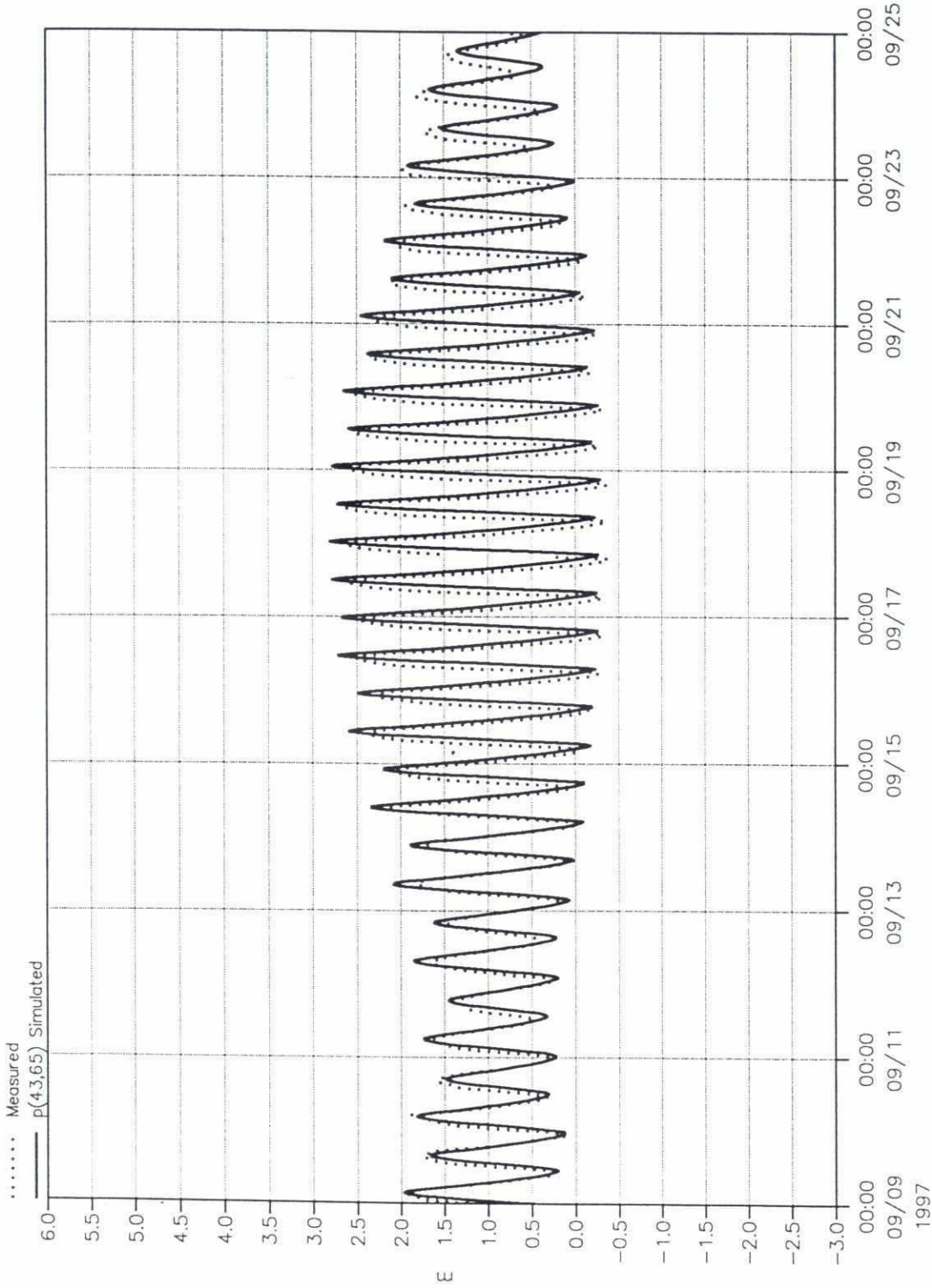
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Project: Meghna Estuary Study		Drawing no.		4.37
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22

30

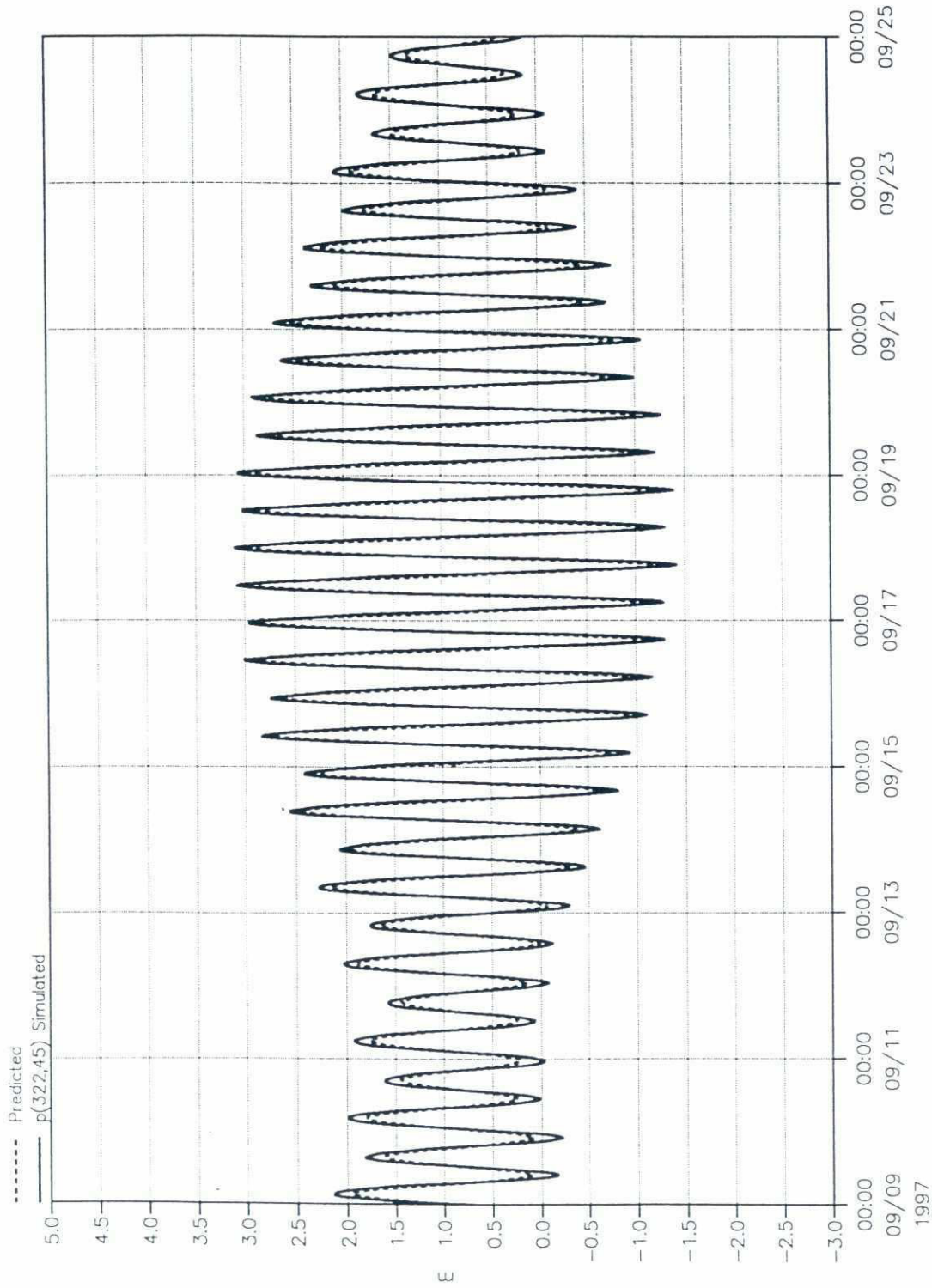


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		Project: Meghna Estuary Study		
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Scale:	Init: p5011	Monsoon season 1997		

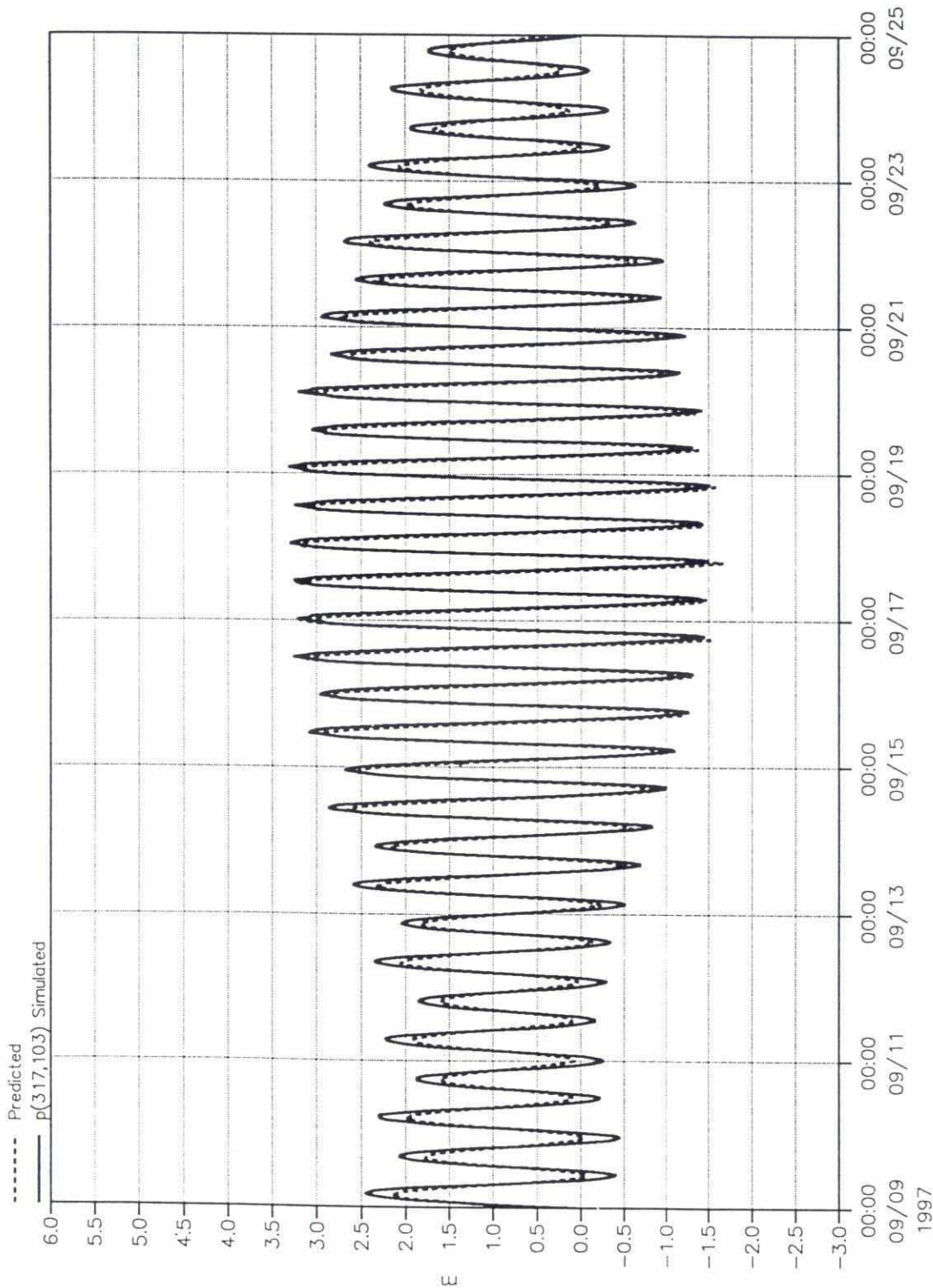


SWMC		Client: Bangladesh Water Development Board		MIKE 21
		Project: Meghna Estuary Study		
File:	Date: Sun May 31 1998	Measured and simulated water level at Khepupara (PWD)		Drawing no. 4.39
Scale:	Init: p5011			
Monsoon Season 1997				

132

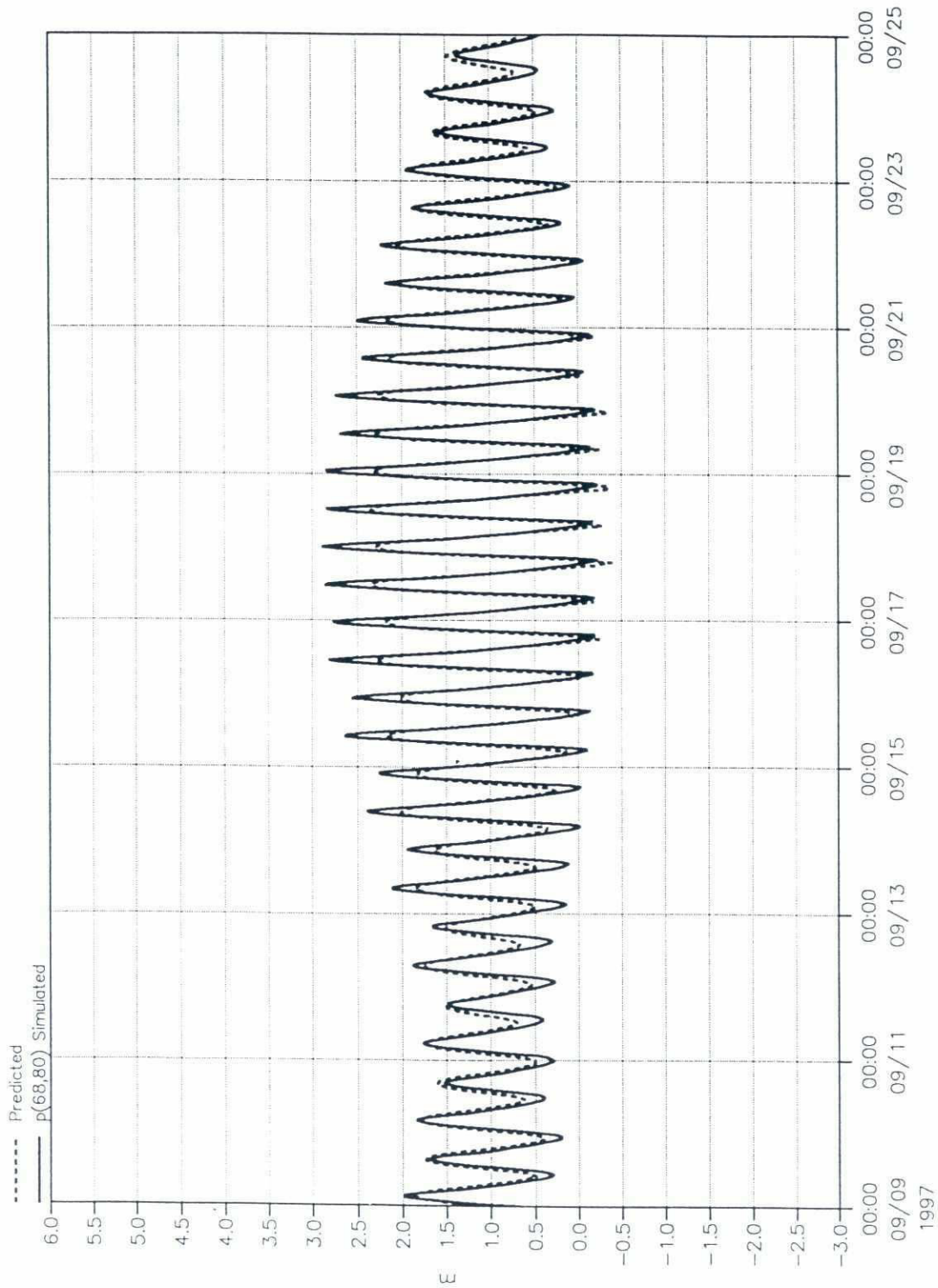


SVMC		Client: Bangladesh Water Development Board		MIKE 21
		Project: Meghna Estuary Study		
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Scale:	Init: p5011			

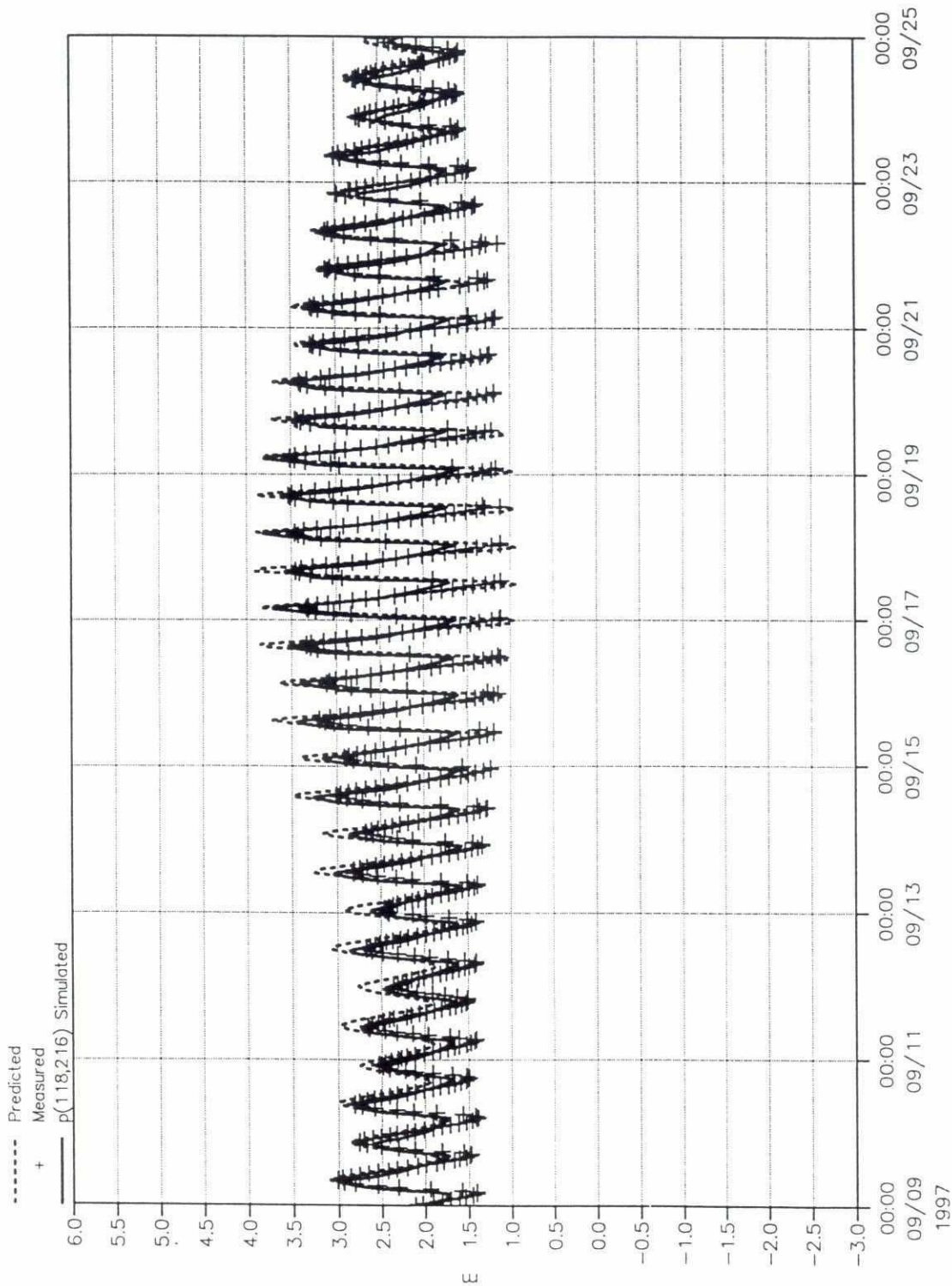


SWMC		Client: Bangladesh Water Development Board		MIKE 21
Project: Meghna Estuary Study		Drawing no. 4.41		
File:	Date: Sun May 31 1998	Measured and predicted water level at Normans Point (PWD)		
Scale:	Init: p5011	Monsoon Season 1997		

838

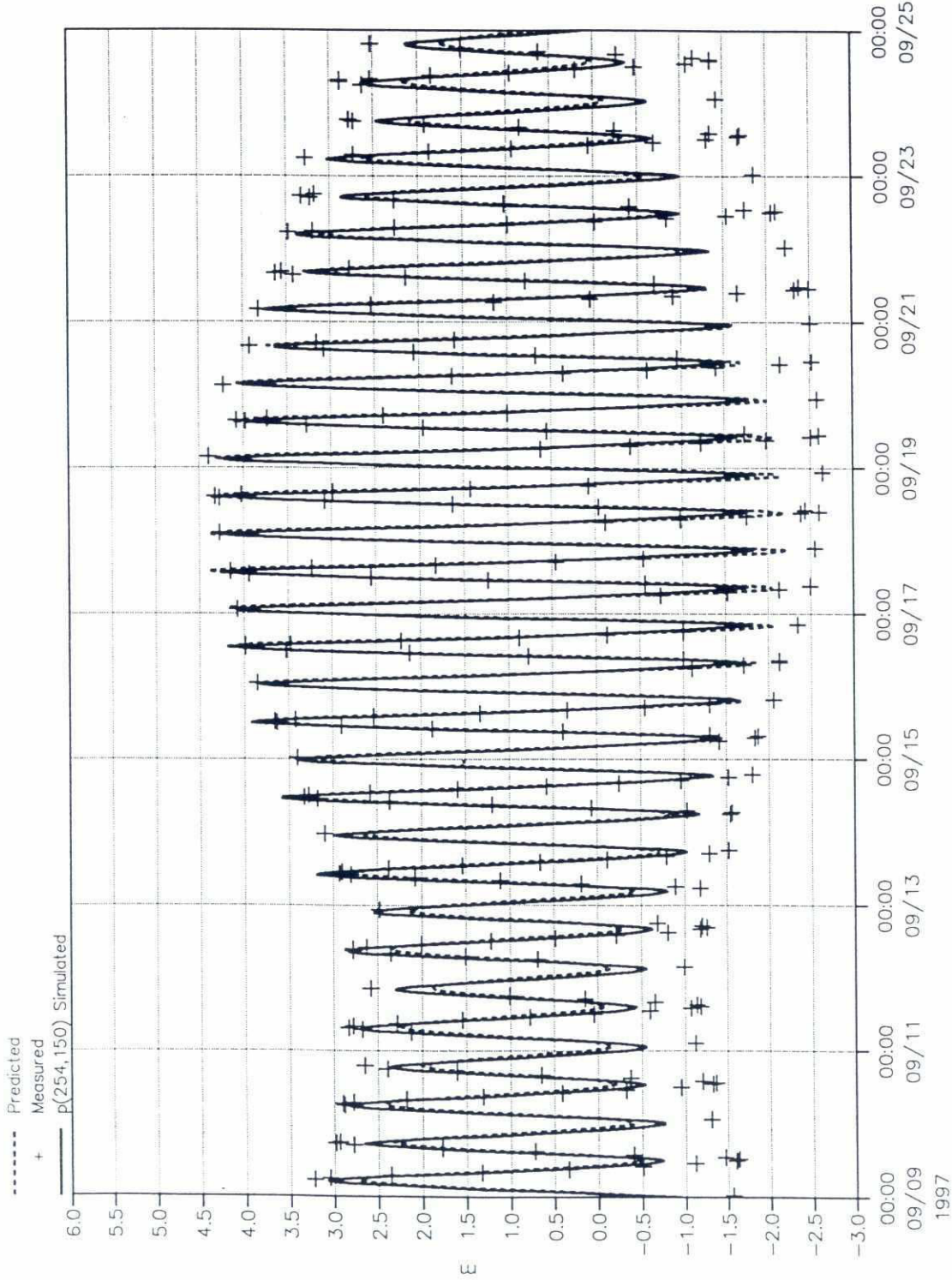


SWMC		Client: Bangladesh Water Development Board		MIKE 21
		Project: Meghna Estuary Study		
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Scale:	Init: p5011			

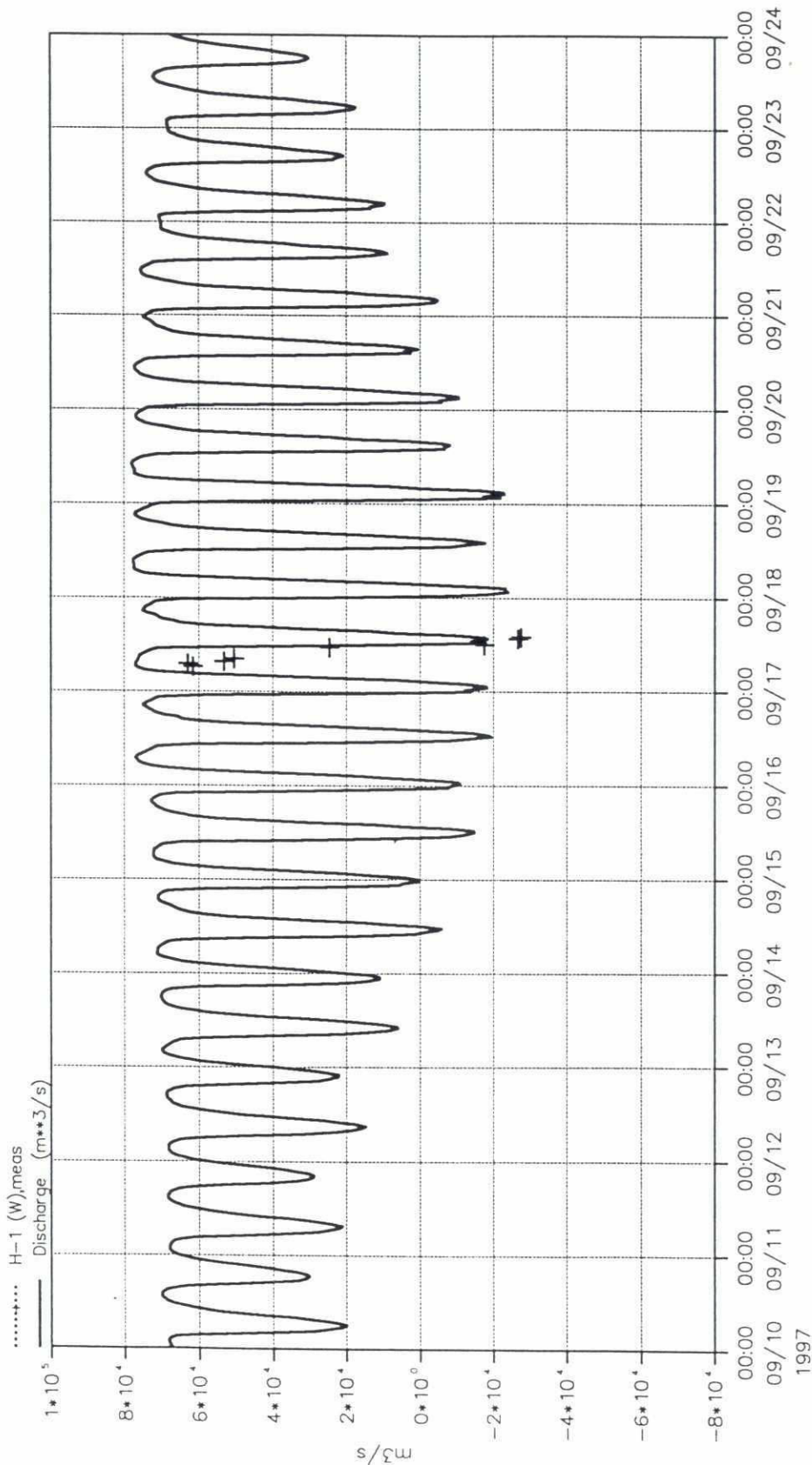


SWMC		Client: Bangladesh Water Development Board		MIKE 21
		Project: Meghna Estuary Study		
File:	Date: Sun May 31 1998	Measured, simulated and predicted water level at Ramdaspur (PWD) Monsoon Season 1997		Drawing no. 4.43
Scale:	Init: p5011			

23/9



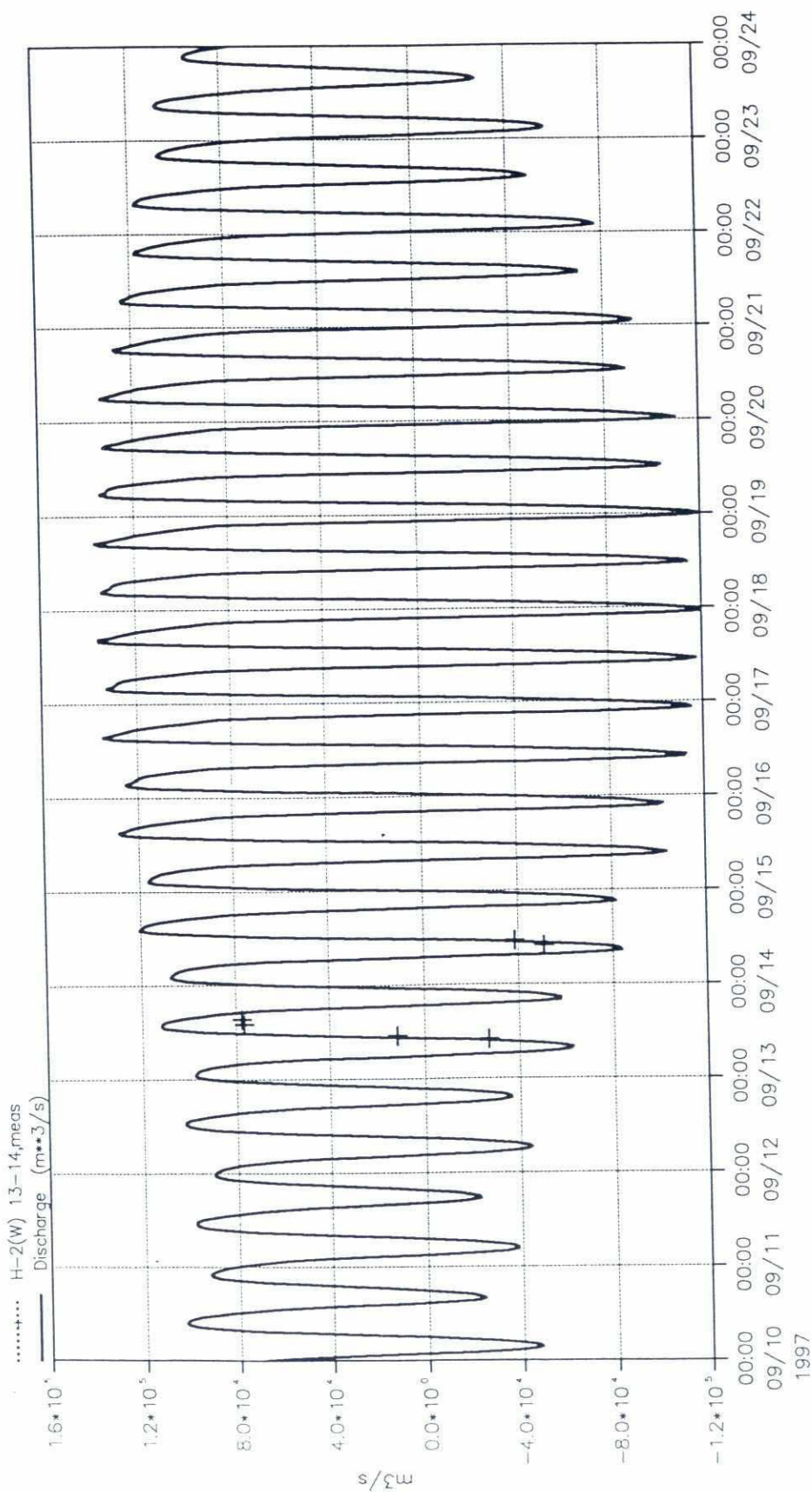
SWMC		Client: Bangladesh Water Development Board		MIKE 21	
Date: Sun May 31 1998		Project: Meghna Estuary Study		Drawing no.	
File:		Measured, simulated and predicted water level at Sandwip (PWD)		4.44	
Scale: Init: p5011		Monsoon Season 1997			



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SWMC		Client:	Bangladesh Water Development Board		MIKE 21
		Project:	Meghna Estuary Study		
File:	Date: Mon Apr 27 1998	H-1 (West) Bhola to Char Gazaria 17 September 1997		Drawing no.	4.45
Scale:	Init: p5011				

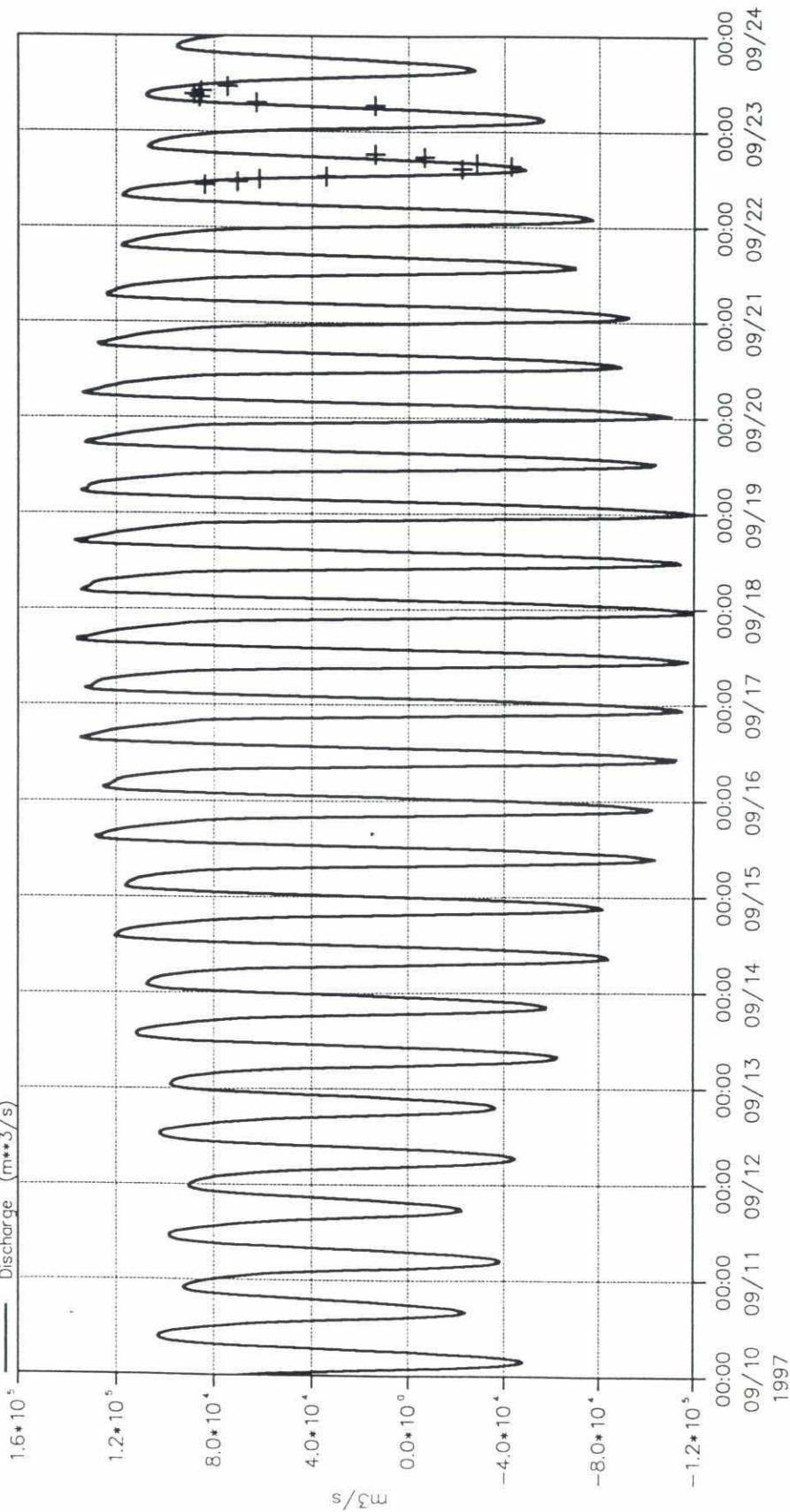
236



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	Project: Meghna Estuary Study		
File:	Date: Mon Apr 27 1998	H-2 (New West) Bhola to Manpura 13-14 September 1997	
Scale:	Init: p5011		

07 Sept-2000
meas097 H-2(W)1314
meas097 H-2(E)2122
meas097 H-2(New E)
meas097 H-2(W)1314
meas097 H-2(W)2223
meas097 H-2

..... H-2(W) 22-23, meas
Discharge (m^3/s)

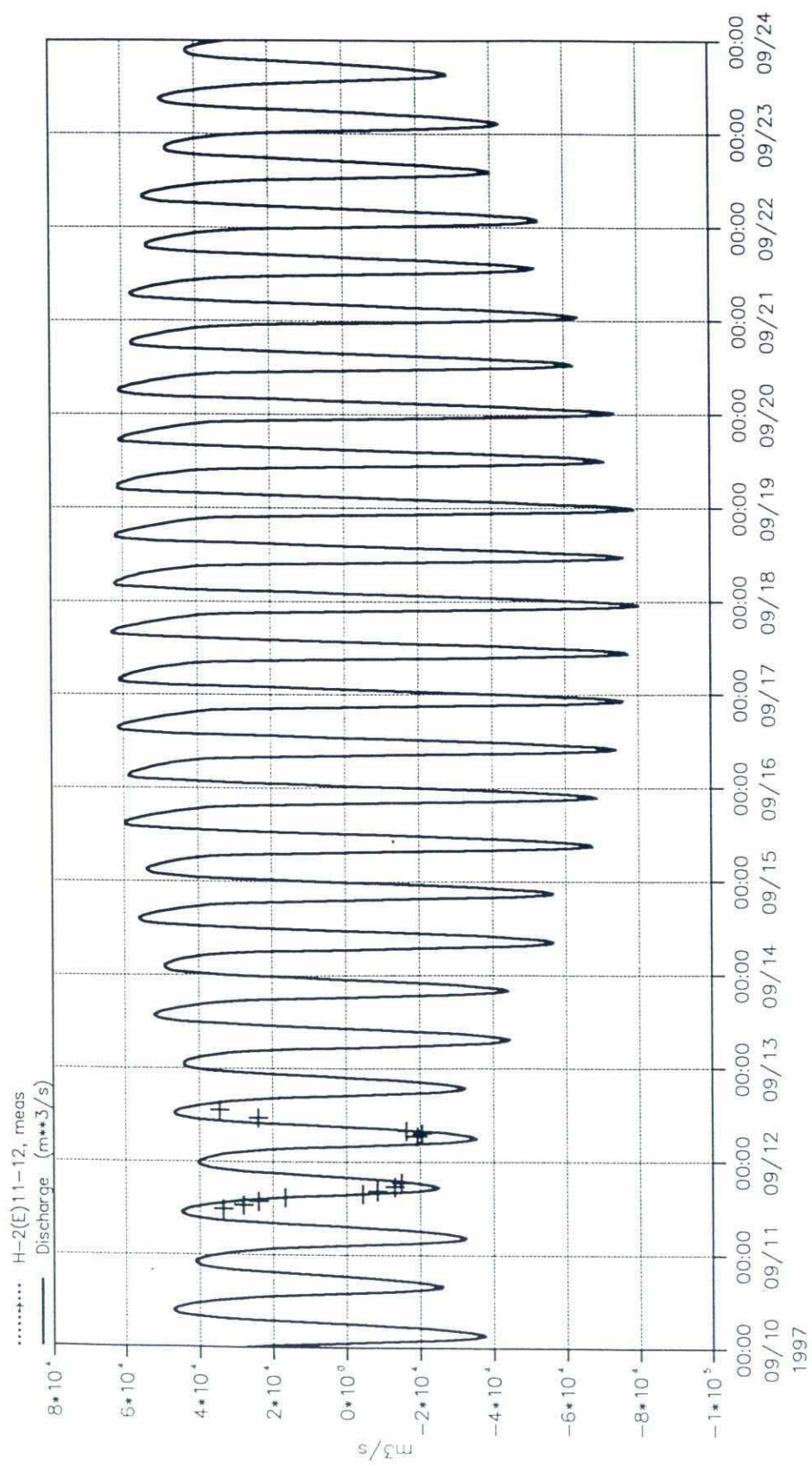


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Scale:	Init: p5011	Bhola to Manpura		4.47
		22-23 September 1997		

23

290

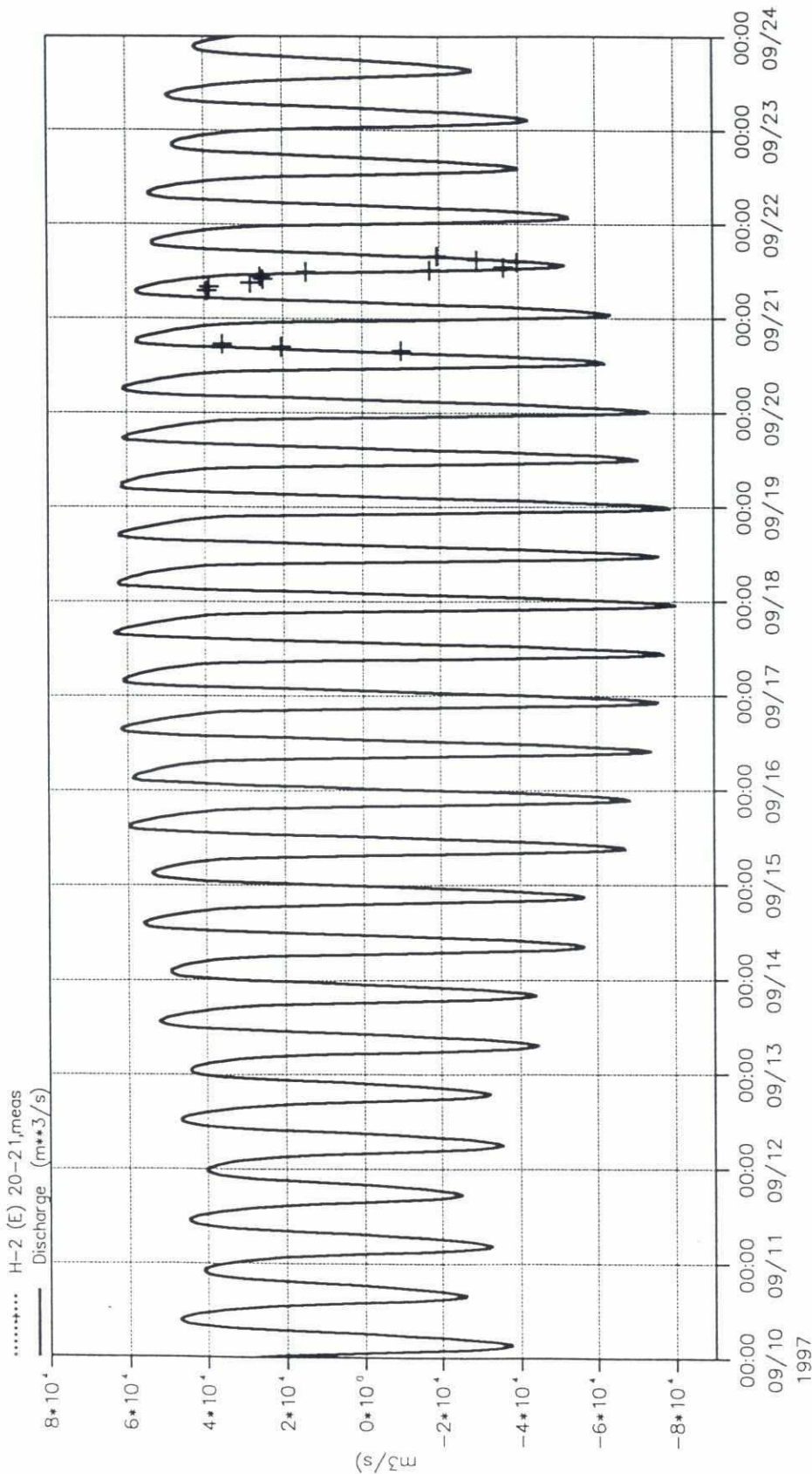
097 SETH-2EN
097 H-2(W)1314
097 H-1(West)
097 H-2(E)122
097 H-2(W)1314
097 H-2(W)1314
097 H-2(W)2223
097 H-1



SWMC		Client: Bangladesh Water Development Board		MIKE 21
		Project: Meghna Estuary Study		
File:	Date: Mon Apr 27 1998	Drawing no. 4.48		
Scale:	Unit: p5011			

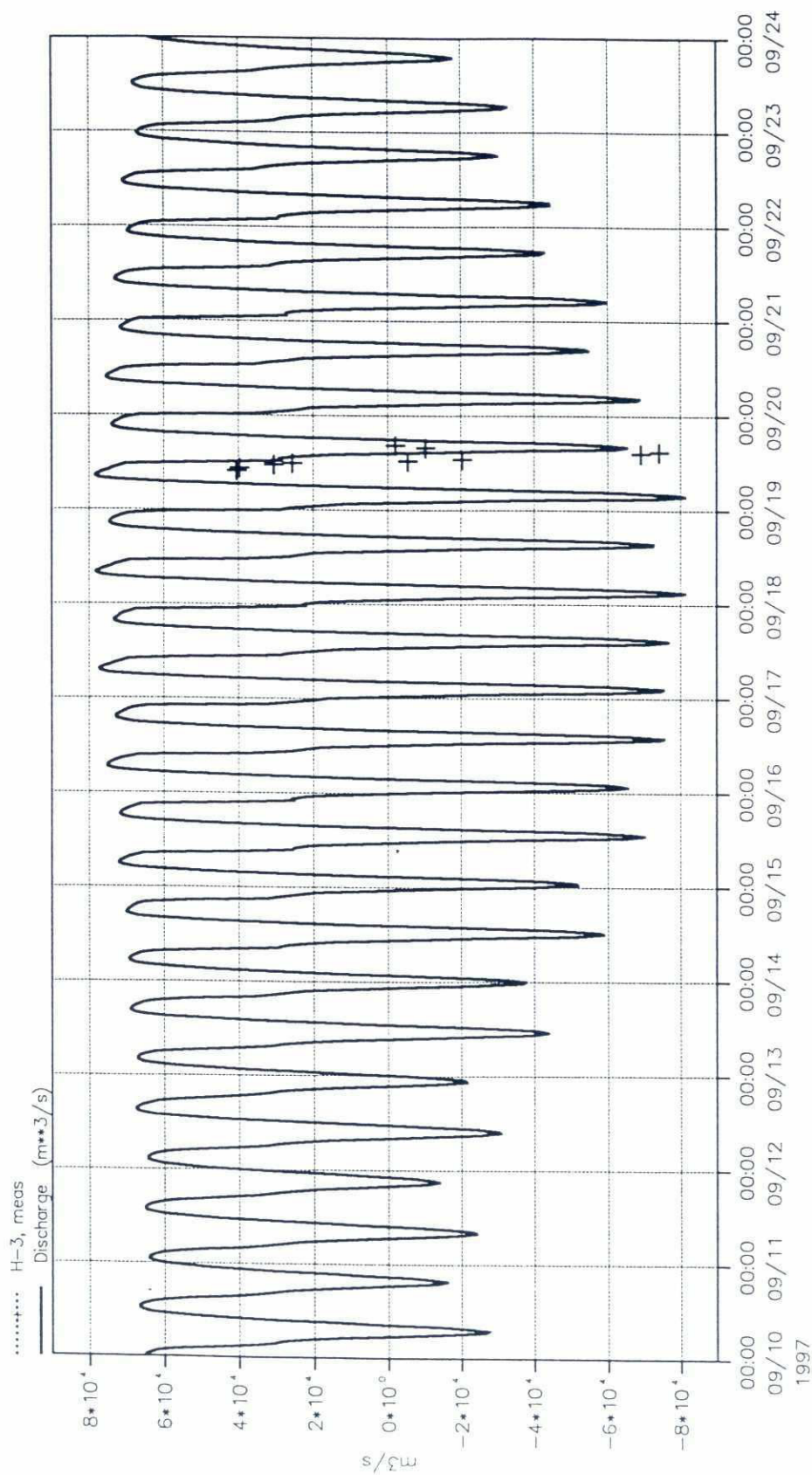
17 Smith-2KEN
 1097 H-2(W)1314
 1097 H-1(West)
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 1097 H-3

292

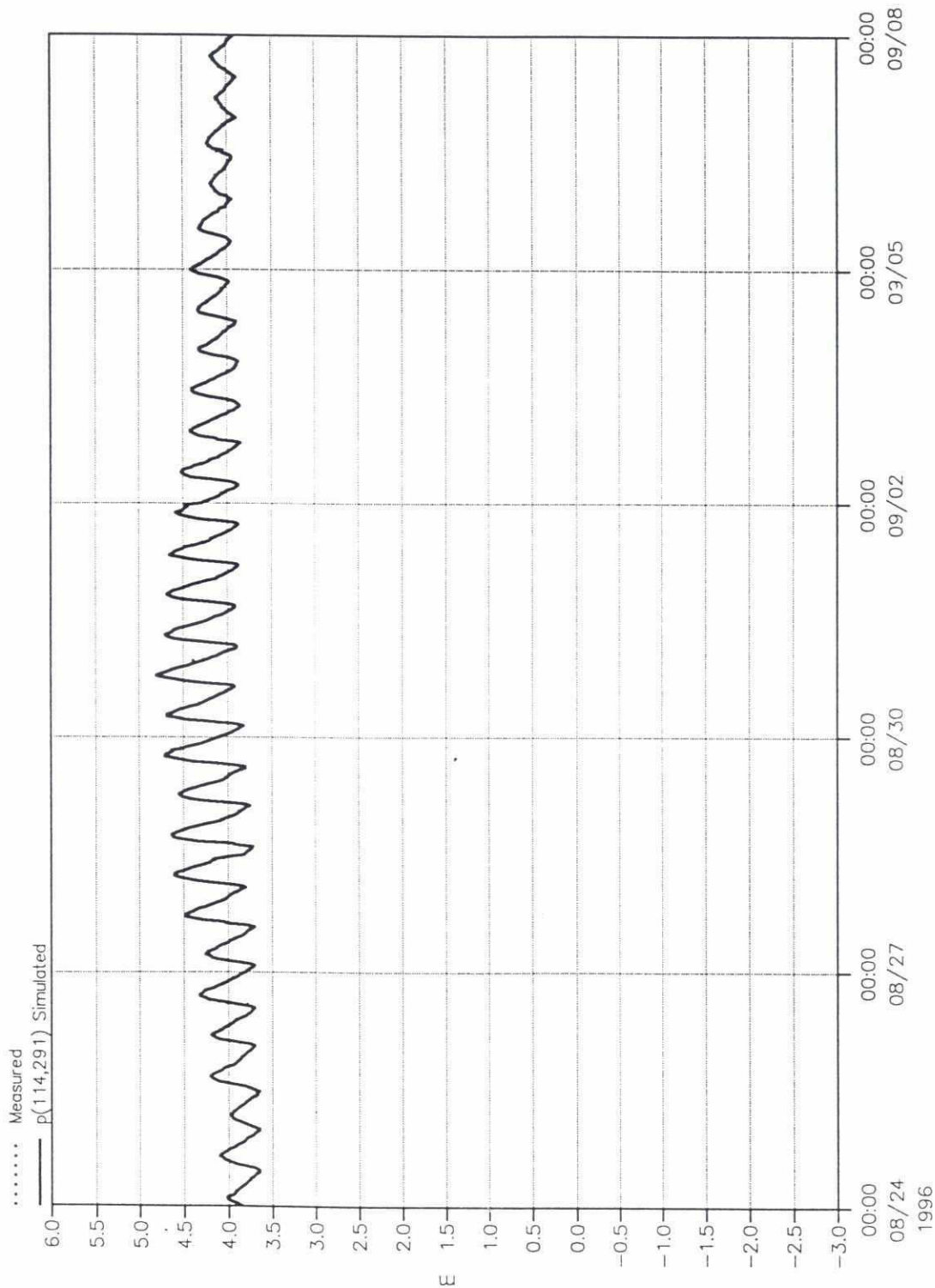


SWMC		Client: Bangladesh Water Development Board		MIKE 21
		Project: Meghna Estuary Study		
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Scale:	Init: p5011			
		H-2 (New East) Monpura to Jahajmara 20-21 September 1997		

✓

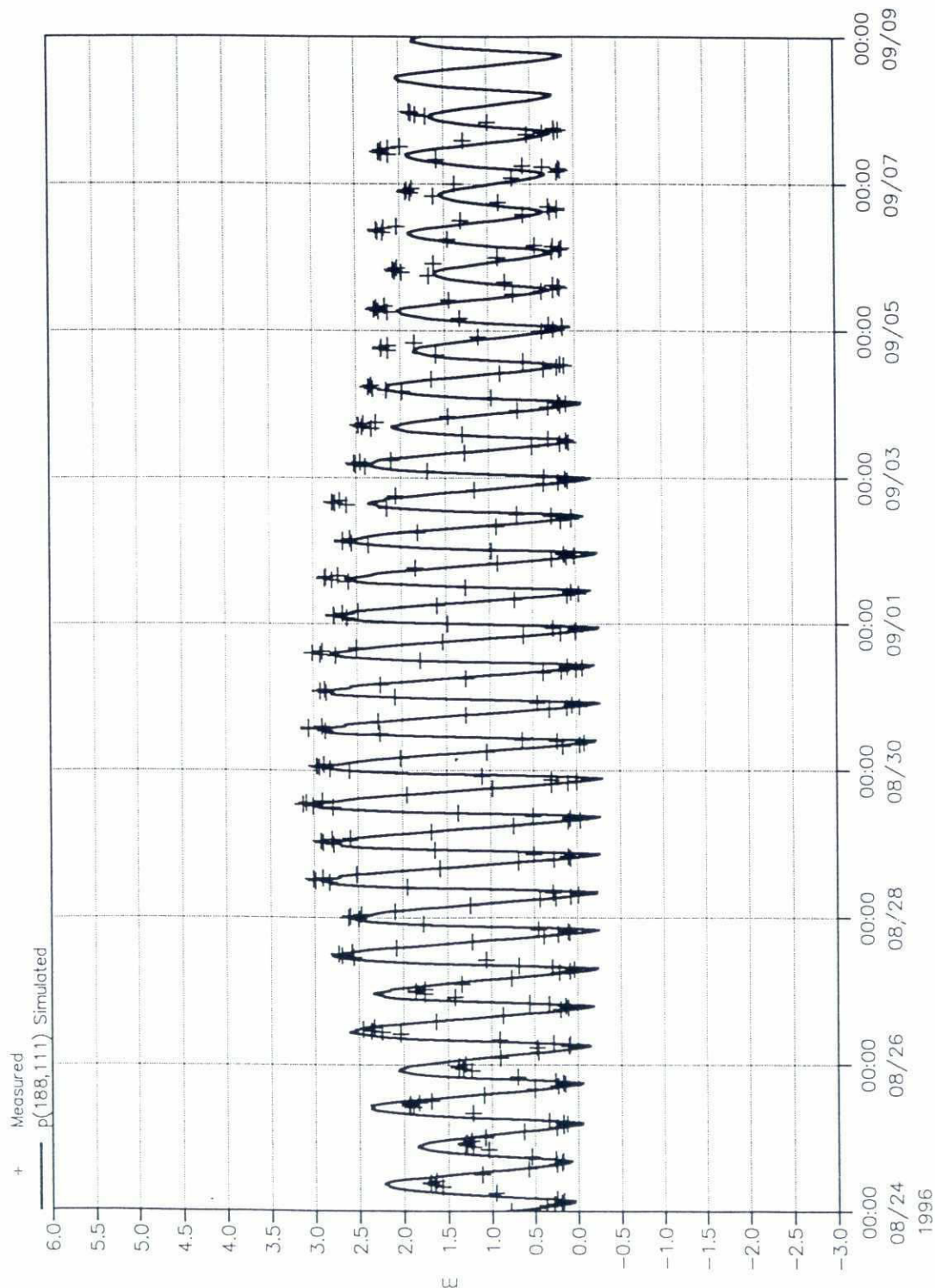


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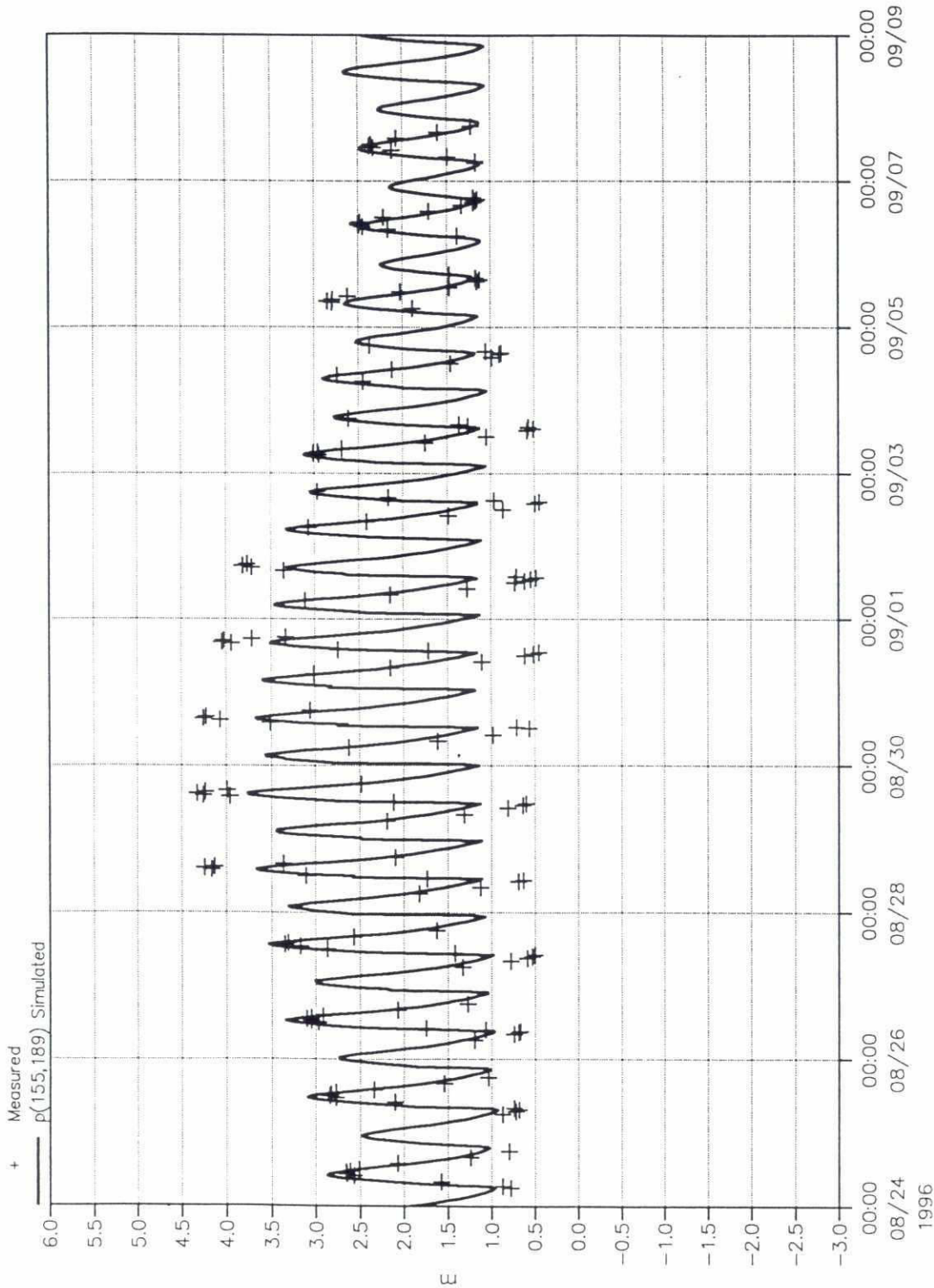


SWMC		Client: Bangladesh Water Development Board	MIKE 21
File:	Date: Sun May 31 1998	Project: Meghna Estuary Study	
Scale:	Init: p5011	Measured and simulated water level at Chandpur (PWD) Monsoon Season 1996	Drawing no. 4.51

298



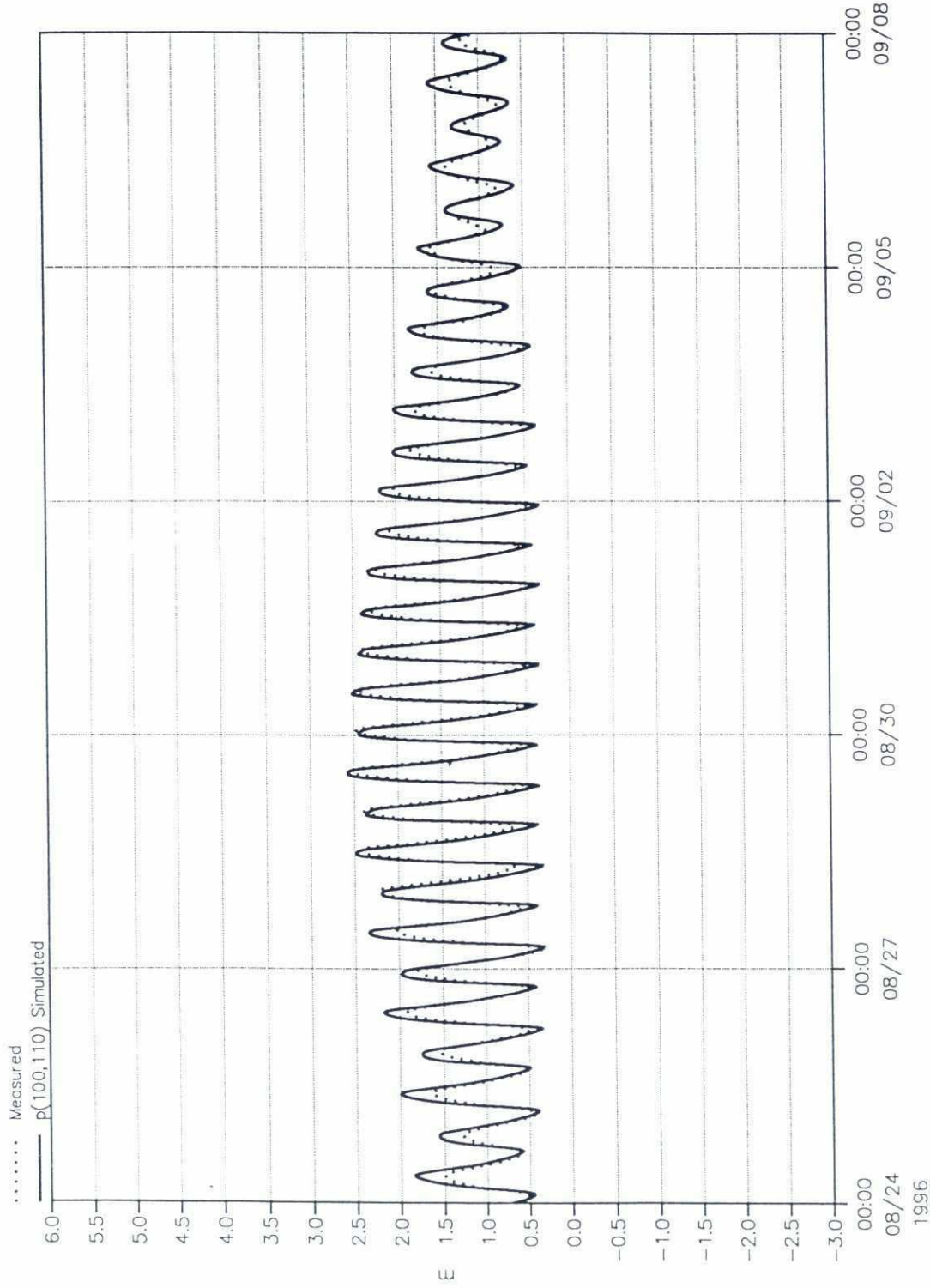
SWMC		Client: Bangladesh Water Development Board		MIKE 21
		Project: Meghna Estuary Study		
File:	Date: Sun May 31 1998	Measured and simulated water level at Char Chenga (PWD) Monsoon Season 1996		Drawing no. 4.52
Scale:	Init: p5011			



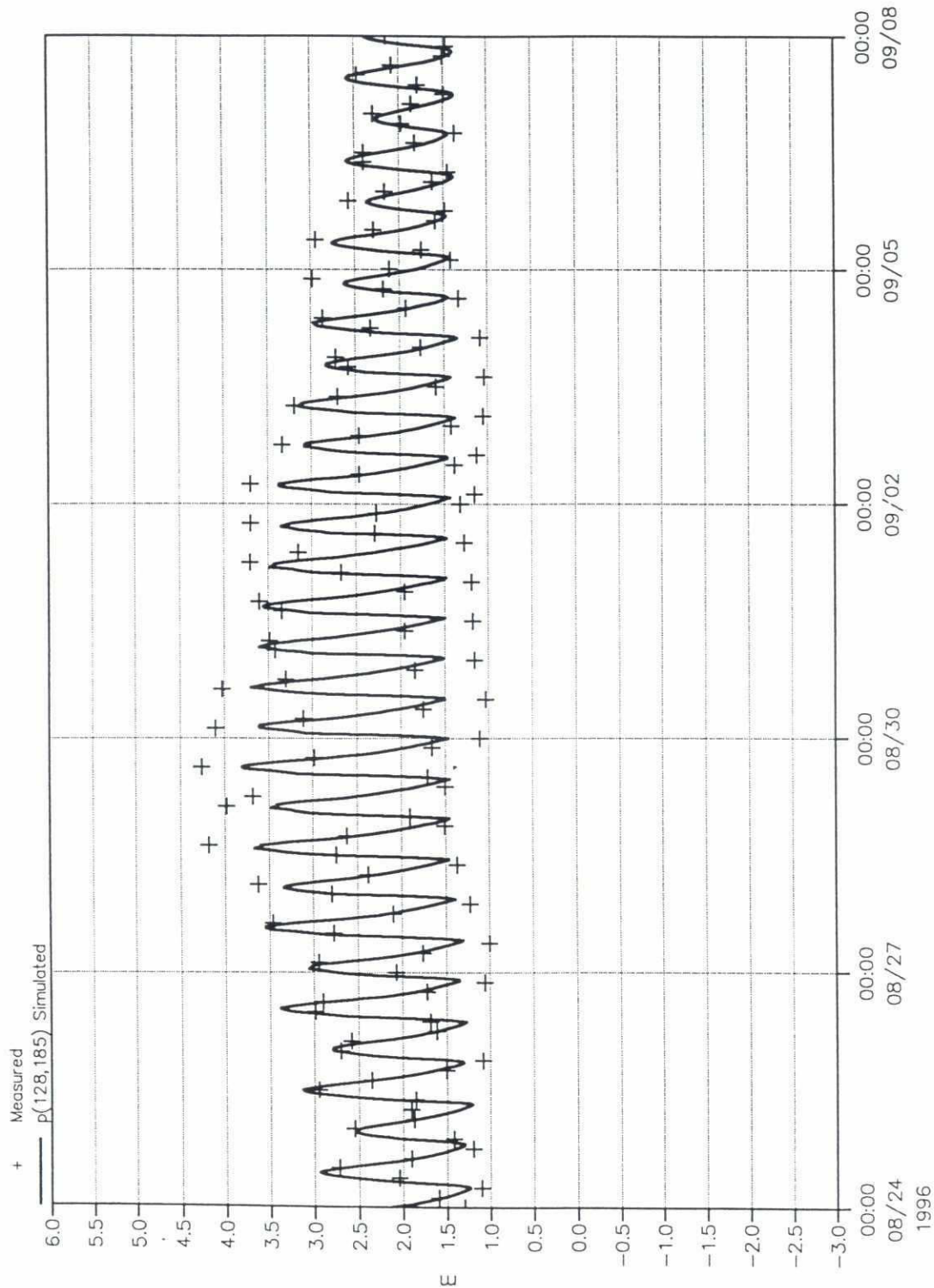
878

SWMC		Client: Bangladesh Water Development Board		MIKE 21
Project: Meghna Estuary Study		Drawing no.		4.53
File:	Date: Sun May 31 1998	Measured and simulated water level at		
Scale:	Init: p5011	Chitakhali (PWD)		
		Monsoon Season 1996		

293

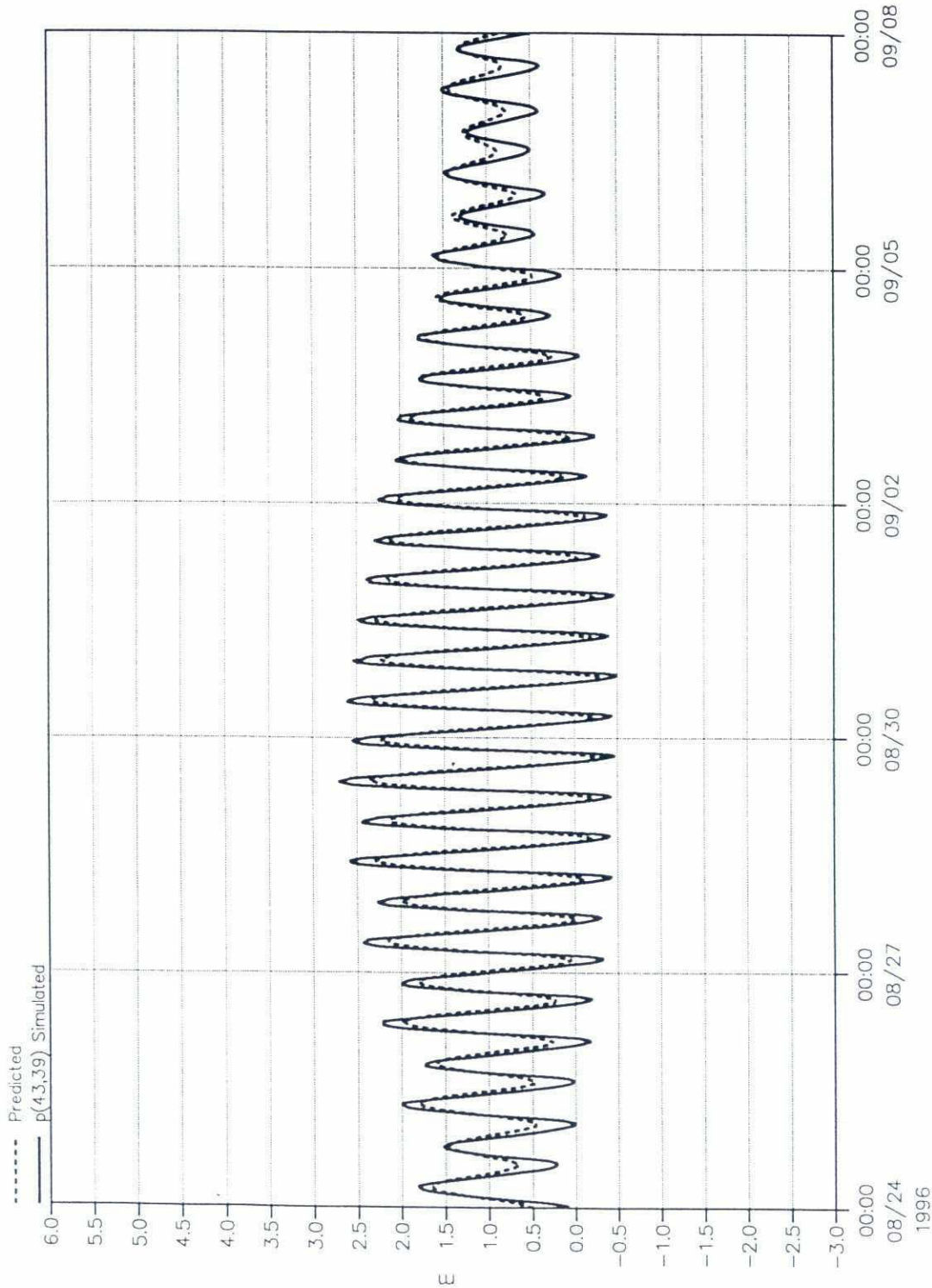


SWMC		Client: Bangladesh Water Development Board		MIKE 21
		Project: Meghna Estuary Study		
File:	Date: Sun May 31 1998	Measured and simulated water level at Dasmunia (PWD) Monsoon Season 1996	Drawing no.	4.54
Scale:	Init: p5011			

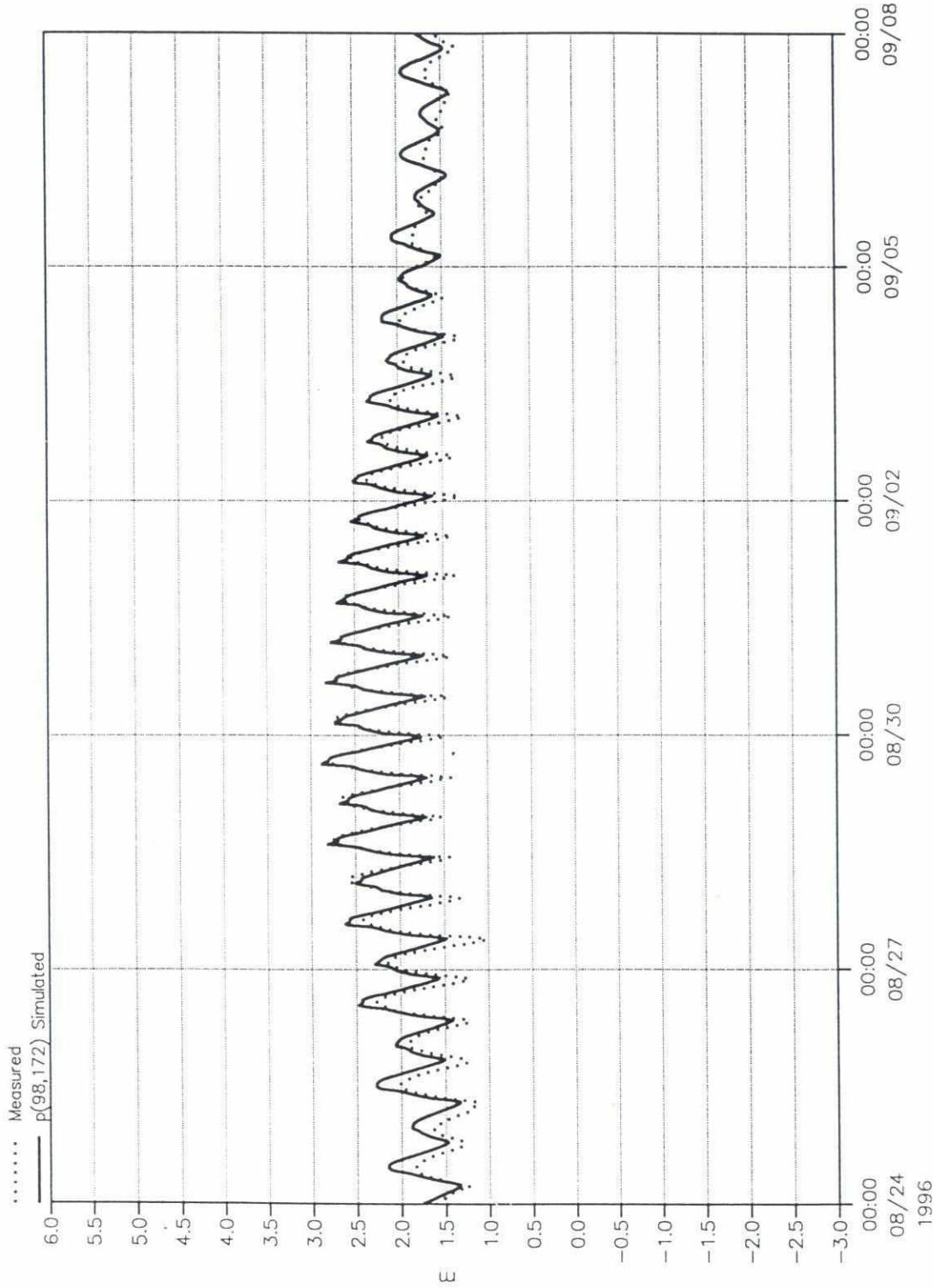


SWMC		Bangladesh Water Development Board		MIKE 21
Client:		Project:		
Date: Sun May 31 1998		Meghna Estuary Study		
File:		Measured and simulated water level at		Drawing no.
Scale:		Daulatkhan (PWD), BWDB		4.55
Init: p5011		Monsoon Season 1996		

298



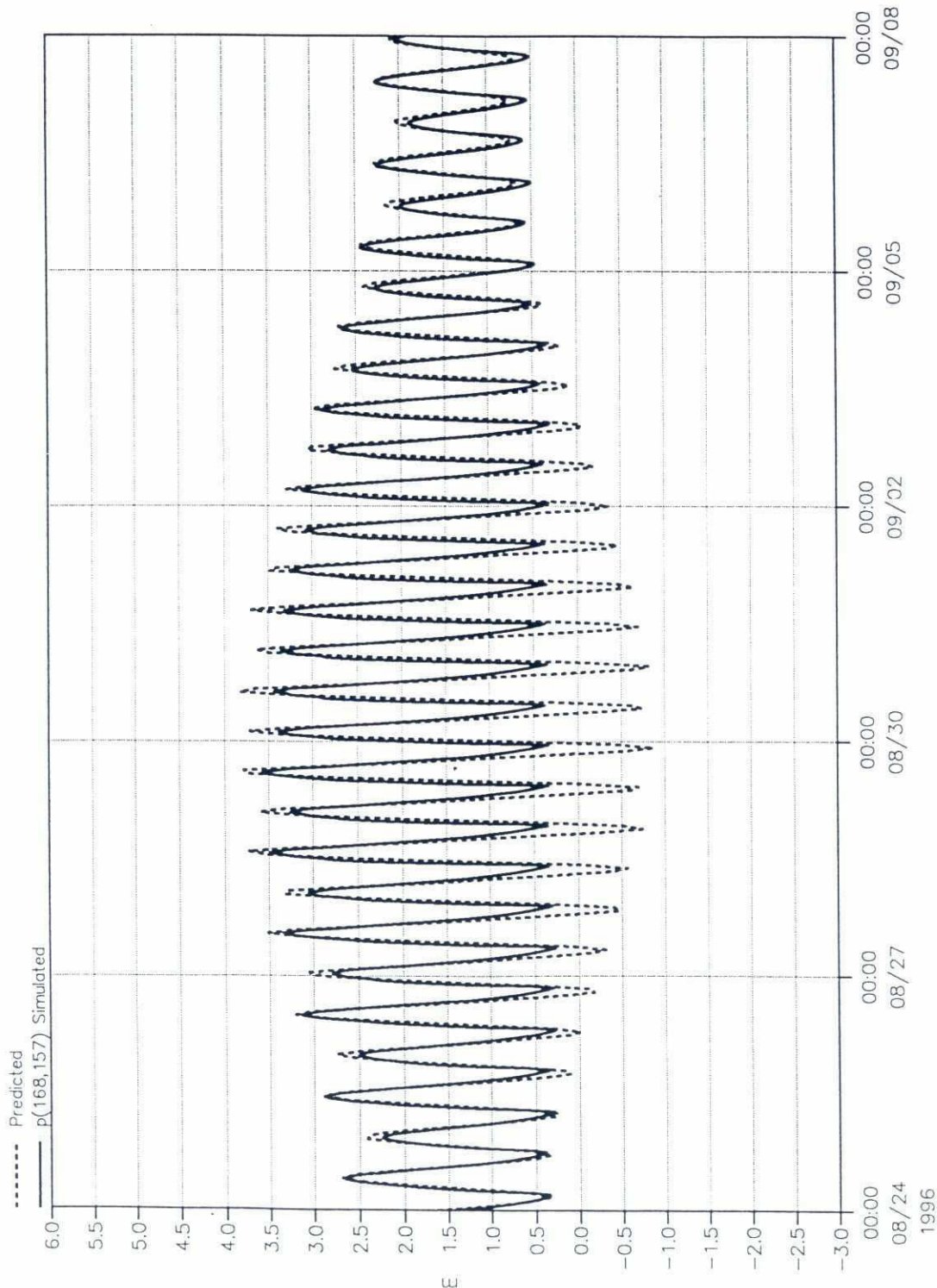
SWMC		Client: Bangladesh Water Development Board		MIKE 21
		Project: Meghna Estuary Study		
File:	Date: Sun May 31 1998	Measured and predicted water level at Dhulasar (PWD)		Drawing no. 4.56
Scale:	Init: p5011	Monsoon Season 1996		



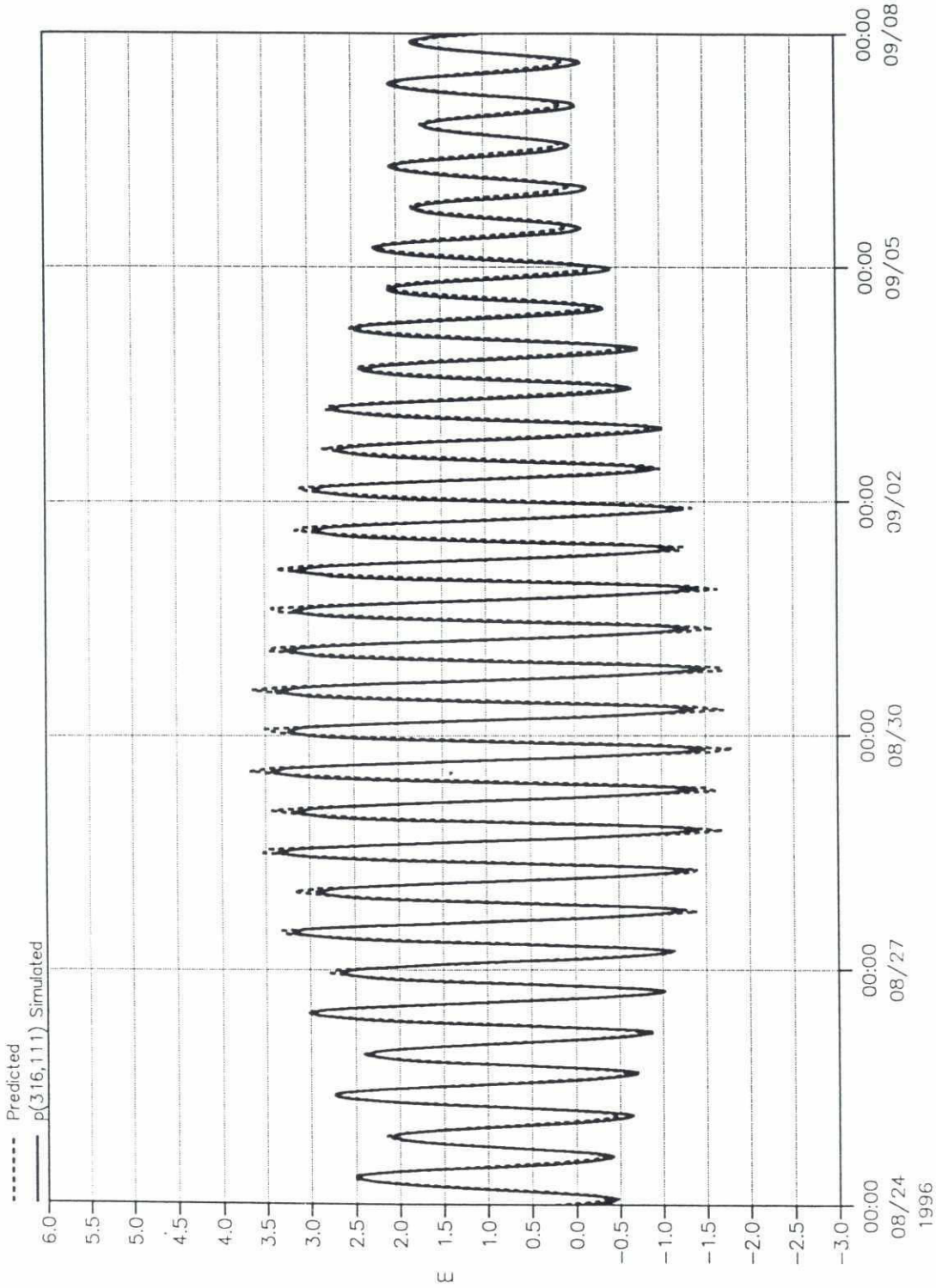
SWMC		Client: Bangladesh Water Development Board		MIKE 21
		Project: Meghna Estuary Study		
File:	Date: Sun May 31 1998	Measured and simulated water level at Dhulia (PWD)		Drawing no. 4.57
Scale:	Init: p5011	Monsoon Season 1996		

2066060996 Dhaka 996

200



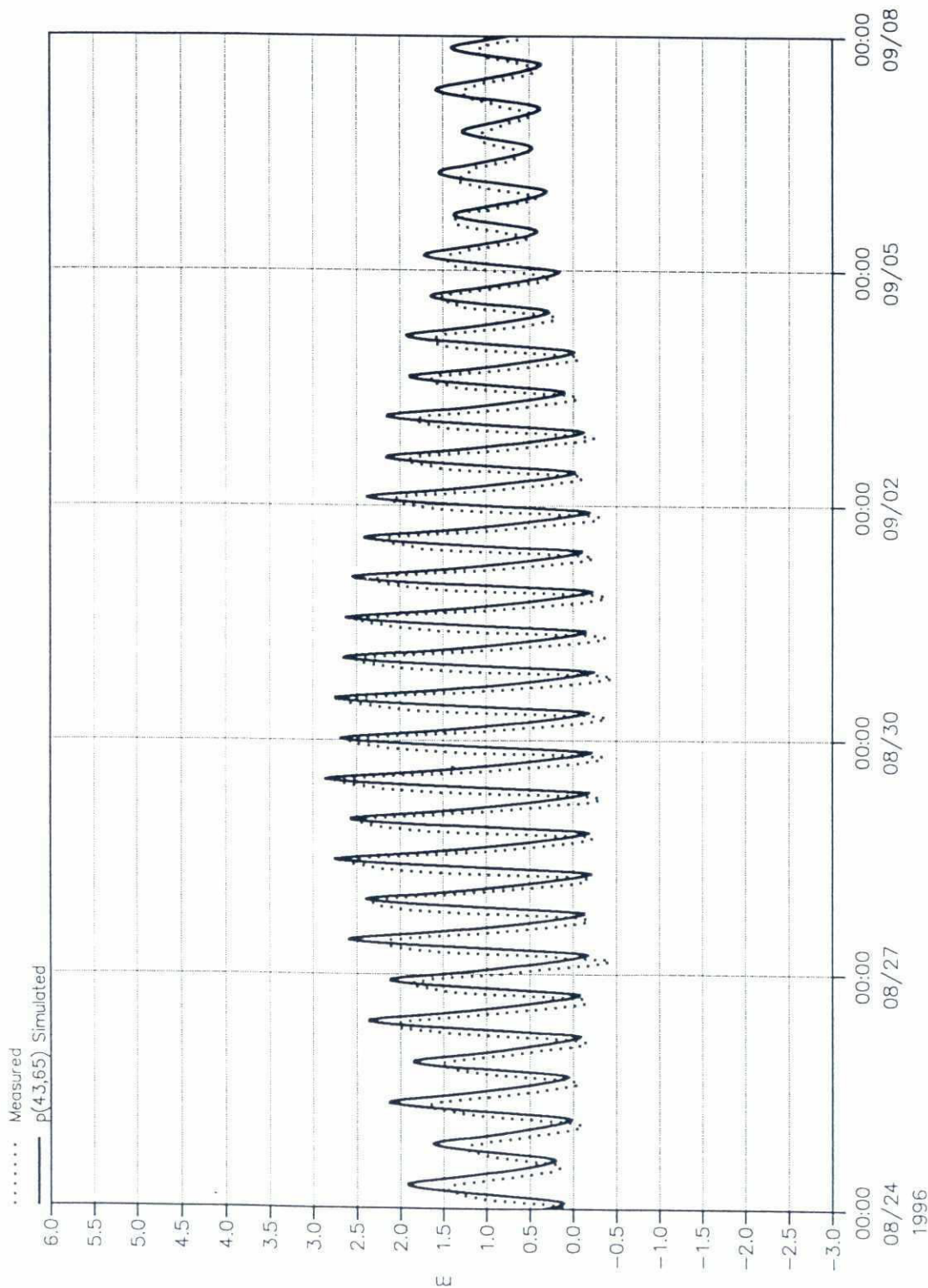
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Project: Meghna Estuary Study				
File:	Date: Sun May 31 1998	Measured and predicted water level at Hatia Bar (PWD) Monsoon Season 1996	Drawing no. 4.58	
Scale:	Init: p5011			



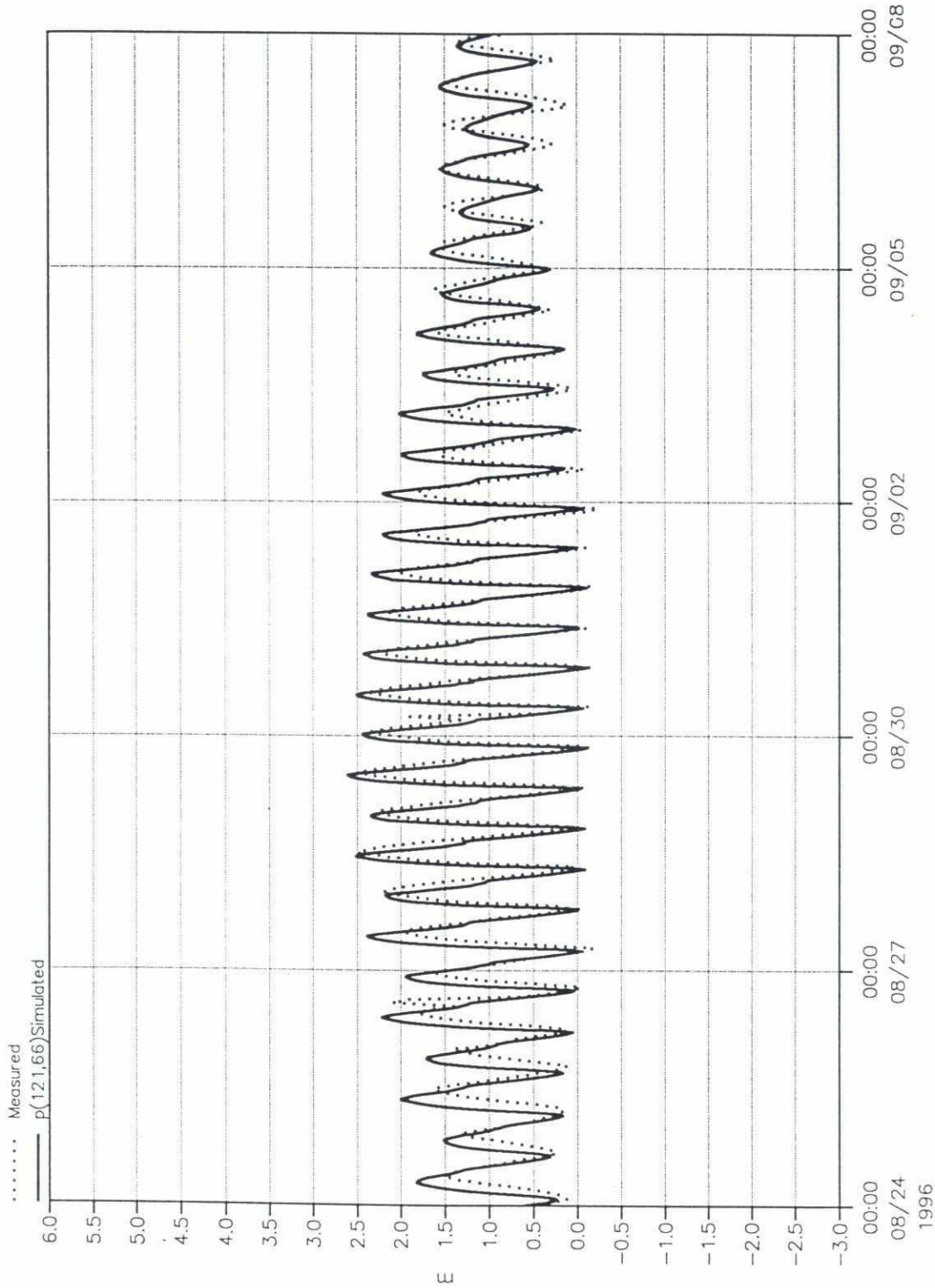
SVMC		Client: Bangladesh Water Development Board		MIKE 21
		Project: Meghna Estuary Study		
File:	Date: Sun May 31 1998	Measured and predicted water level at Khal No. 18 (PWD) Monsoon Season 1996		Drawing no. 4.59
Scale:	Init: p5011			

20

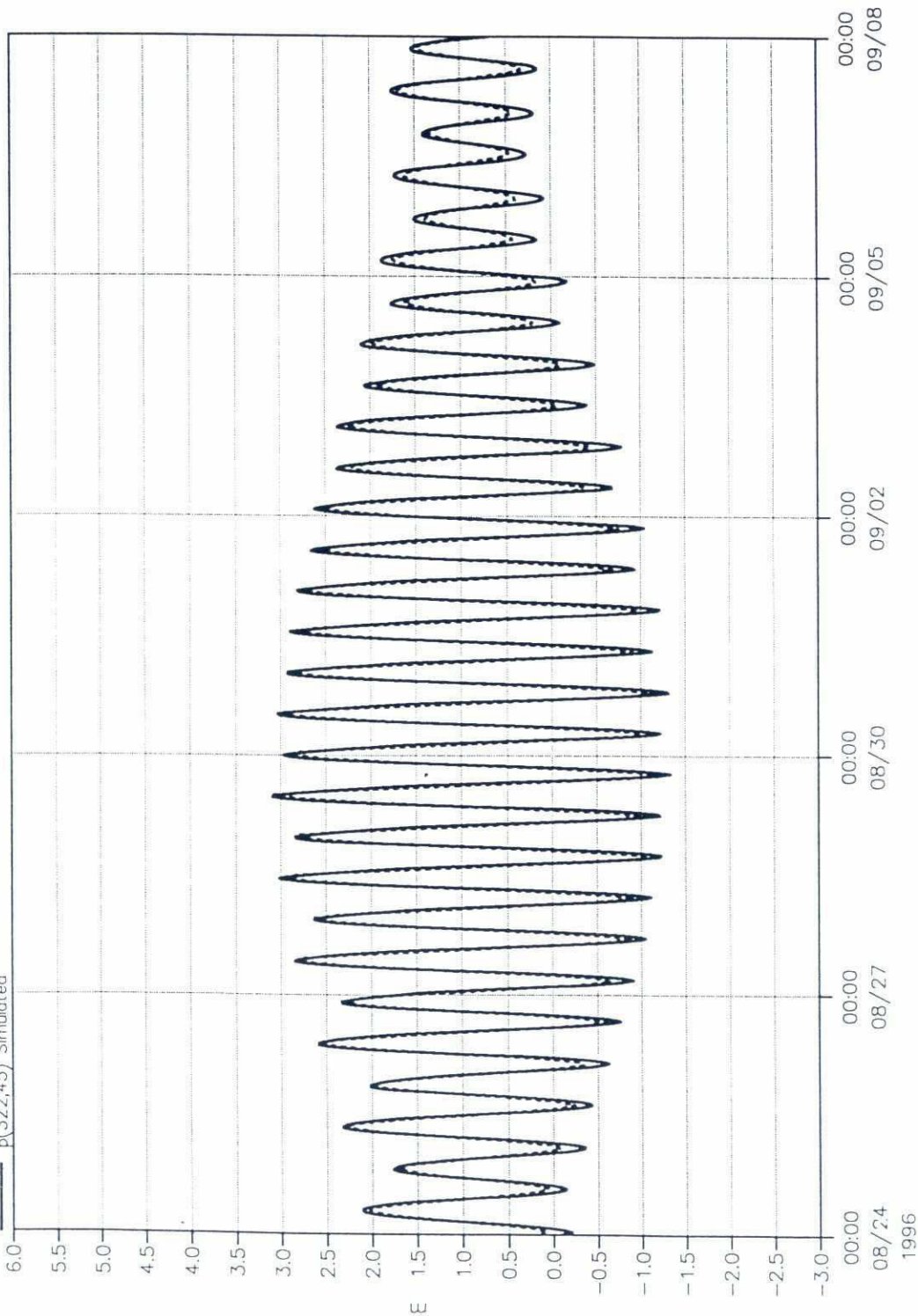
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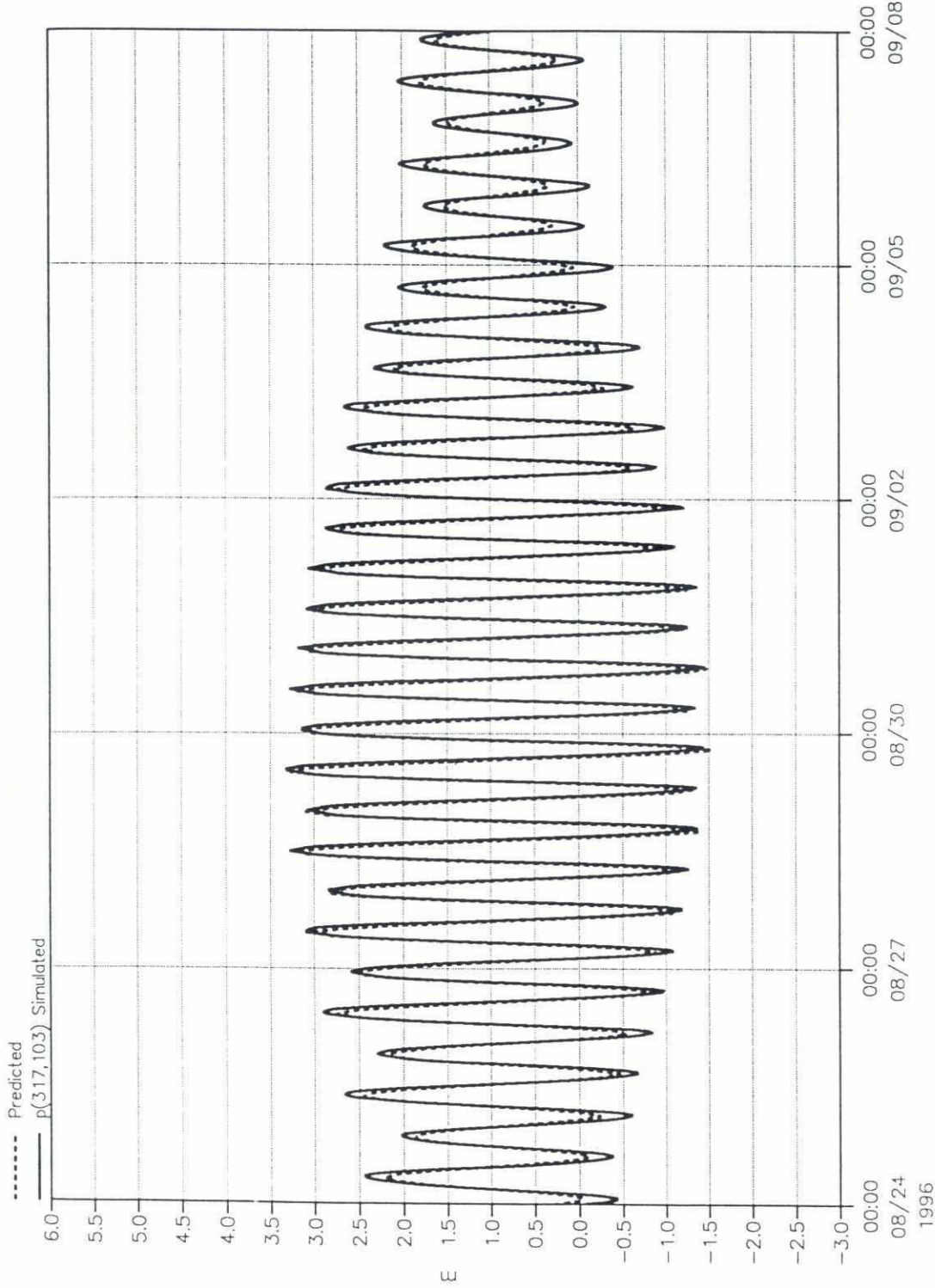
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		Project: Meghna Estuary Study			
File:	Date: Sun May 31 1998	Measured and simulated water level at Khepupara (PWD)		Drawing no. 4.60	
Scale:	Init: p5011	Monsoon Season 1996			



SVMC		Client: Bangladesh Water Development Board		MIKE 21
		Project: Meghna Estuary Study		
File:	Date: Sun May 31 1998	Measured and simulated water level at Kochopia (PWD)		Drawing no. 4.61
Scale:	Init: p5011	Monsoon Season 1996		



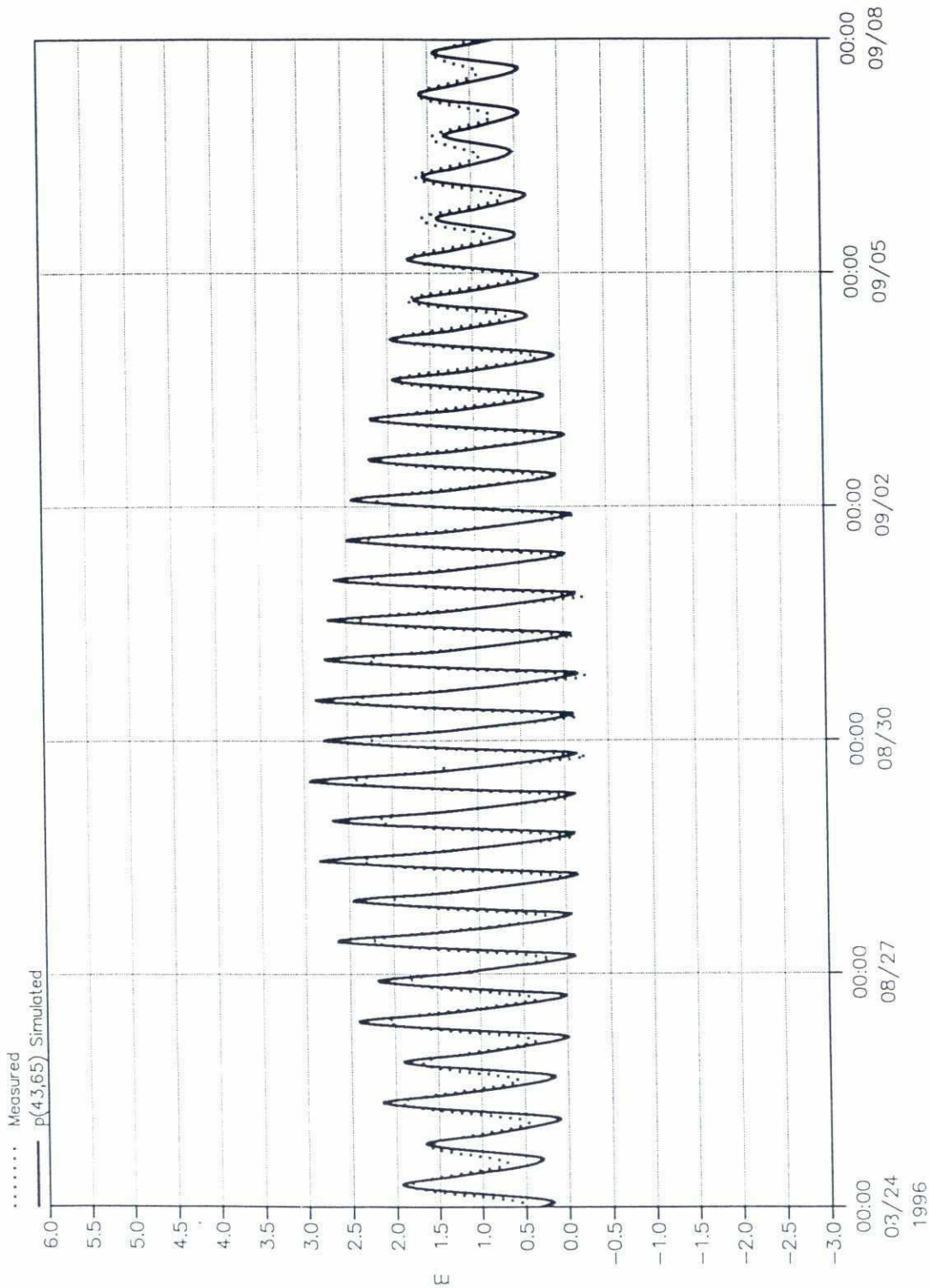
SWMC		Client: Bangladesh Water Development Board		MIKE 21	
		Project: Meghna Estuary Study			
File:	Date: Sun May 31 1998	Measured and predicted water level at Kutubdia Island (PWD)		Drawing no. 4.62	
Scale:	Init: p5011	Monsoon Season 1996			



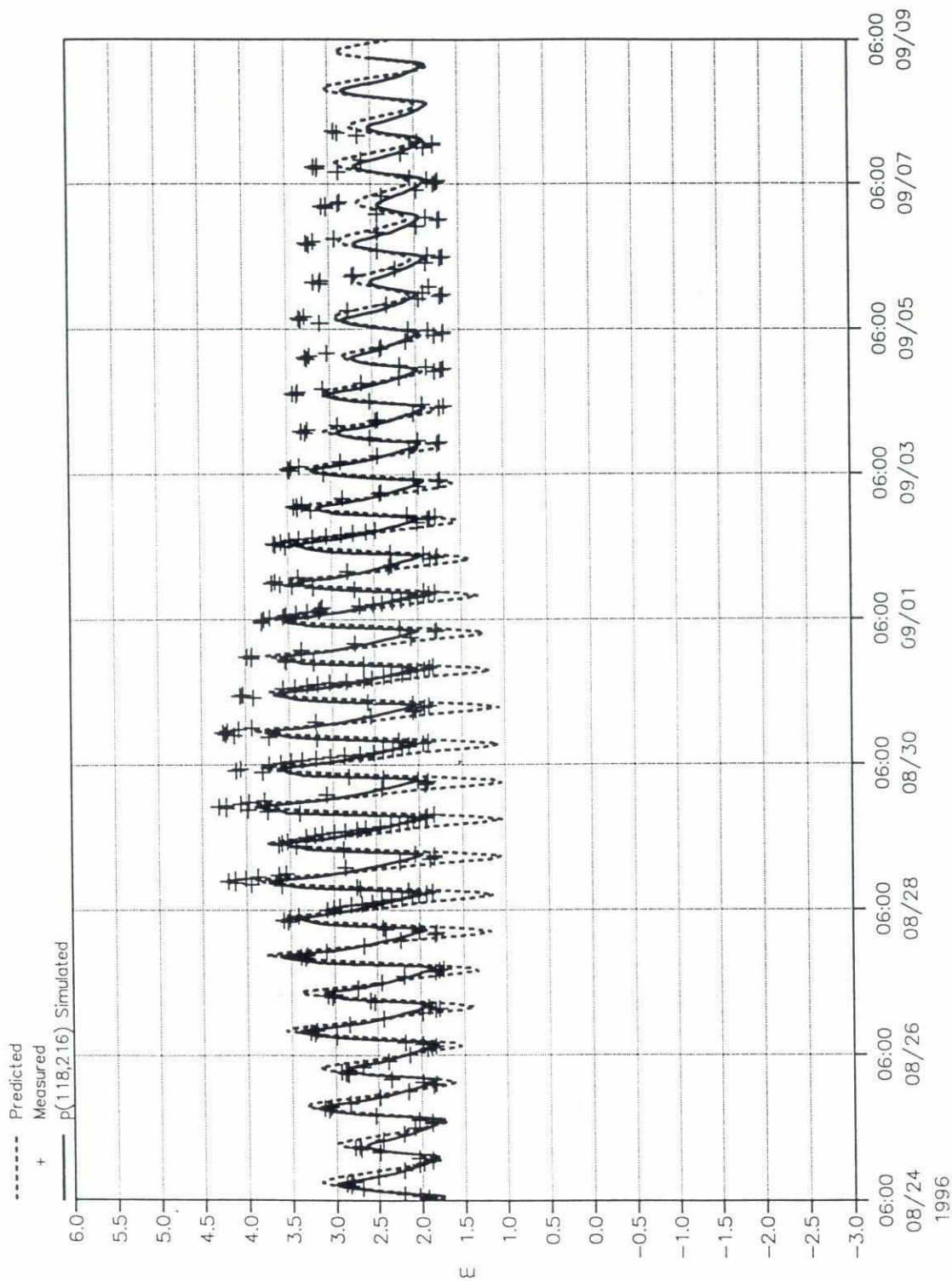
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Date: Sun May 31 1998		Project: Meghna Estuary Study		
File:		Measured and predicted water level at Normans Point (PWD)		Drawing no.
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208

203



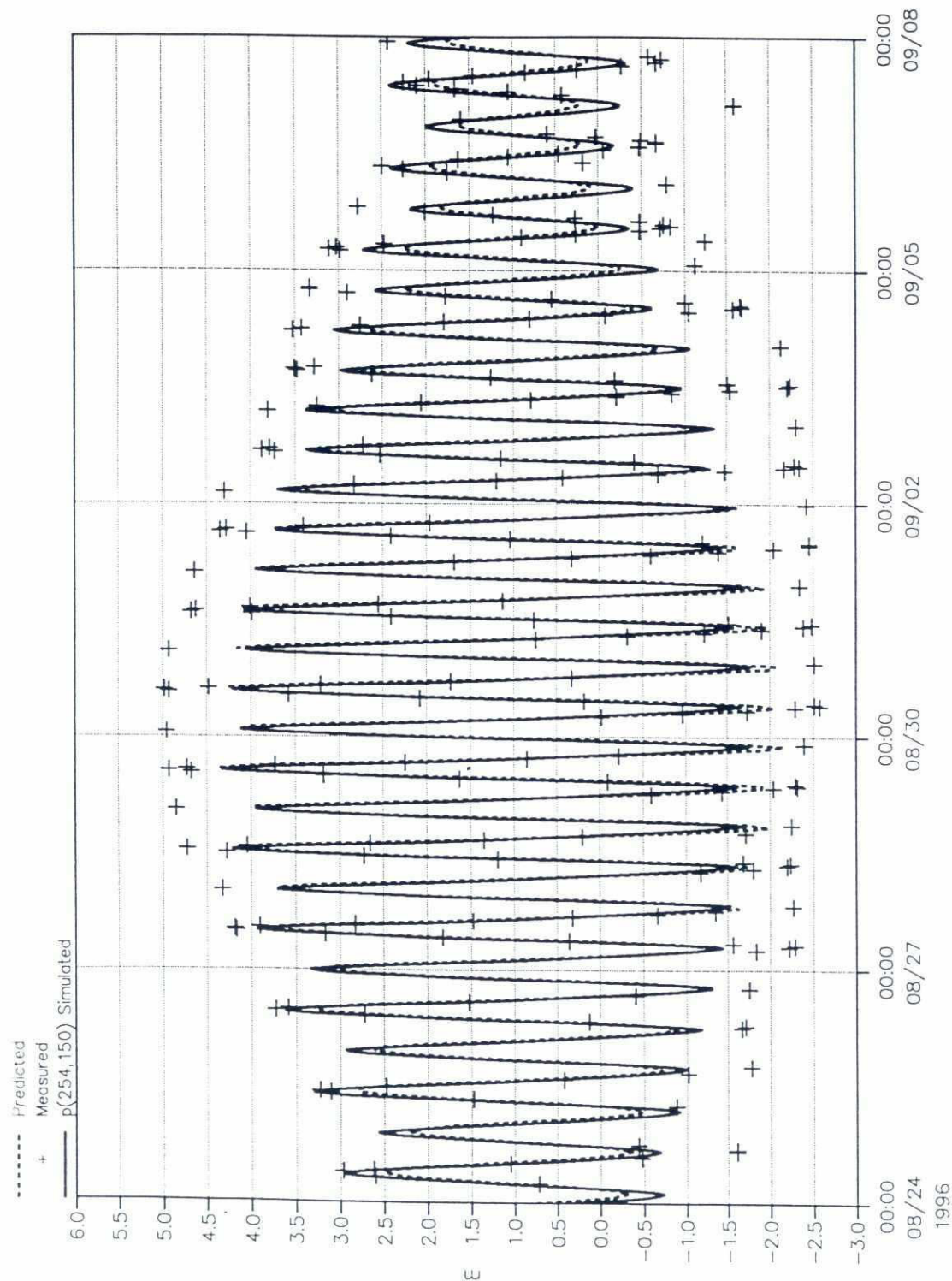
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		Project: Meghna Estuary Study		
File:	Date: Sun May 31 1998	Measured and simulated water level at Rabnabad Channel (PWD) Monsoon Season 1996		Drawing no. 4.64
Scale:	Init: p5011			



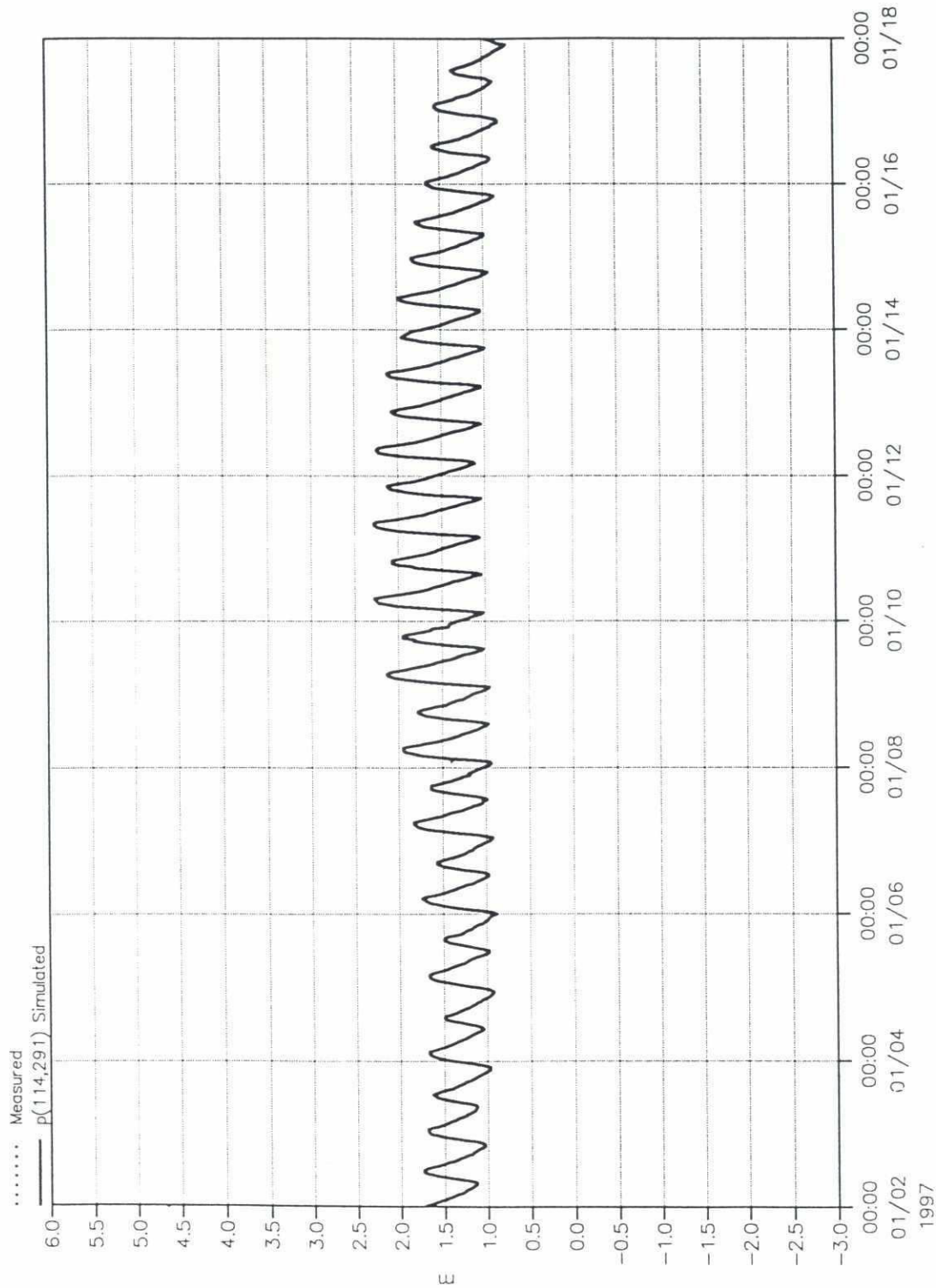
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File:	Date: Sun May 31 1998	Measured, simulated and predicted water level at Ramdaspur Monsoon Season 1996	
Scale:	Init: p5011		
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23

207

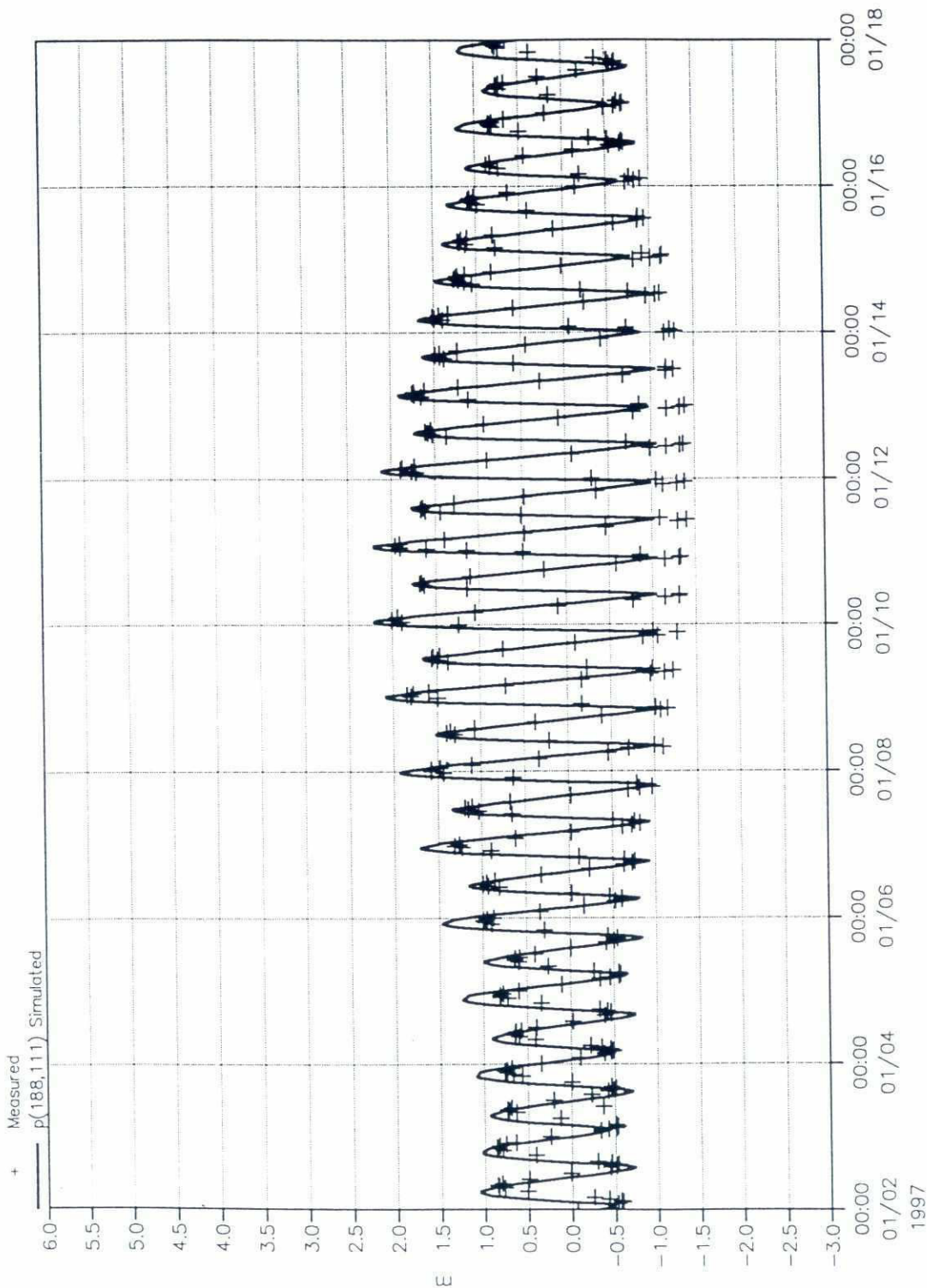


SWMC		Client: Bangladesh Water Development Board		MIKE 21	
		Project: Meghna Estuary Study			
File:	Date: Sun May 31 1998	Measured, simulated and predicted water level at Sandwip (PWD)		Drawing no. 4.66	
Scale:	Init: p5011	Monsoon Season 1996			

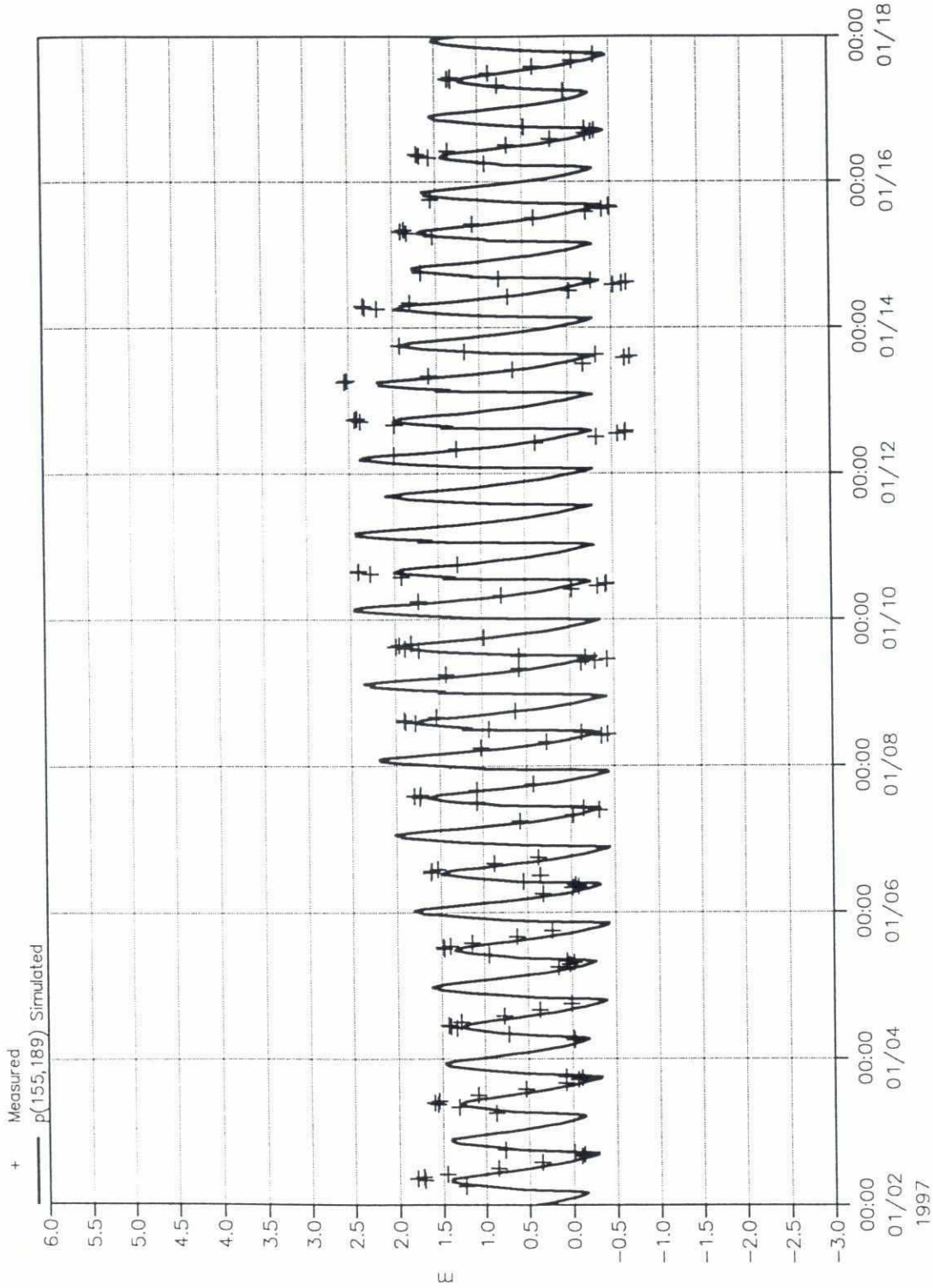


SWMC		Client: BANGLADESH WATER DEVELOPMENT BOARD		MIKE 21
		Project: MEGHNA ESTUARY STUDY		
File:	Date: Sun May 31 1998	Measured and simulated water level at Chandpur (PWD) Dry Season 1997		Drawing no. 4.67
Scale:	Init: p5011			

247



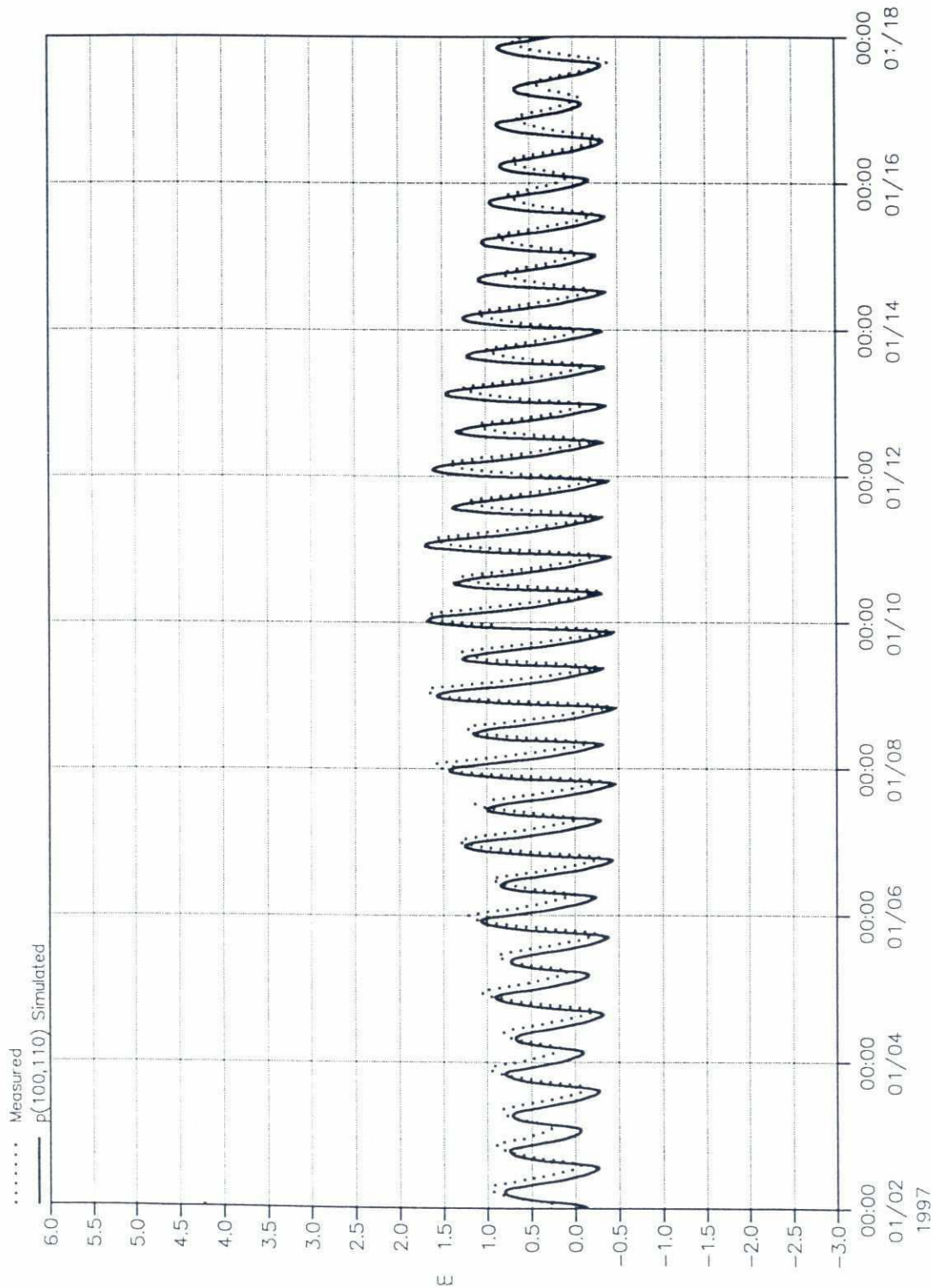
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		Project: MEGHNA ESTUARY STUDY		
File:	Date: Wed May 13 1998	Measured and simulated water level at Char Chenga (PWD) Dry period Validation, 1997		Drawing no. 4.68
Scale:	Unit: p5011			



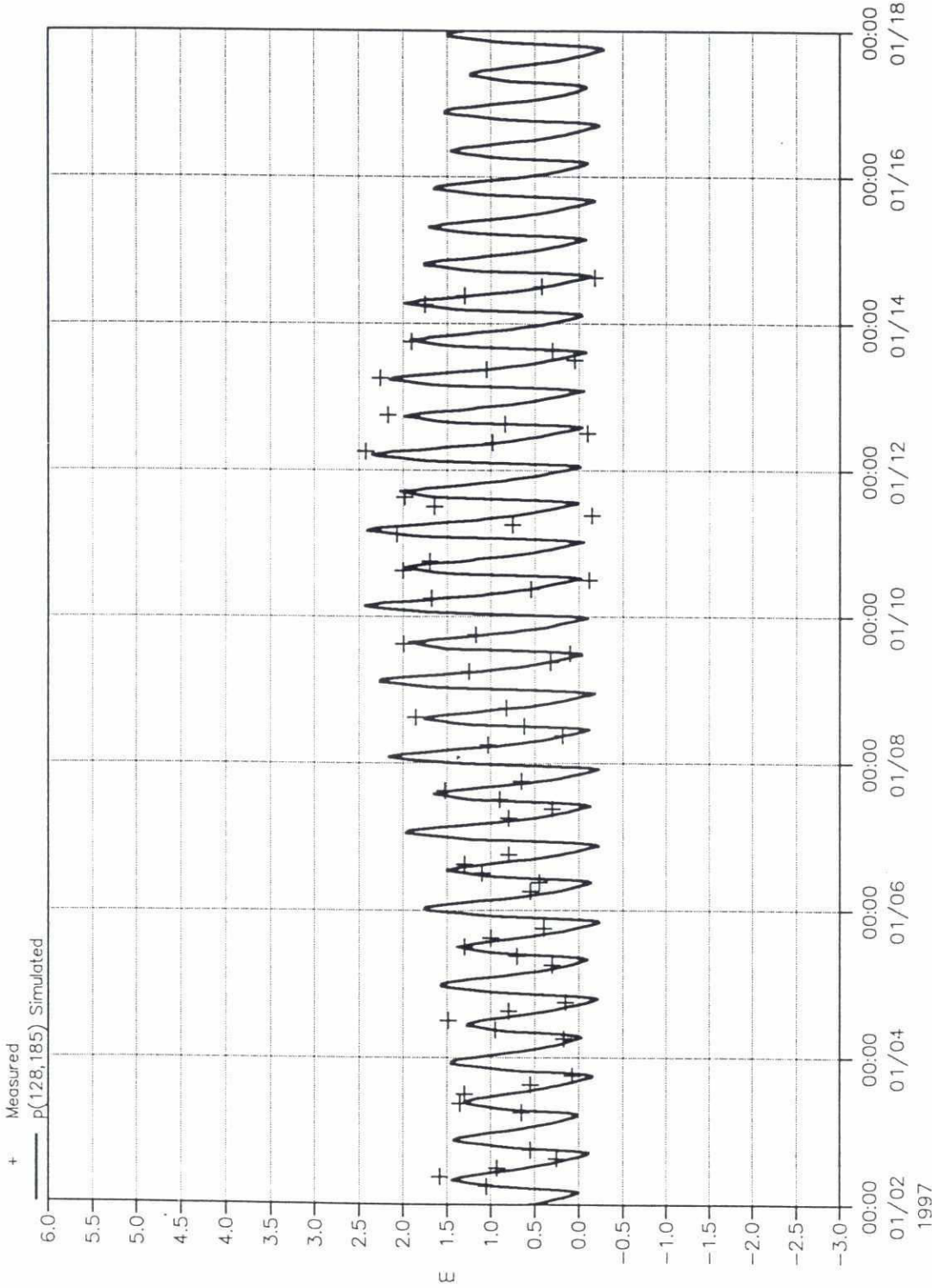
222

SWMC		Client:	BANGLADESH WATER DEVELOPMENT BOARD		MIKE 21
		Project:	MEGHNA ESTUARY STUDY		
File:	Date: Sun May 31 1998	Measured and simulated water level at Chitalkhali (PWD) Dry Season 1997		Drawing no. 4.69	
Scale:	Init: p5011				

222



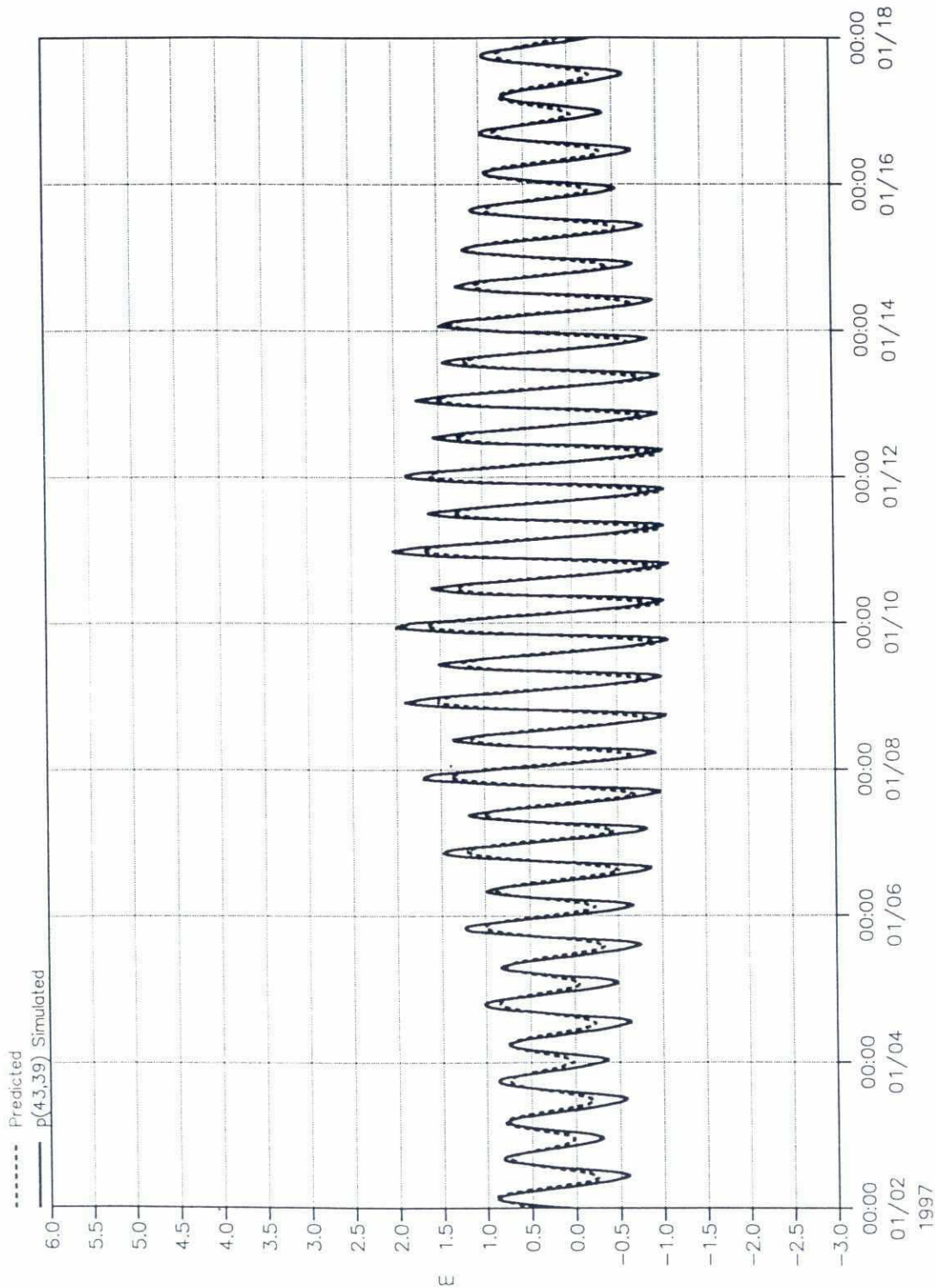
SWMC		Client:	BANGLADESH WATER DEVELOPMENT BOARD		MIKE 21
		Project:	MEGHNA ESTUARY STUDY		
File:	Date: Sun May 31 1998	Measured and simulated water level at Dasmunia (PWD) Dry Season 1997		Drawing no. 4.70	
Scale:	Init: p5011				



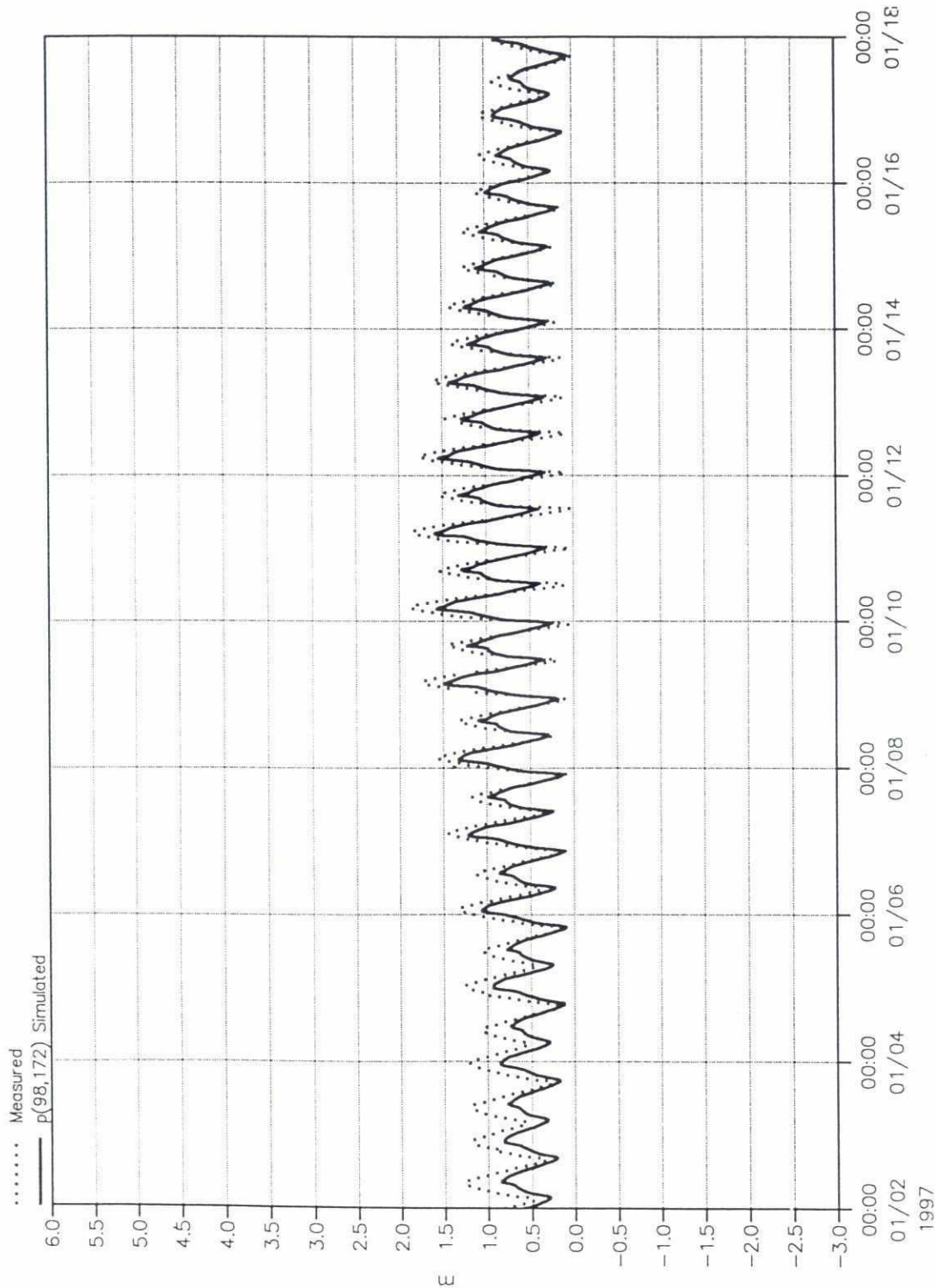
SWMC		Client: BANGLADESH WATER DEVELOPMENT BOARD		MIKE 21
		Project: MEGHNA ESTUARY STUDY		
File:	Date: Sun May 31 1998	Measured and simulated water level at Daulatkhan (PWD), BWDB Dry Season 1997		Drawing no. 4.71
Scale:	Init: p5011			

228

17 sm01974
297 4502H



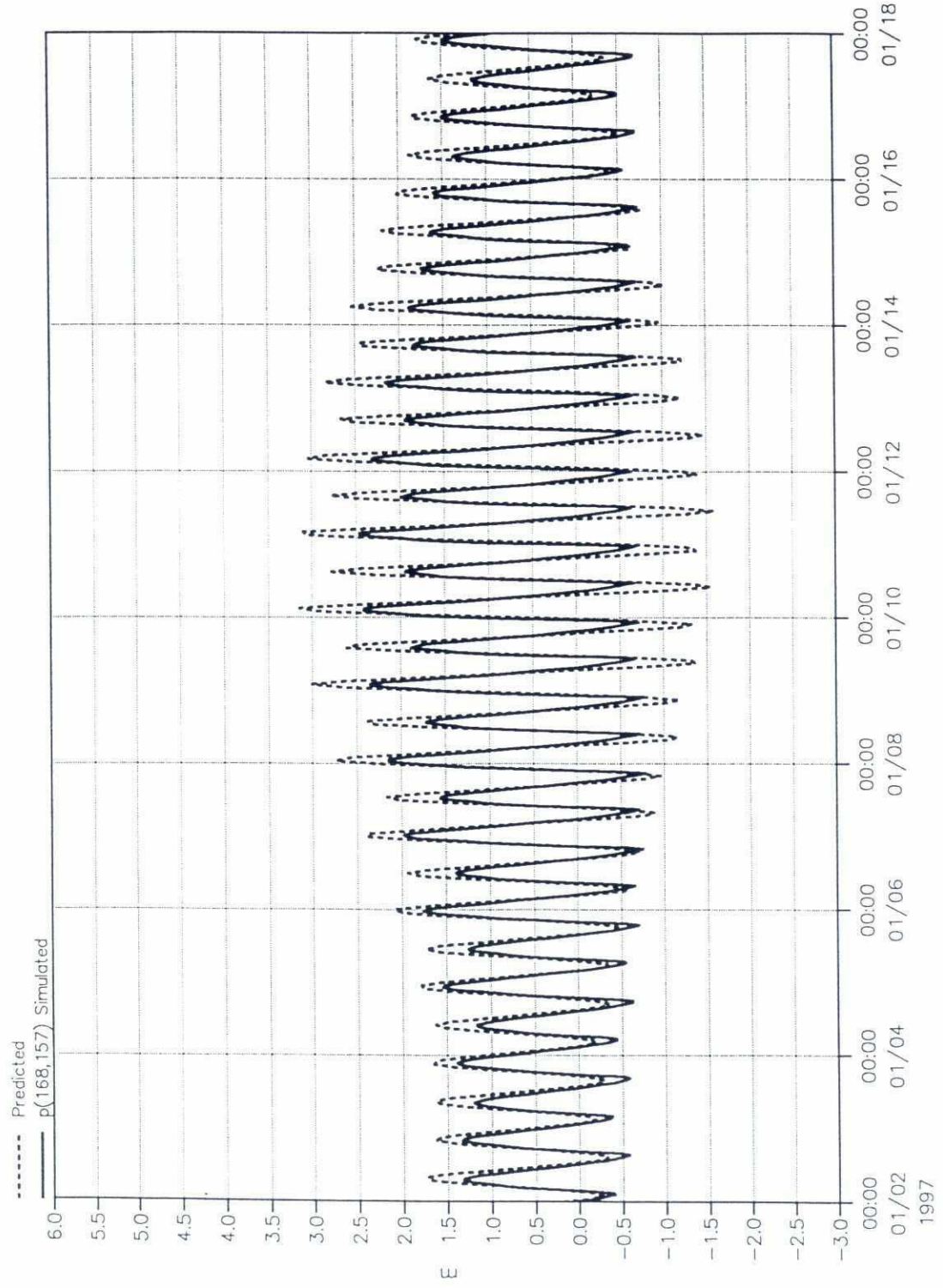
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		Project: MEGHNA ESTUARY STUDY	
File:	Date: Sun May 31 1998	Measured and predicted water level at Dhulasar (PWD) Dry Season 1997	
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		Drawing no.	4.72



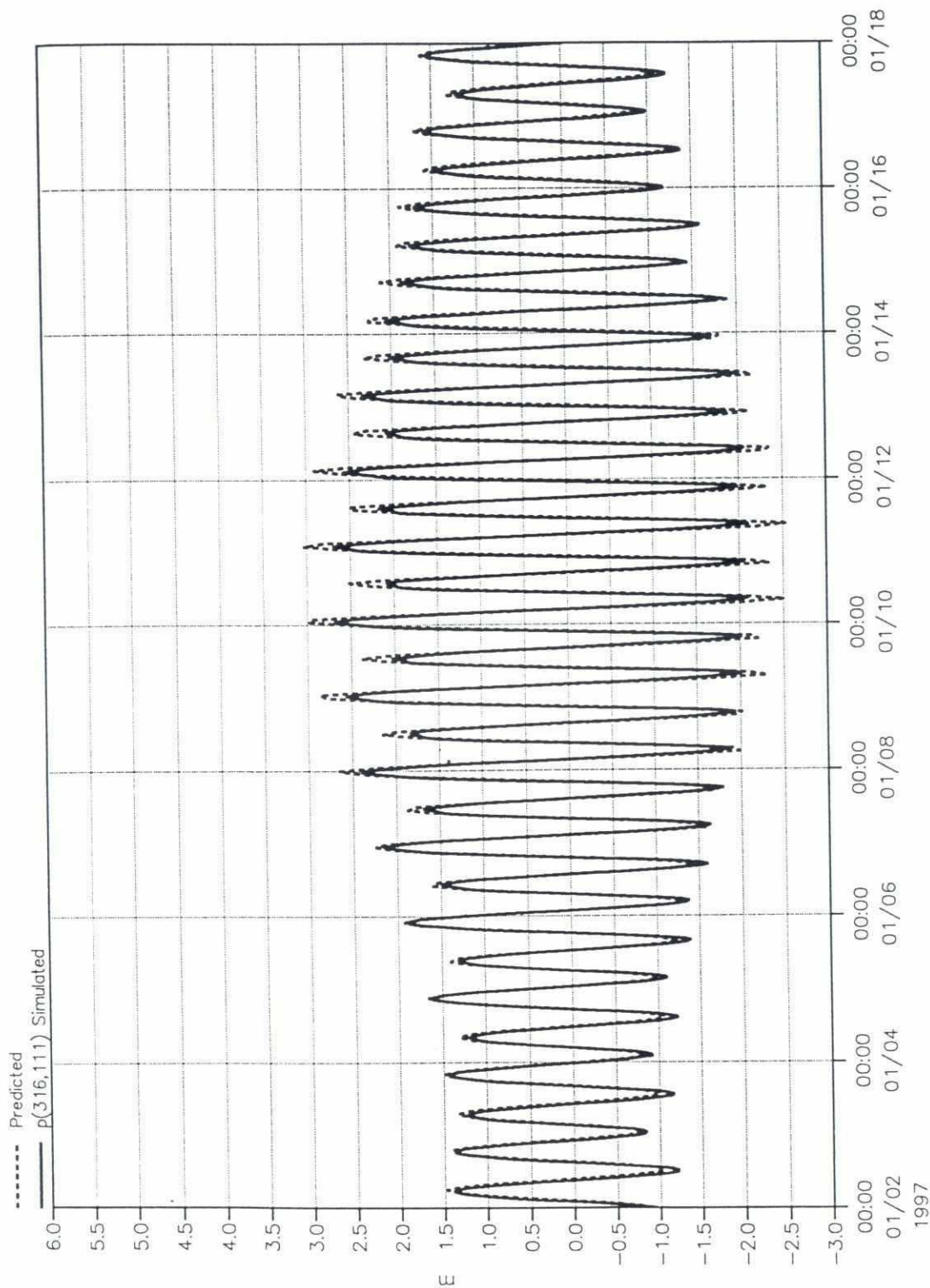
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		Project:	MEGHNA ESTUARY STUDY		
File:	Date: Sun May 31 1998	Measured and simulated water level at Dhulia (PWD) Dry Season 1997		Drawing no. 4.73	
Scale:	Unit: p5011				

197 4506N
0297 4506N

233



SWMC		Client: BANGLADESH WATER DEVELOPMENT BOARD		MIKE 21
		Project: MEGHNA ESTUARY STUDY		
File:	Date: Sun May 31 1998	Measured and predicted water level at Halia Bar (PWD) Dry Season 1997		
Scale:	Init: p5011			
		Drawing no. 4.74		



SWMC		Client: BANGLADESH WATER DEVELOPMENT BOARD		MIKE 21
		Project: MEGHNA ESTUARY STUDY		
File:	Date: Sun May 31 1998	Measured and predicted water level at Khal No. 18 (PWD) Dry Season 1997		Drawing no. 4.75
Scale:	Init: p5011			

SWMC

Client:

BANGLADESH WATER DEVELOPMENT BOARD

Project:

MEGHNA ESTUARY STUDY

File:

Date: Sun May 31 1998

Measured and predicted water level at
Khal No. 18 (PWD)
Dry Season 1997

Scale:

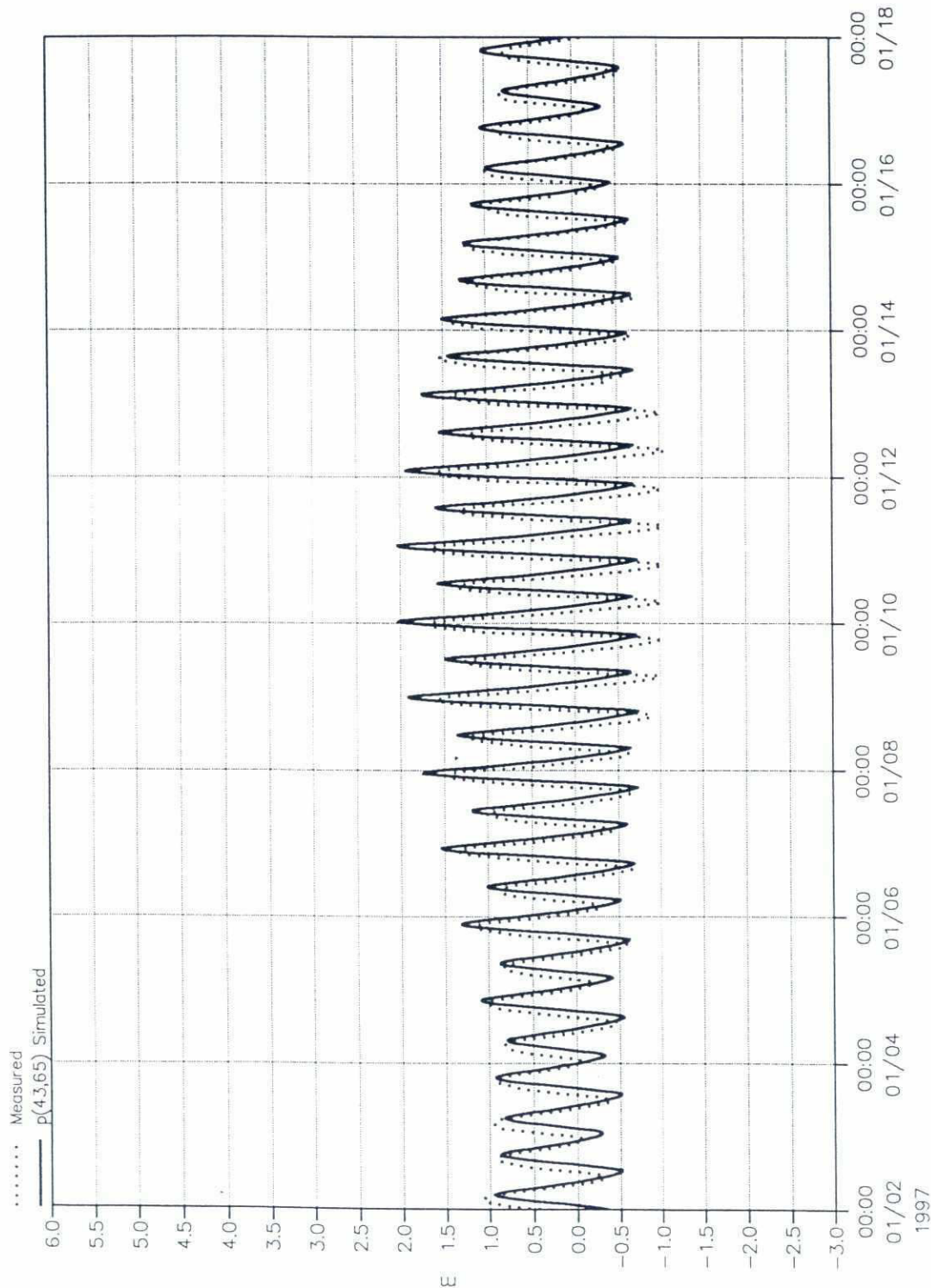
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Drawing no.

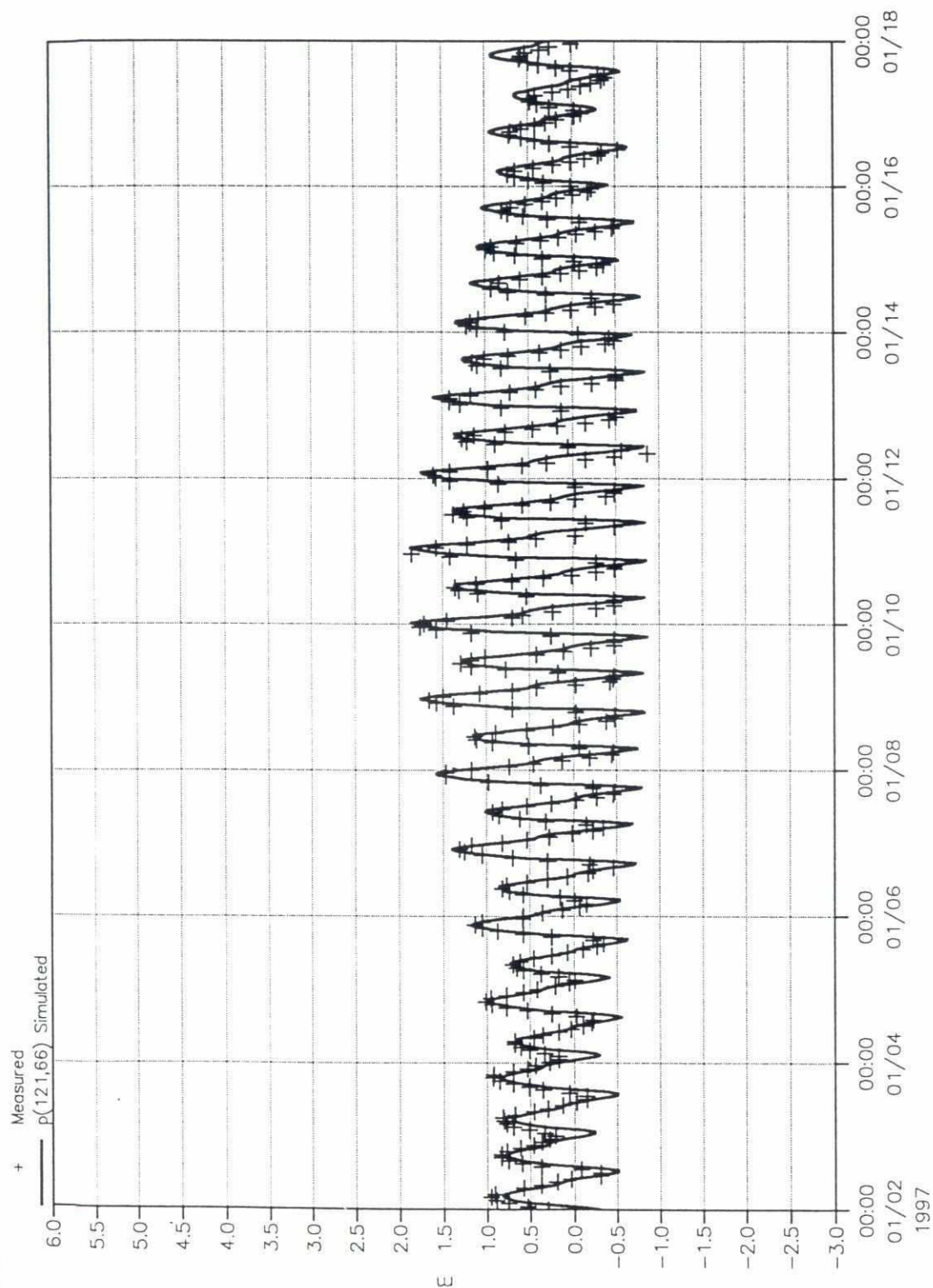
4.75

209

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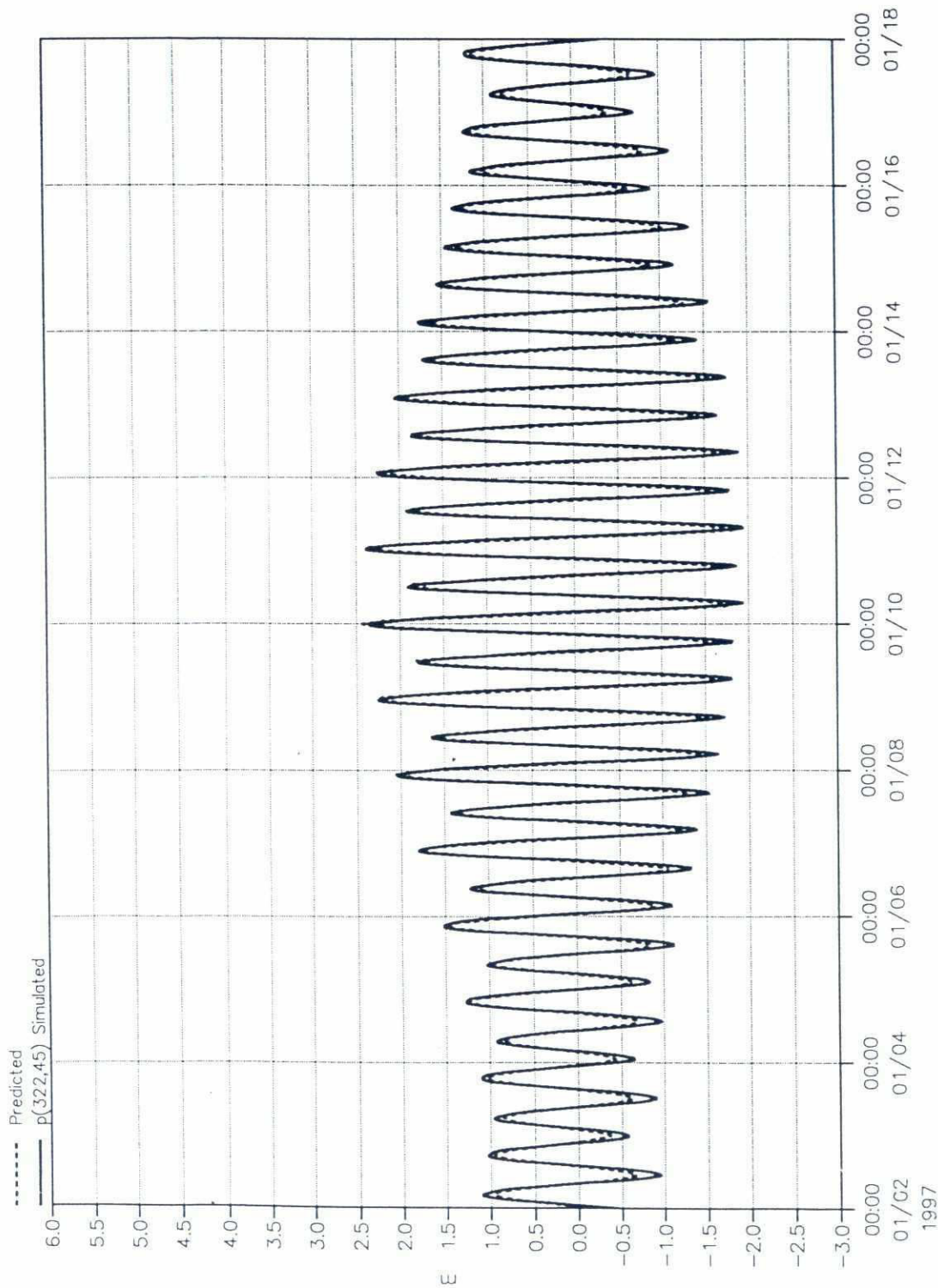


SWMC		Client:	BANGLADESH WATER DEVELOPMENT BOARD		MIKE 21
		Project:	MEGHNA ESTUARY STUDY		
File:	Date: Sun May 31 1998	Measured and simulated water level at Khepupara (PWD)		Drawing no.	4.76
Scale:	Init: p5011	Dry Season 1997			

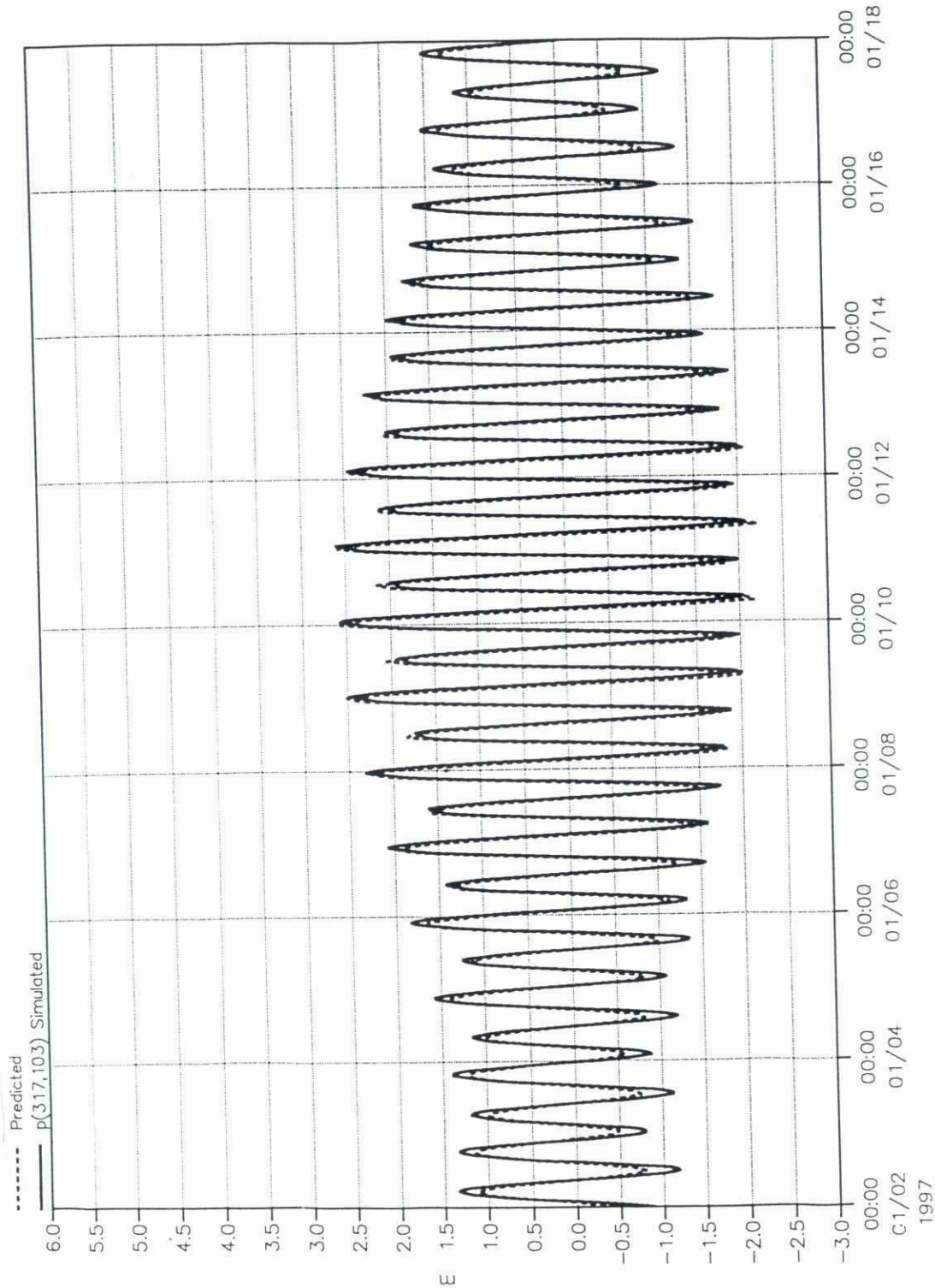


SWMC	File:	Date: Sun May 31 1998	Client: BANGLADESH WATER DEVELOPMENT BOARD Project: MEGHNA ESTUARY STUDY	Drawing no. 4.77
	Scale:	Init: p5011		

200

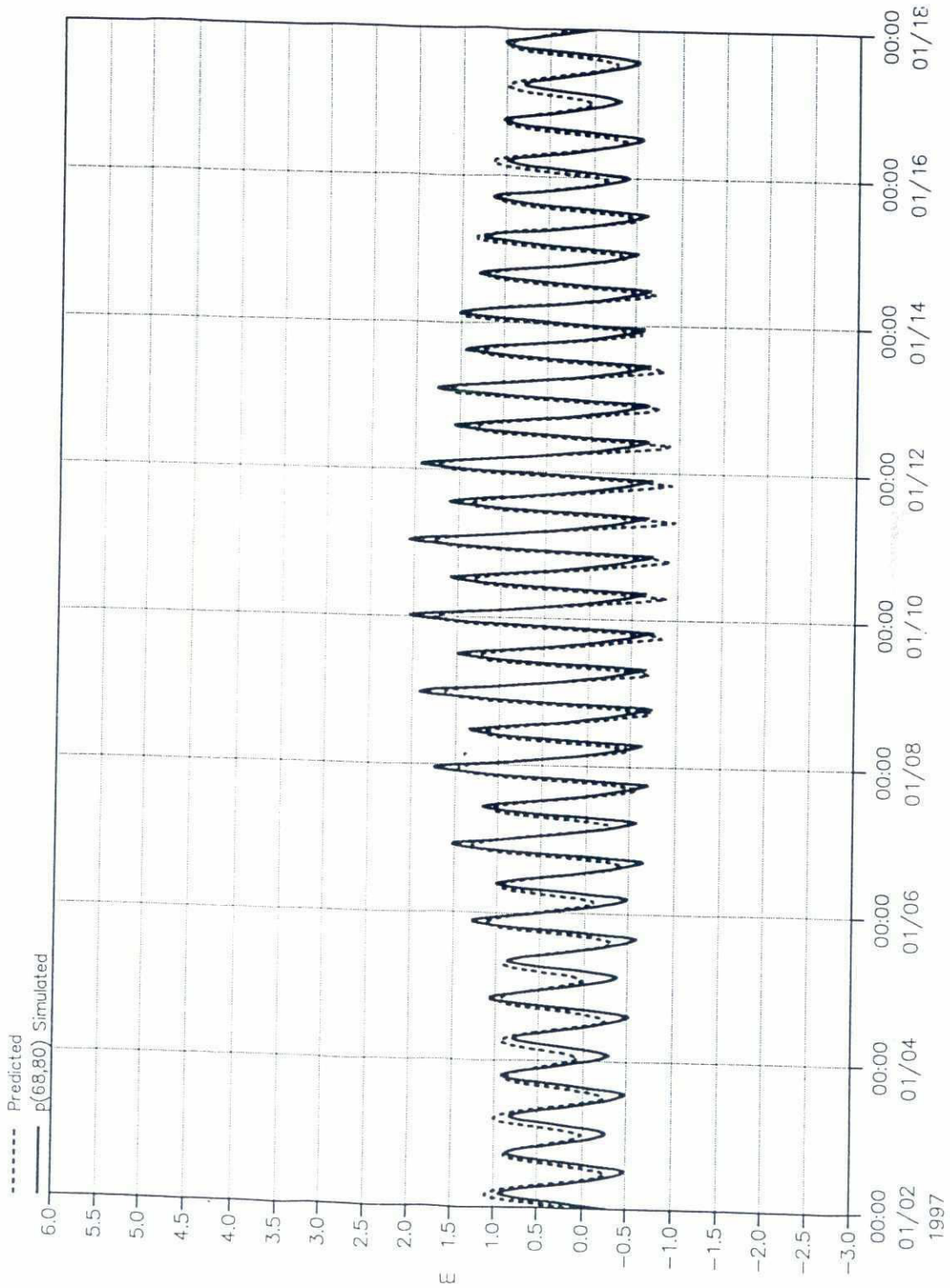


SVMC		Client: BANGLADESH WATER DEVELOPMENT BOARD	MIKE 21
		Project: MEGHNA ESTUARY STUDY	
File:	Date: Sun May 31 1998	Measured and predicted water level at Kutubdia Island (PWD) Dry Season 1997	Drawing no. 4.78
Scale:	Init: p5011		



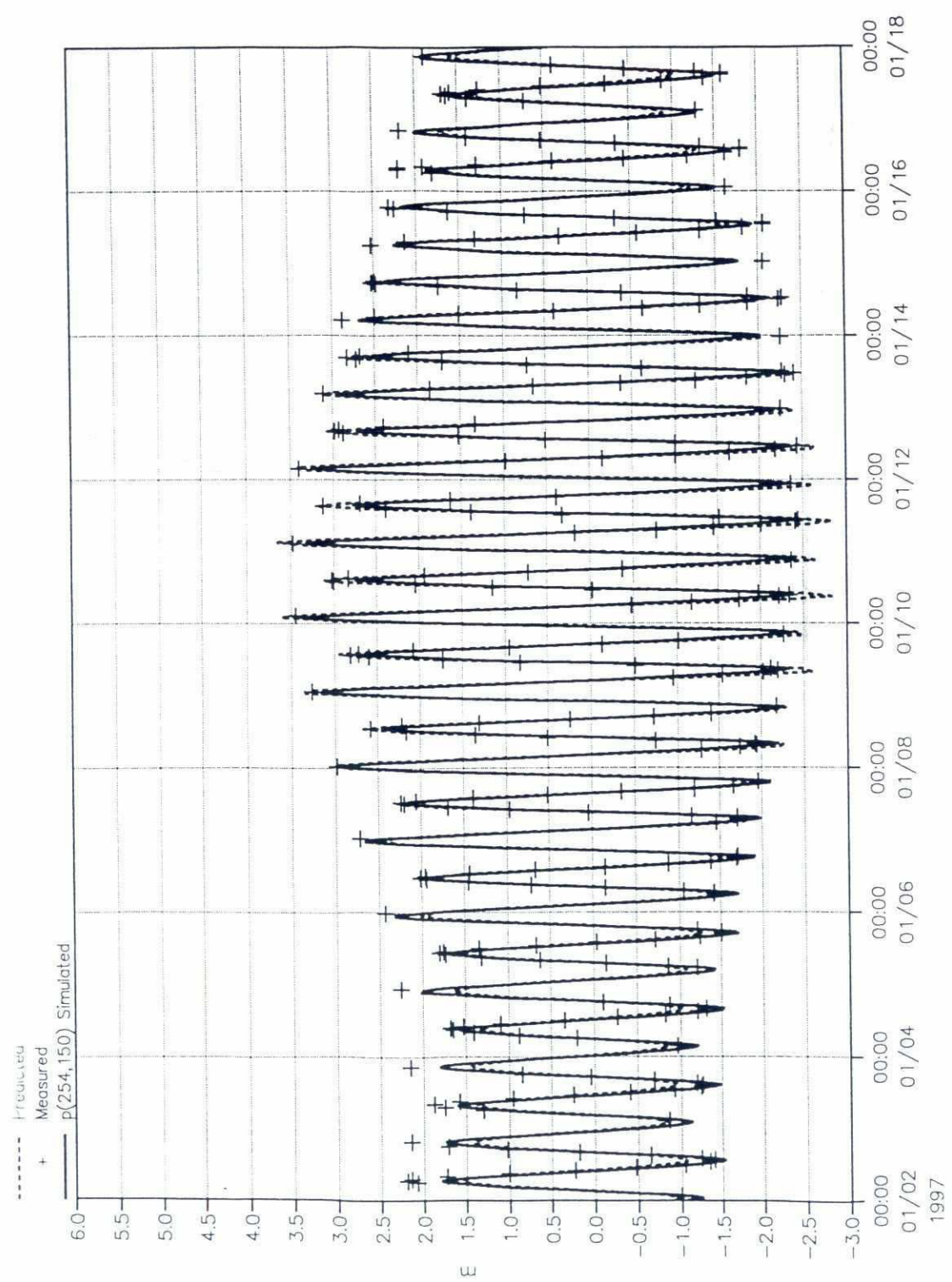
SWMC		Client: BANGLADESH WATER DEVELOPMENT BOARD			MIKE 21
		Project: MEGHNA ESTUARY STUDY			
File:	Date: Sun May 31 1998	Measured and predicted water level at Normans Point (PWD) Dry Season 1997		Drawing no. 4.79	
Scale:	Init: p5011				

202

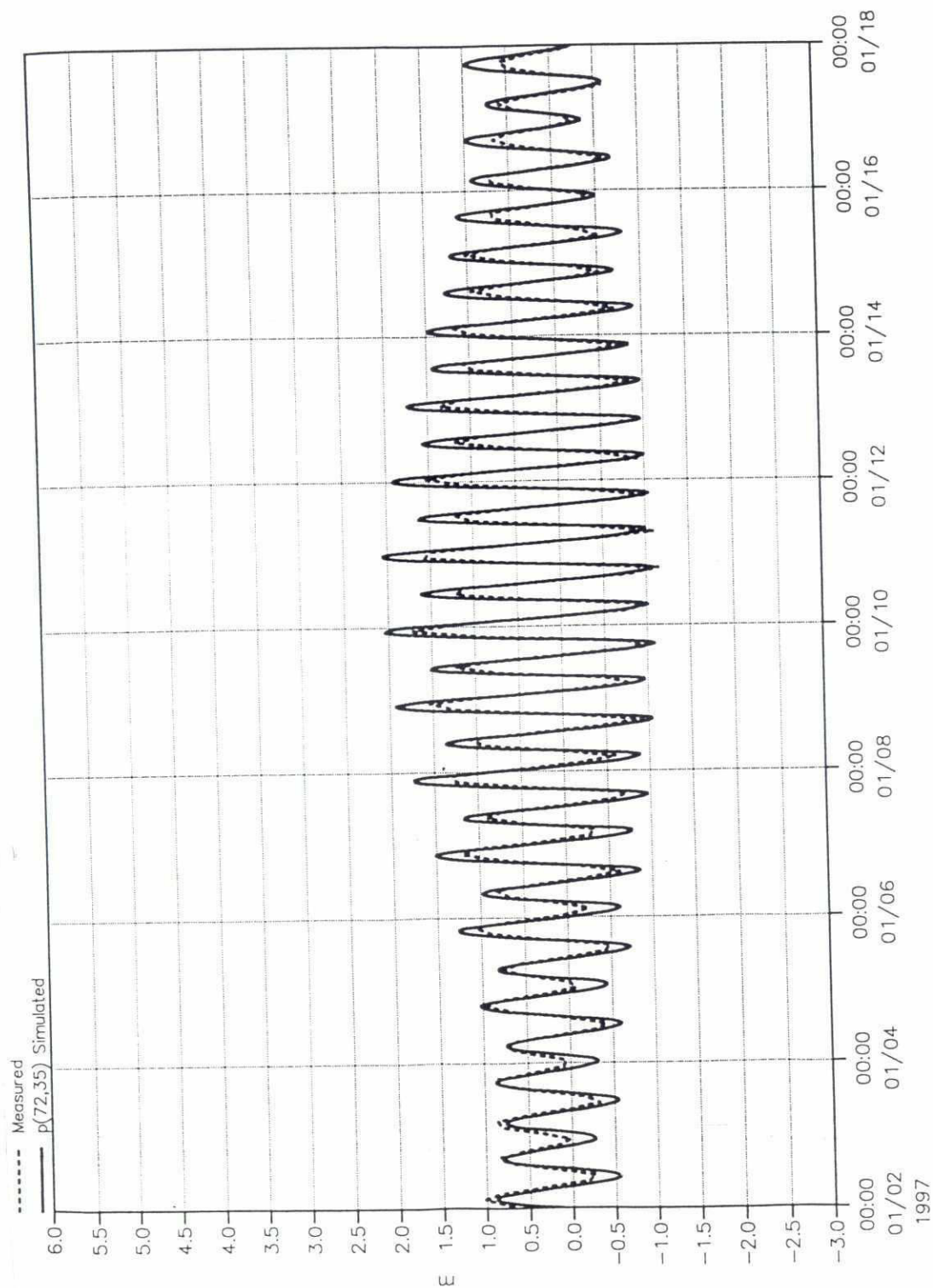


SWMC		Client: BANGLADESH WATER DEVELOPMENT BOARD		MIKE 21	
Date: Sun May 31 1998		Project: MEGHNA ESTUARY STUDY		Drawing no.	
File:		Measured and predicted water level at Rabnabad Channel (PWD)		4.80	
Scale: Init: p5011		Dry season 1997			

268
97 smd197A
180297 smd197C
~297 4507C

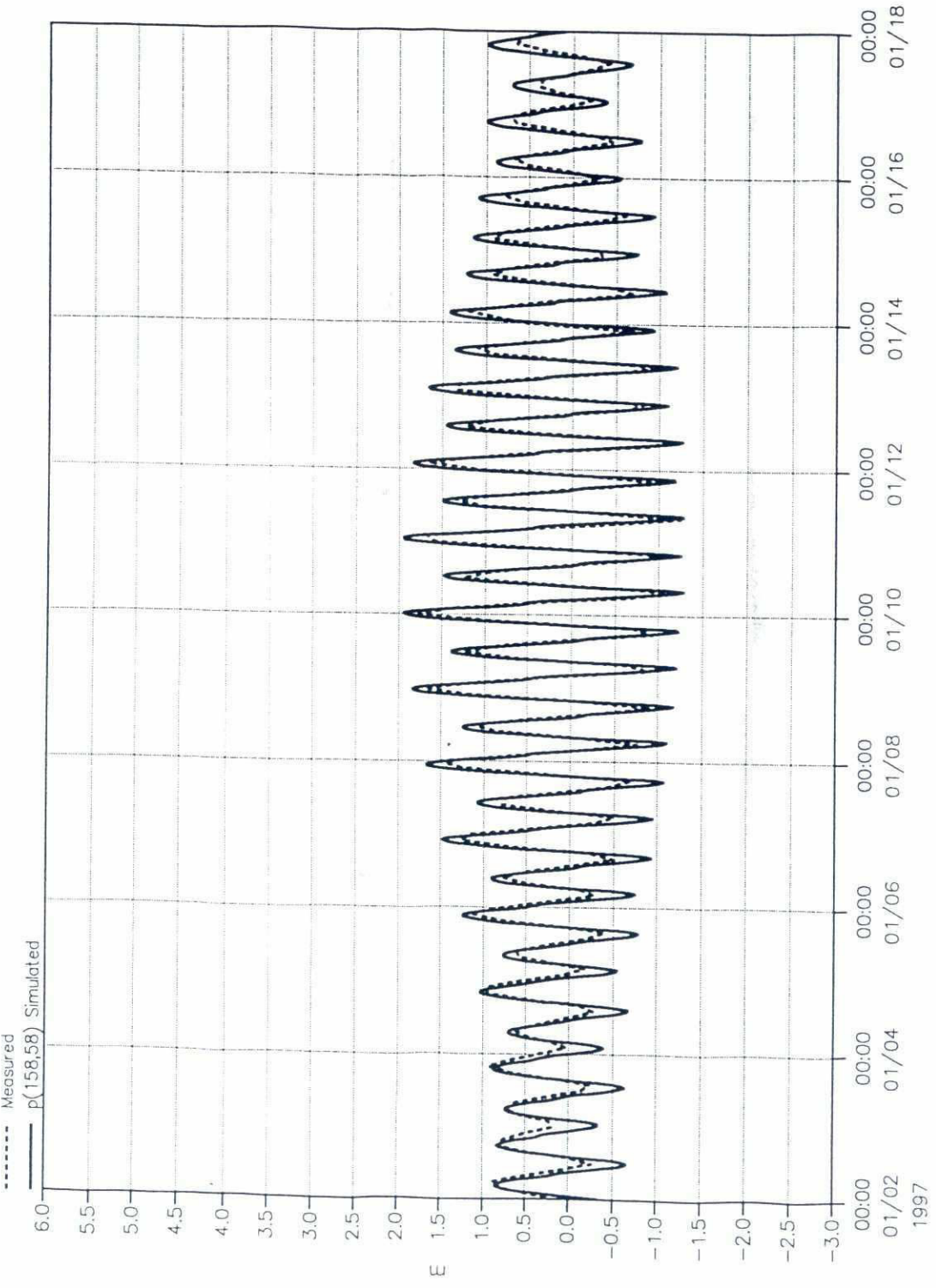


SWMC		Client: BANGLADESH WATER DEVELOPMENT BOARD	MIKE 21
		Project: MEGHNA ESTUARY STUDY	
File:	Date: Sun May 31 1998	Measured, simulated and predicted water level at Sandwip (PWD) Dry Season 1997	
Scale:	Init: p5011		
		Drawing no.	4.82



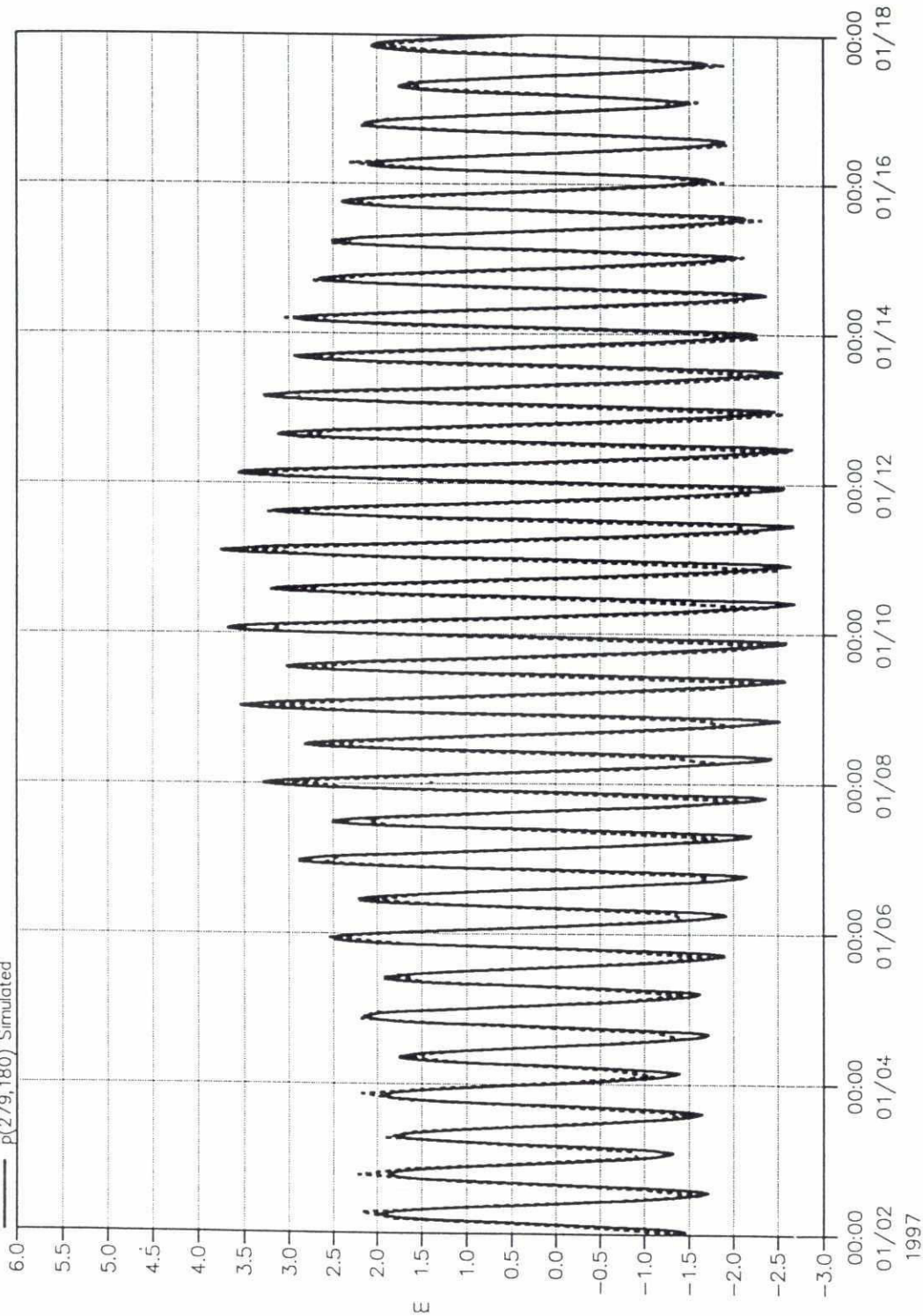
SWMC		Client: BANGLADESH WATER DEVELOPMENT BOARD	MIKE 21
Date: Mon Jun 1 1998		Project: MEGHNA ESTUARY STUDY	
File:		Measured and predicted water level at MES 1 (PWD)	Drawing no. 4.83
Scale:	Init: p5011	Dry Season 1997	

204



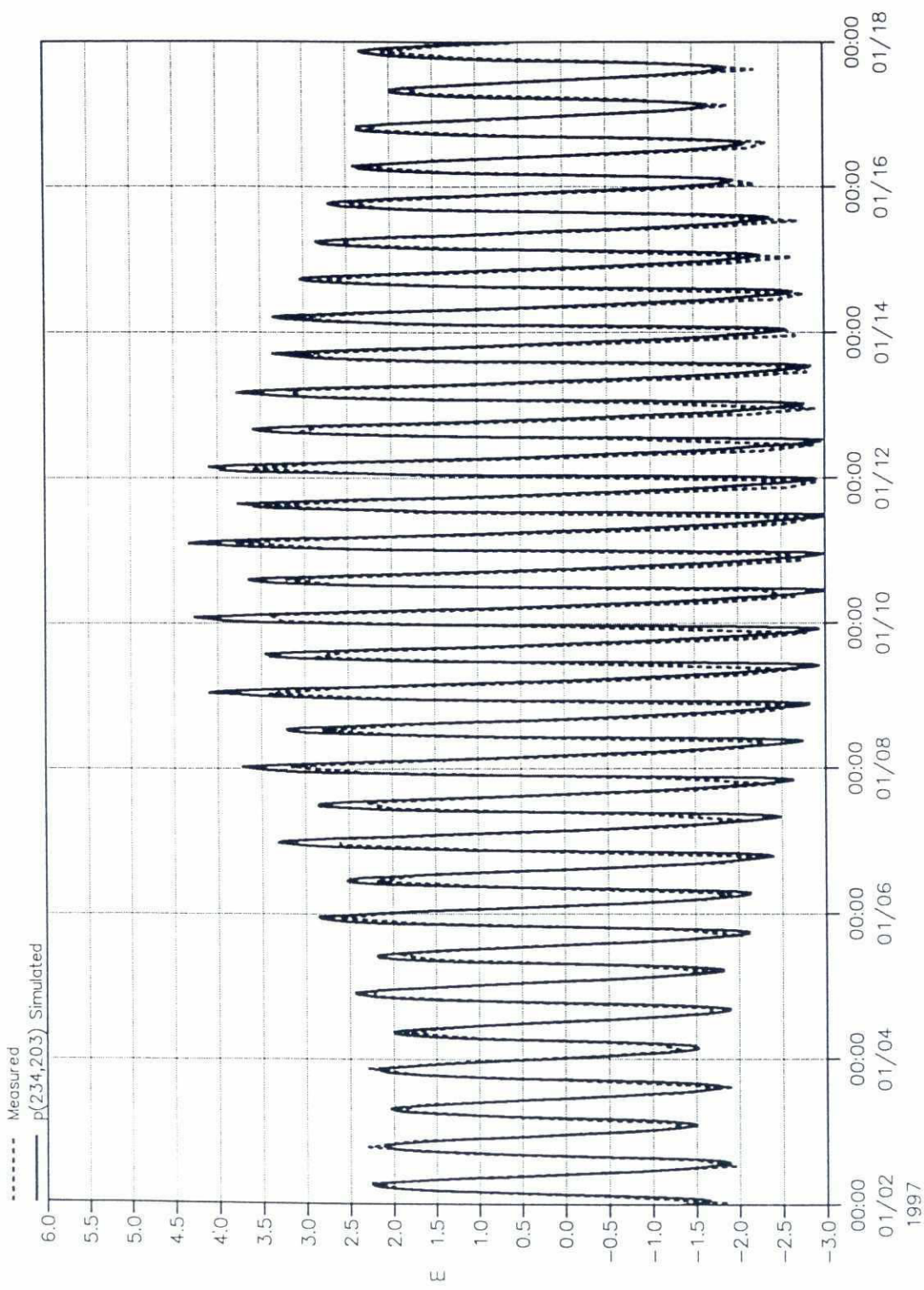
SVMC		Client: BANGLADESH WATER DEVELOPMENT BOARD		MIKE 21
		Project: MEGHNA ESTUARY STUDY		
File:	Date: Mon Jun 1 1998	Measured and predicted water level at MES 2 (PWD) Dry Season 1997		Drawing no. 4.84
Scale:	Init: p5011			

----- Measured
 ——— p(279,180) Simulated

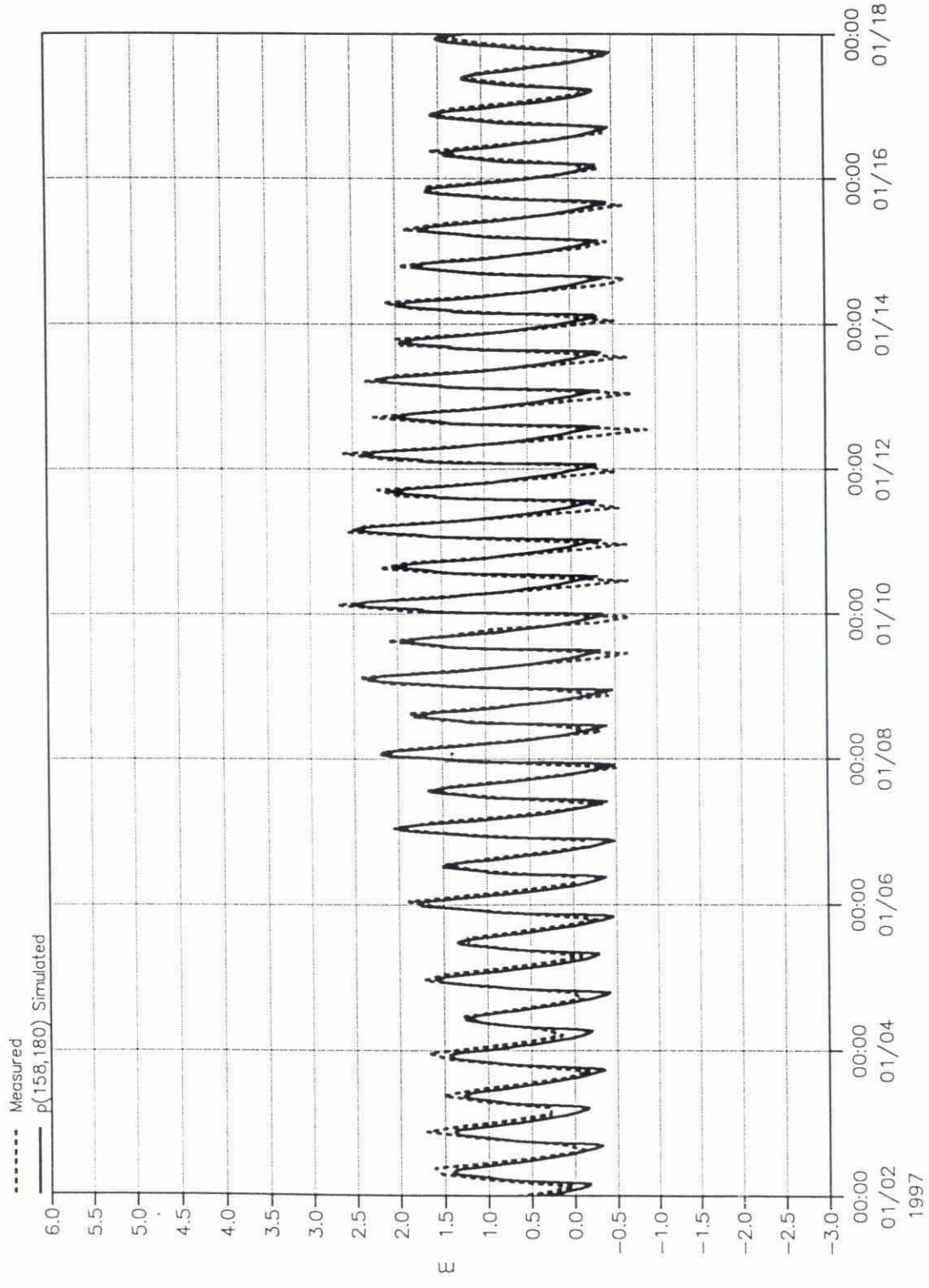


SWMC		Client: BANGLADESH WATER DEVELOPMENT BOARD		MIKE 21
		Project: MEGHNA ESTUARY STUDY		
File:	Date: Mon Jun 1 1998	Measured and predicted water level at MES 4 (PWD)		Drawing no. 4.85
Scale:	Init: p5011	Dry Season 1997		

202

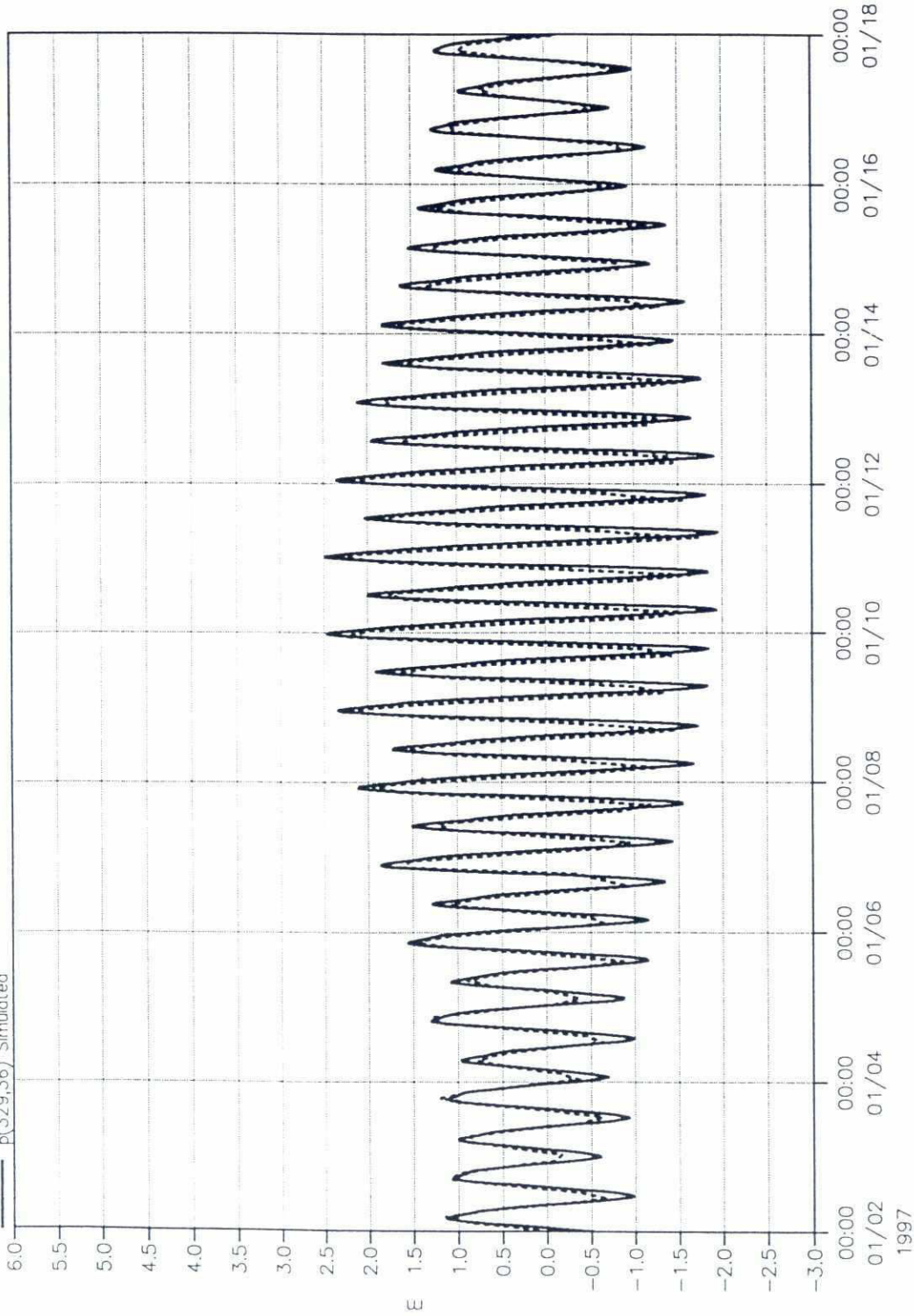


SWMC		Client:	BANGLADESH WATER DEVELOPMENT BOARD		MIKE 21
		Project:	MEGHNA ESTUARY STUDY		
File:	Date: Mon Jun 1 1998	Measured and predicted water level at MES 5 (PWD)		Drawing no.	4.86
Scale:	Unit: p5011	Dry Season 1997			



SWMC		Client: BANGLADESH WATER DEVELOPMENT BOARD	MIKE 21
		Project: MEGHNA ESTUARY STUDY	
File:	Date: Mon Jun 1 1998	Measured and predicted water level at MES 6 (PWD) Dry Season 1997	
Scale:	Init: p5011		
		Drawing no.	4.87

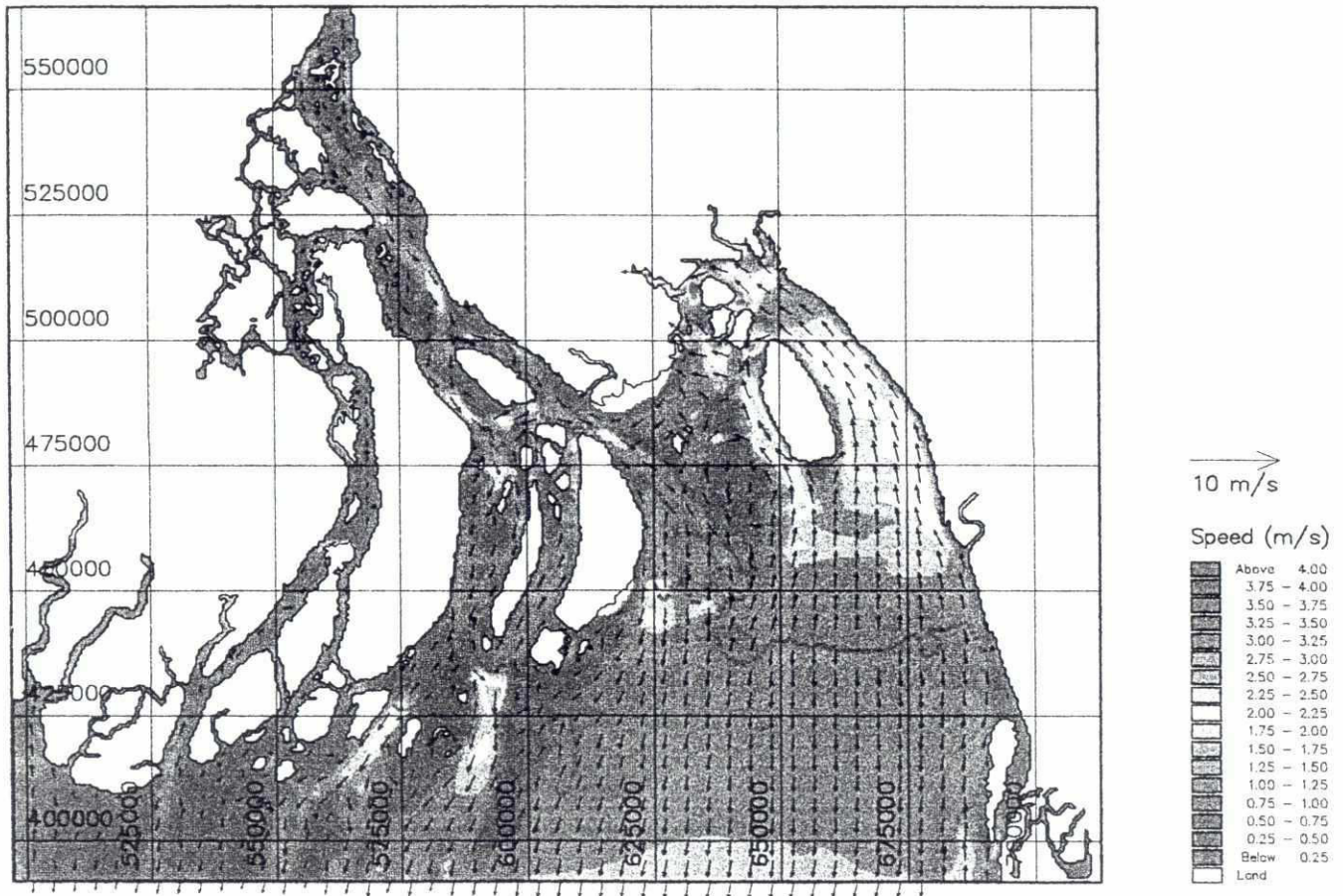
----- Measured
—— p(329,36) Simulated



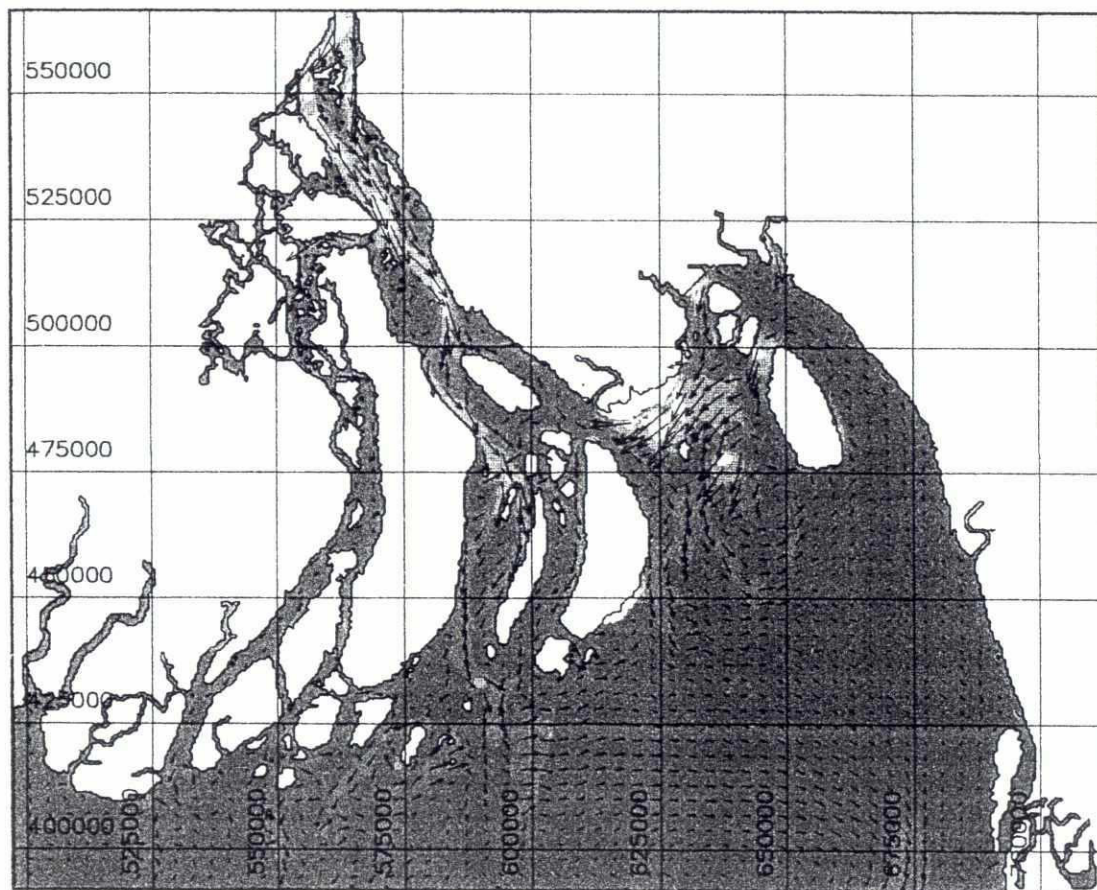
SVMC		Client:	BANGLADESH WATER DEVELOPMENT BOARD		MIKE 21
		Project:	MEGHNA ESTUARY STUDY		
File:	Date: Mon Jun 1 1998	Measured and predicted water level at SE (PWD) Dry Season 1997		Drawing no. 4.88	
Scale:	Init: p5011				

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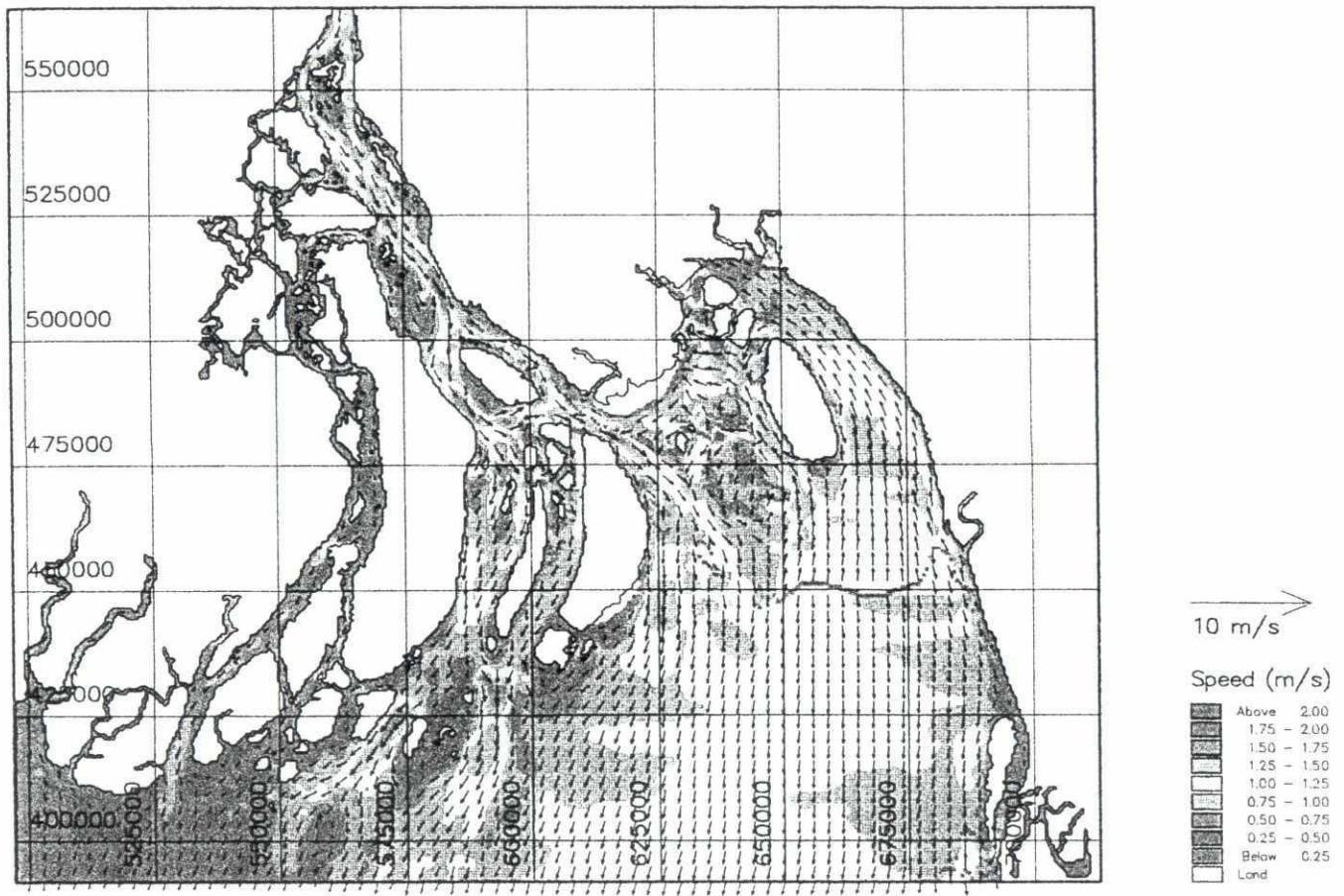
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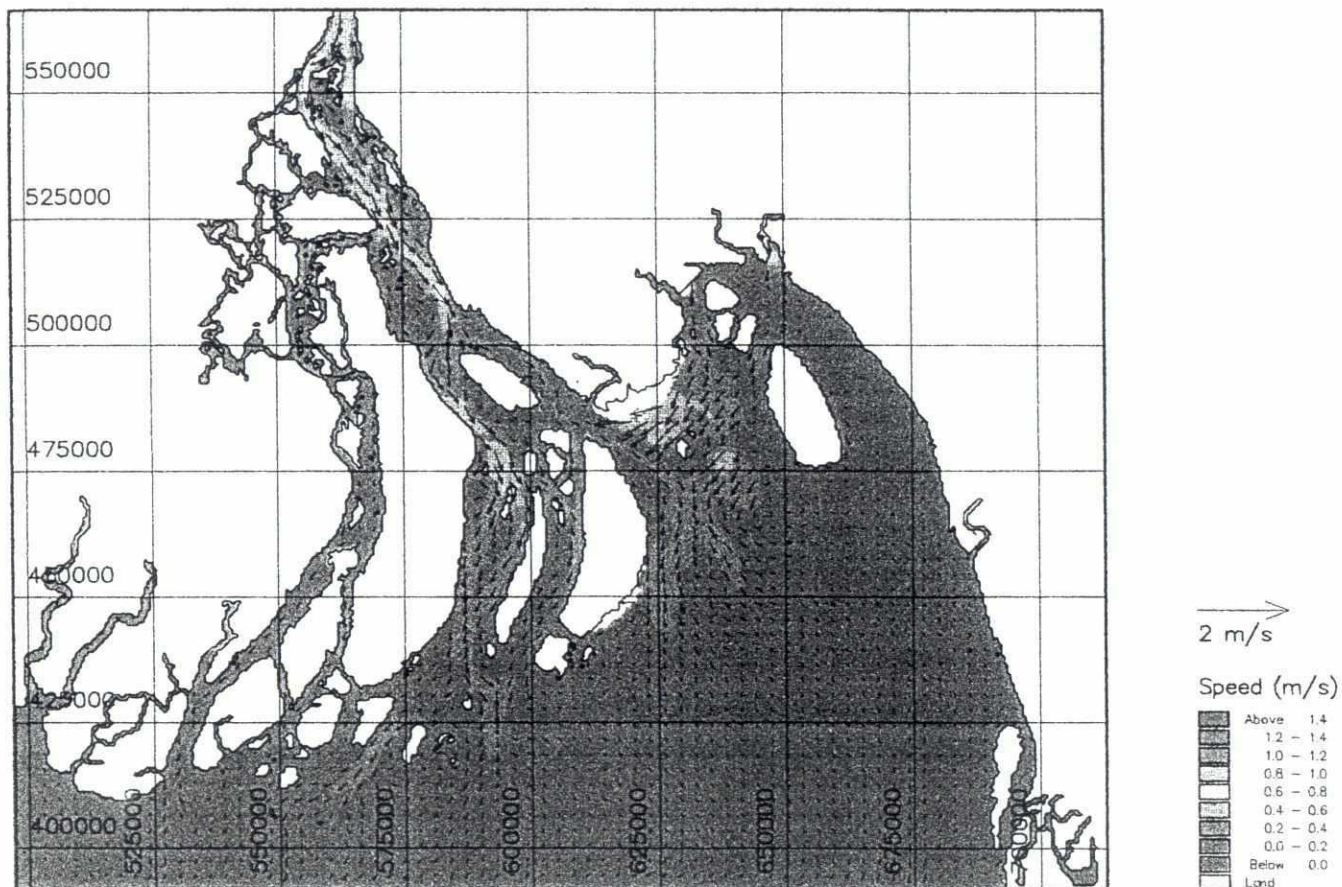
SWMC		Client:	Bangladesh Water Development Board	MIKE 21
		Project:	Meghna Estuary Study	
File:	Date: Mon Jun 8 1998	Max velocities for Spring Tide, Dry Season 1996 Existing situation		Drawing no. 5.1
Scale: 1:1500000	Init: p5011			



<div>SWMC</div>		Client:	Bangladesh Water Development Board	MIKE 21
		Project:	Meghna Estuary Study	
File:	Date: Mon Jun 8 1998	Net flow for Spring Tide, Dry Season 1996 Existing situation		Drawing no. 5.2
Scale: 1:1500000	Init: p5011			



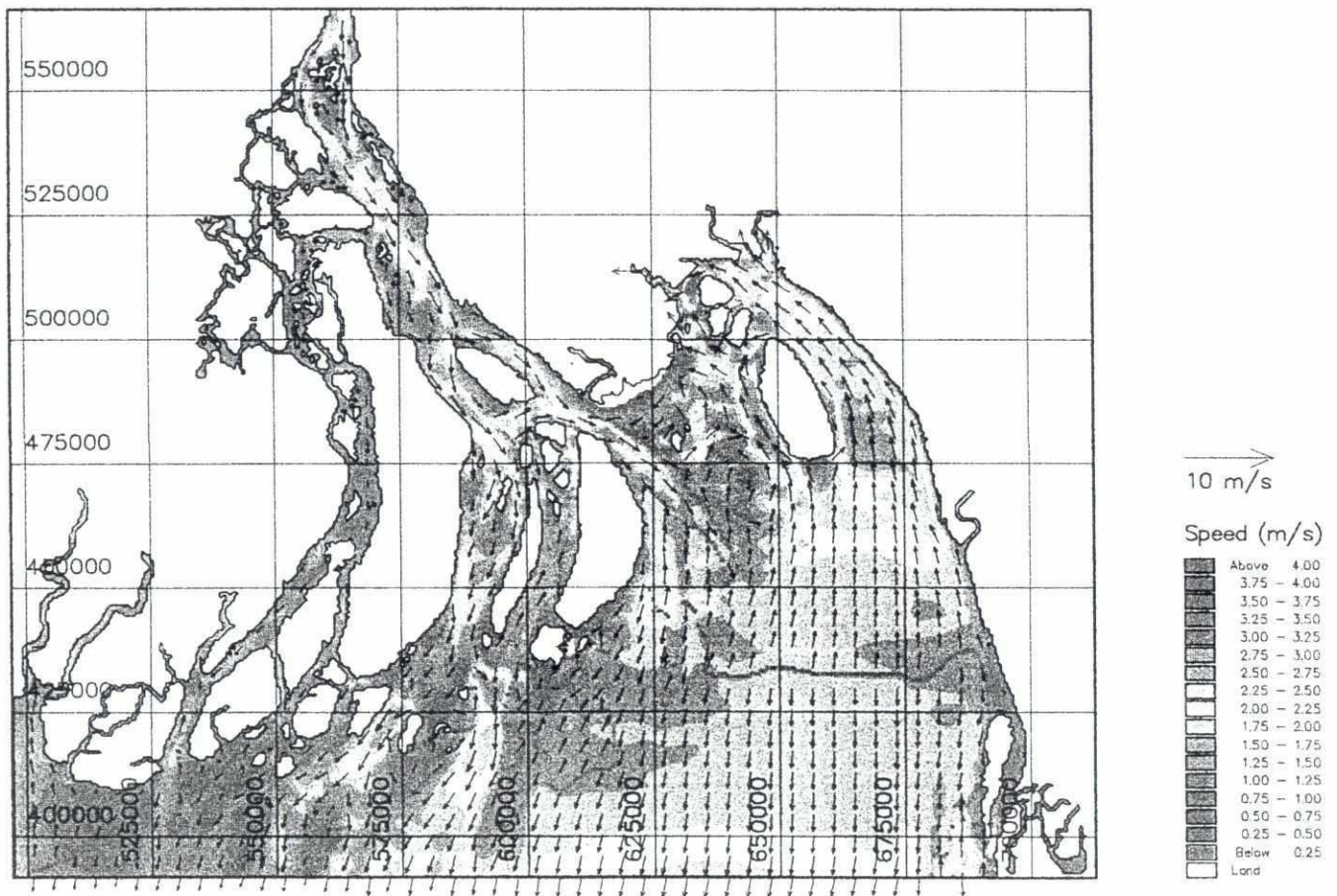
SWMC		Client:	Bangladesh Water Development Board	MIKE 21
		Project:	Meghna Estuary Study	
File:	Date: Mon Jun 8 1998	Max velocities for Neap Tide, Dry Season 1996 Existing situation		Drawing no. 5.3
Scale: 1:1500000	Init: p5011			



SWMC		Client:	Bangladesh Water Development Board	MIKE 21
		Project:	Meghna Estuary Study	
File:	Date: Mon Jun 8 1998	Net flow for Neap Tide, Dry Season 1996 Existing situation	Drawing no. 5.4	
Scale: 1:1500000	Init: p5011			

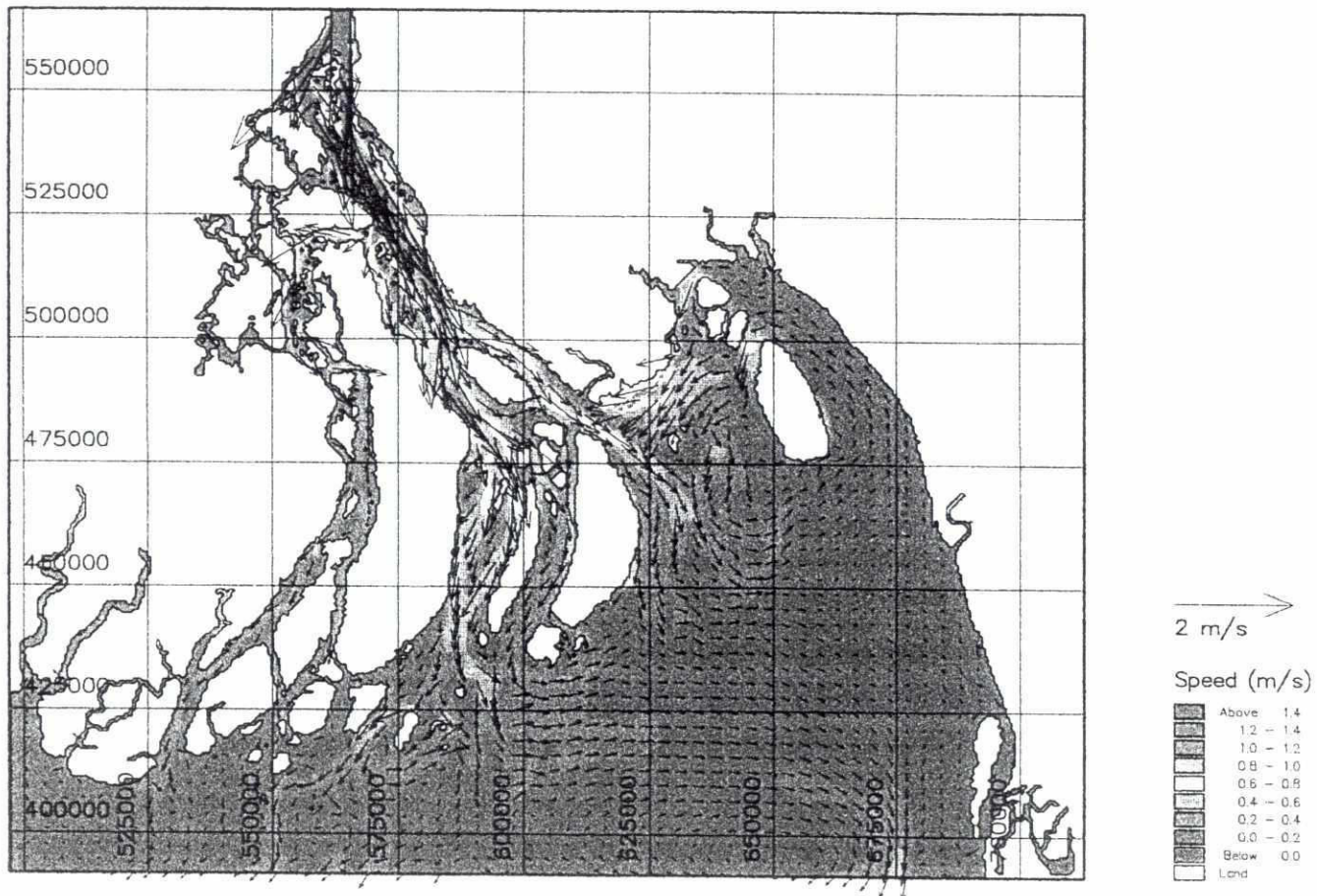
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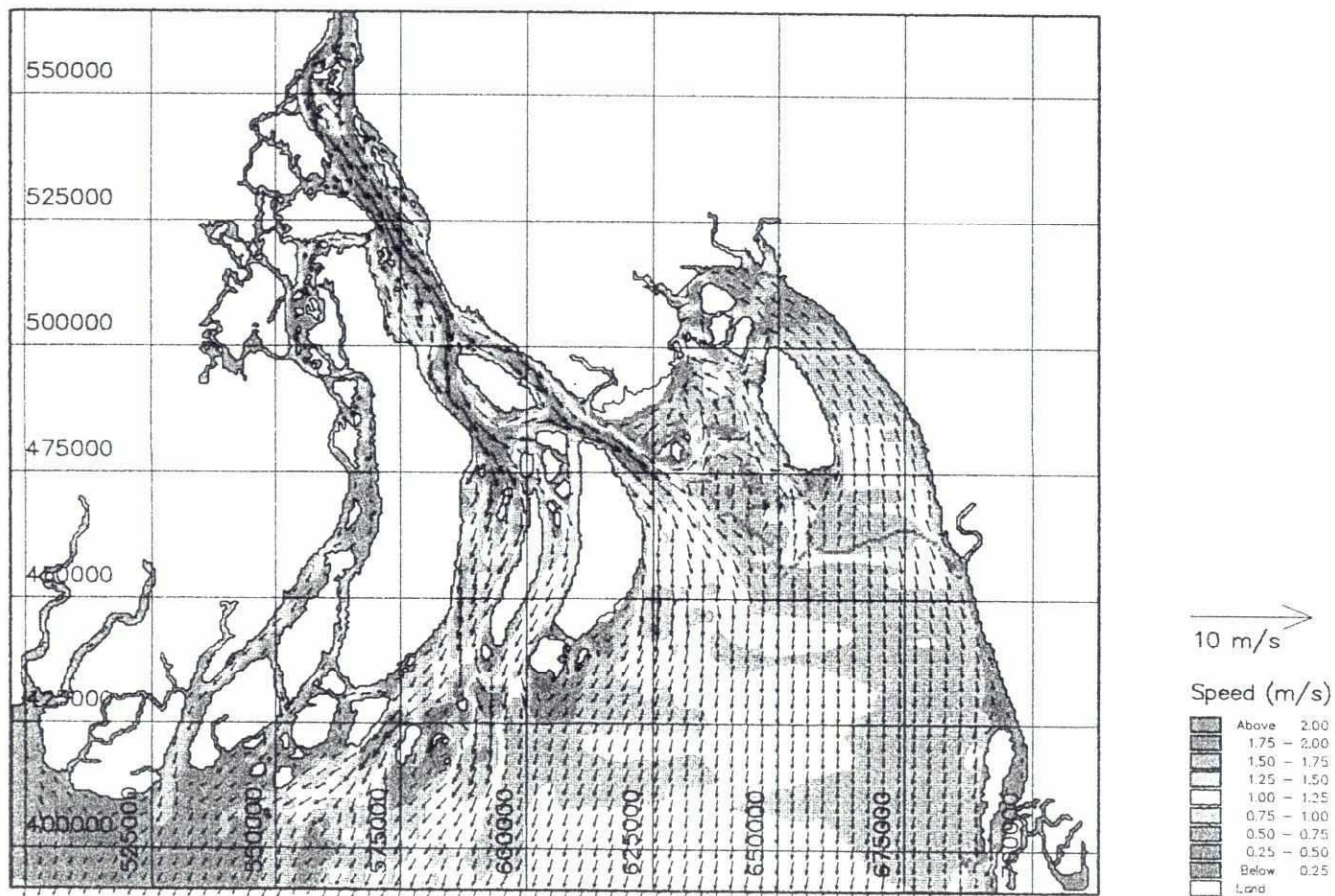


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		Project:	Meghna Estuary Study	
File:	Date: Mon Jun 8 1998	Max velocities for Spring Tide, Monsoon Season 1997 Existing situation		Drawing no. 5.5
Scale: 1:1500000	Int: p5011			

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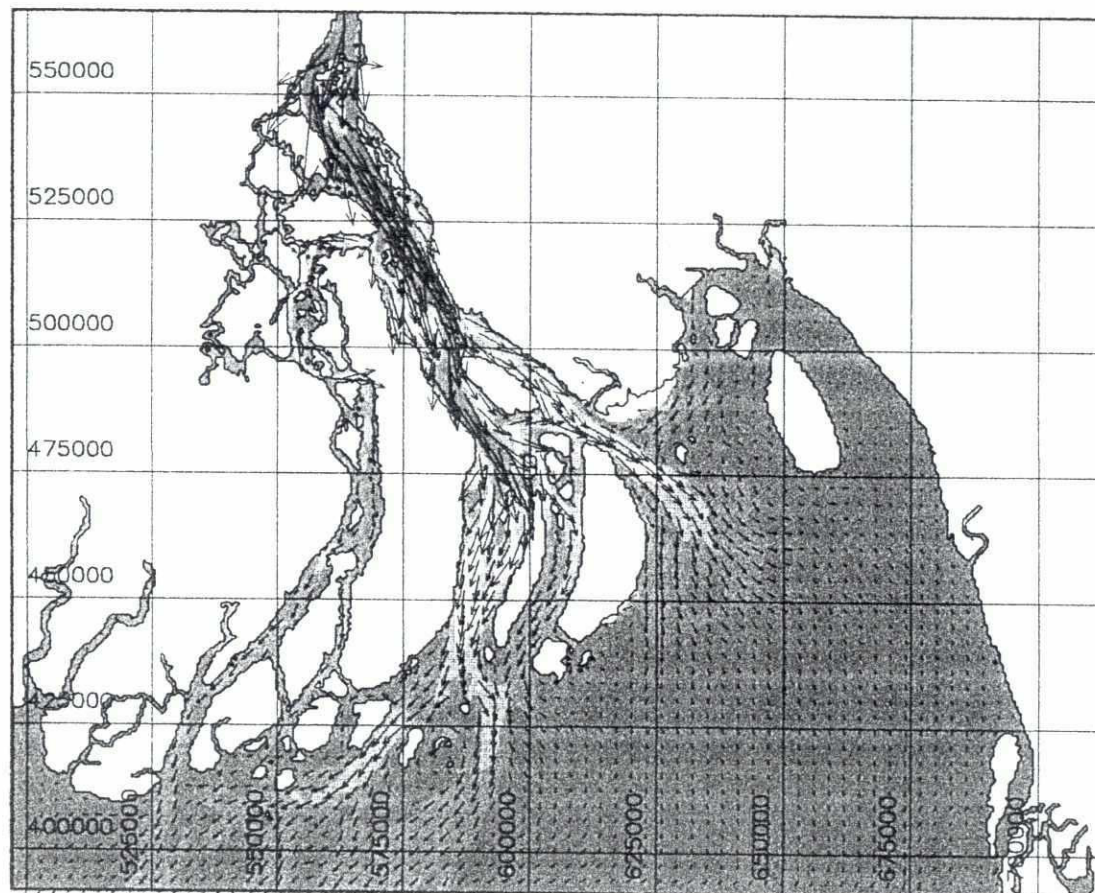
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File:	Date: Mon Jun 8 1998	Net flow for Spring Tide, Monsoon Season 1997 Existing situation			Drawing no.
Scale: 1:1500000	Int: p5011				5.6



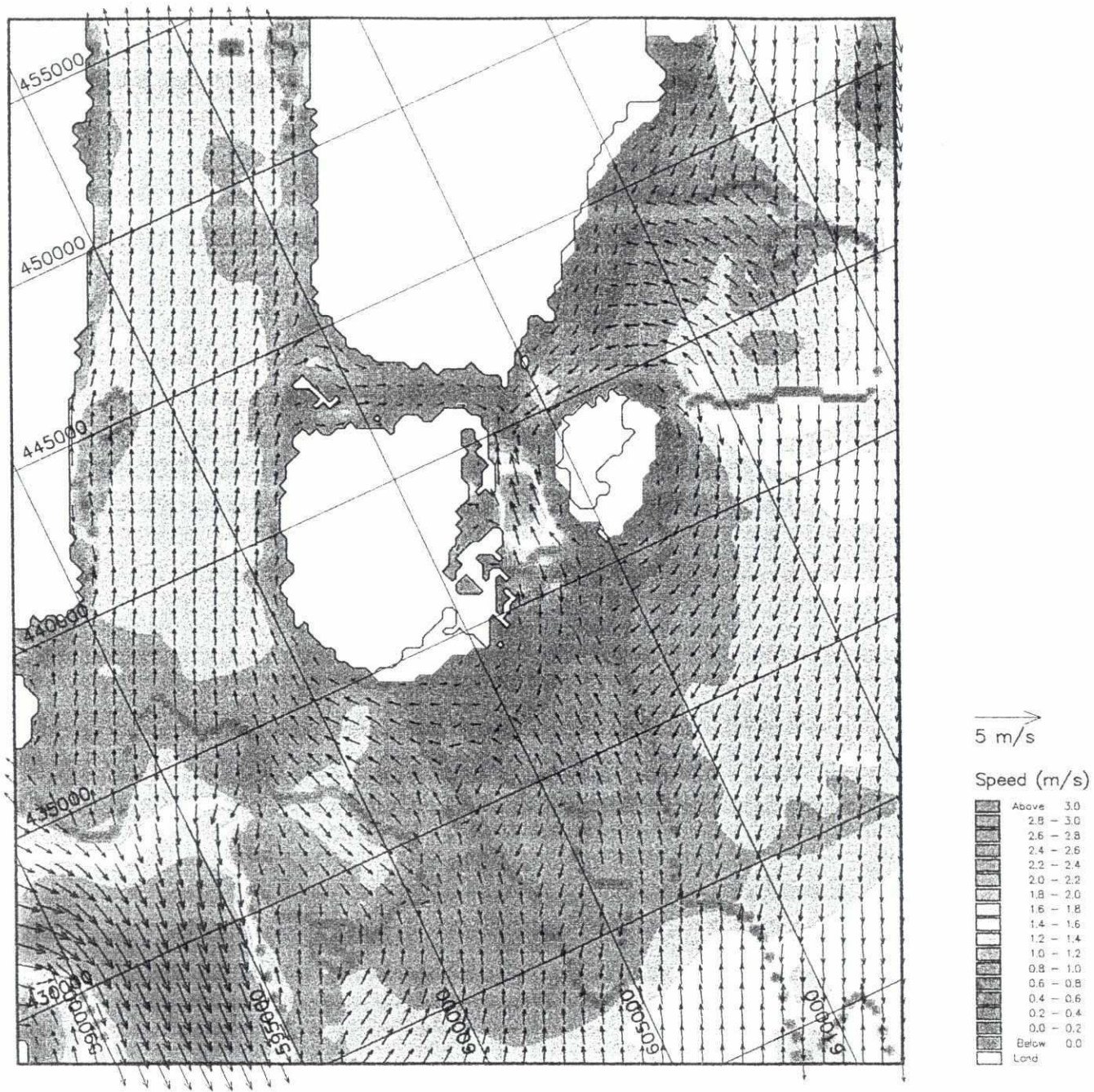
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File:	Date: Mon Jun 8 1998	Max velocities for Neap Tide, Monsoon Season 1997 Existing situation		Drawing no.
Scale: 1:1500000	Int: p5011			5.7

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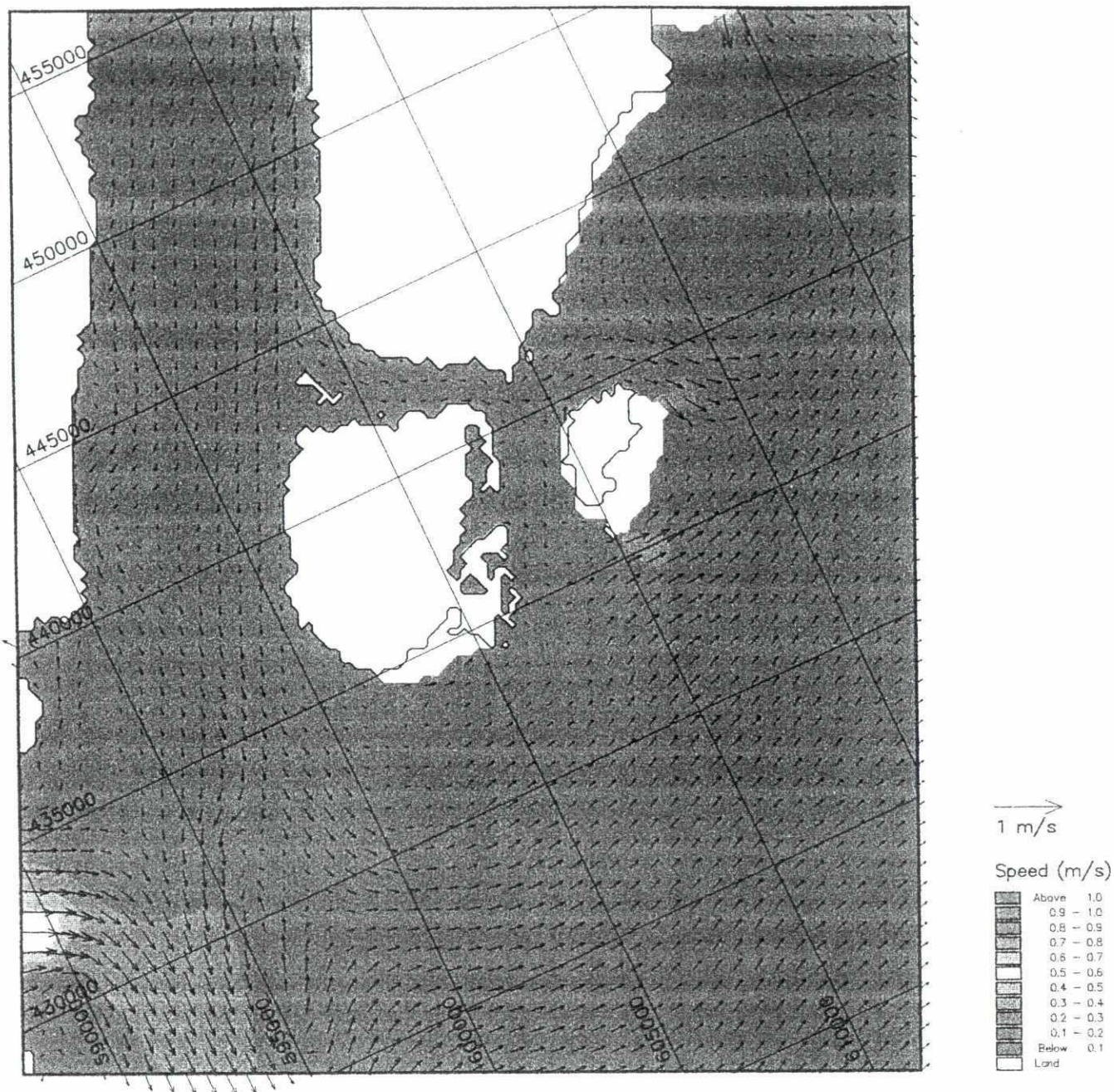
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		Project:	Meghna Estuary Study	
File:	Date: Mon Jun 8 1998	Net flow for Neap Tide, Monsoon Season 1997 Existing situation	Drawing no. 5.8	
Scale: 1:1500000	Init: p5011			



SWMC		Client:	Bangladesh Water Development Board		MIKE 21
		Project:	Meghna Estuary Study		
File:	Date: Mon Jun 8 1998	Max velocities for Spring Tide, Dry Season 1996 Existing situation			Drawing no.
Scale: 1:185000	Int: p5011				5.9

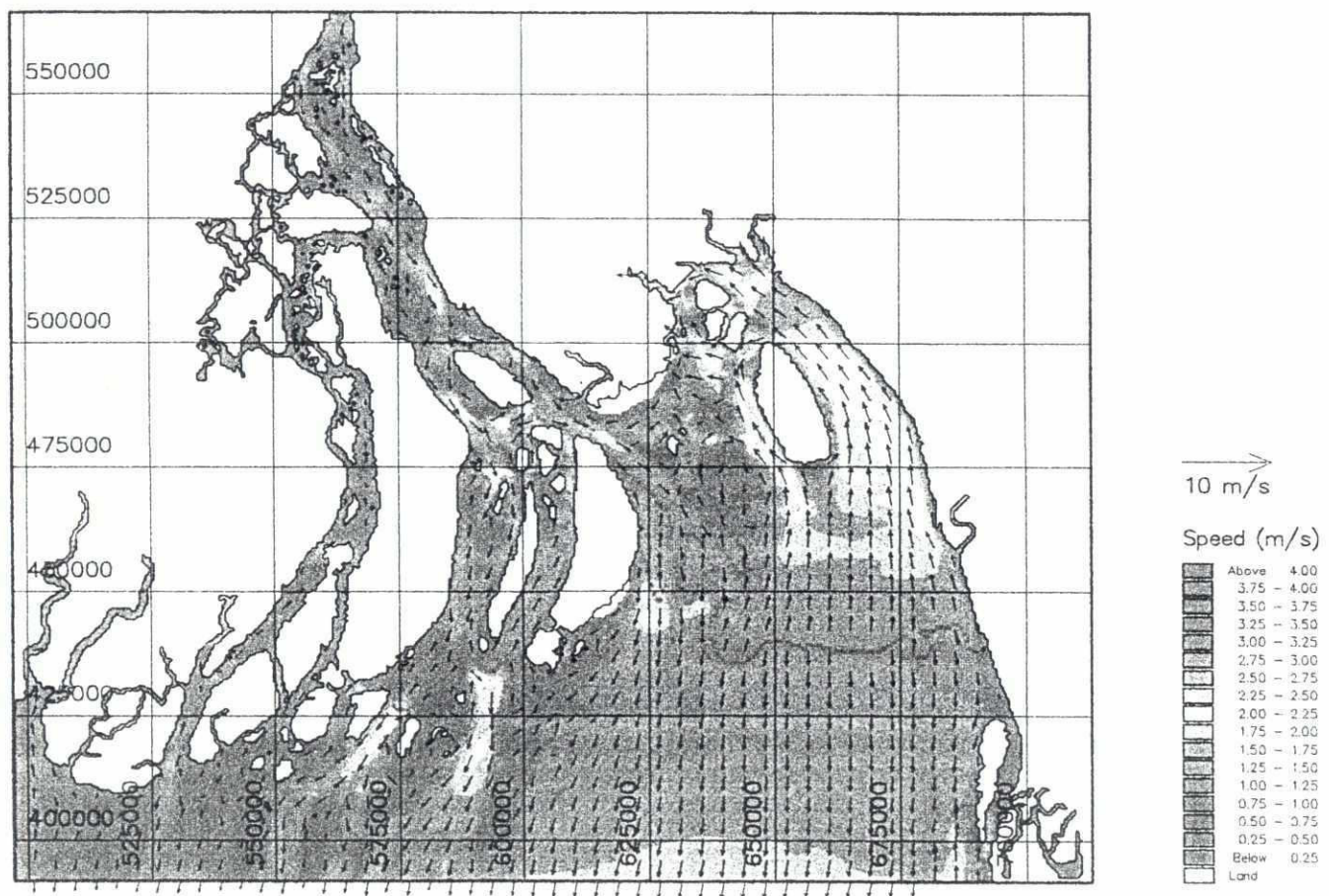
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USDA 10/96



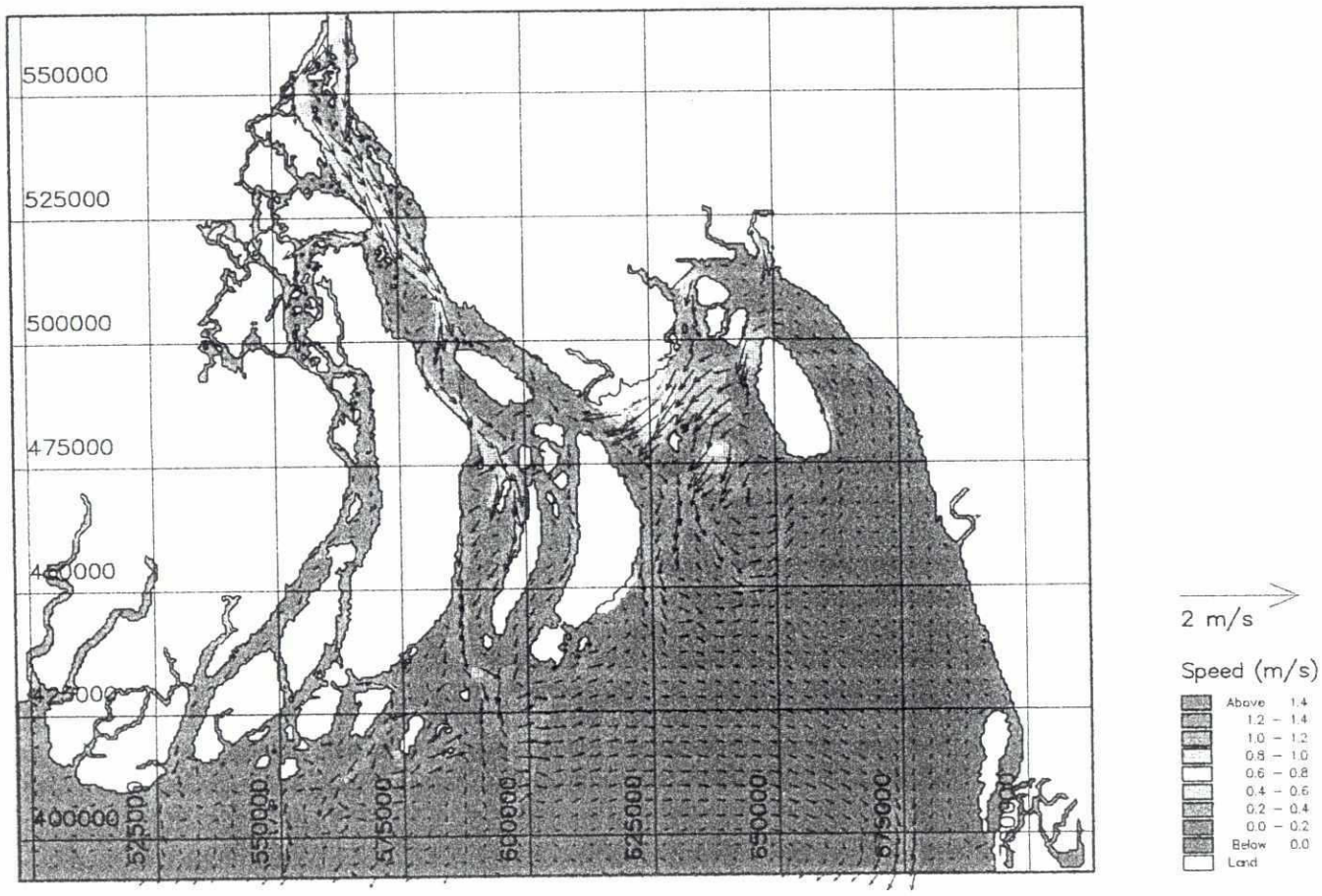
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		Project:	Meghna Estuary Study	
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222

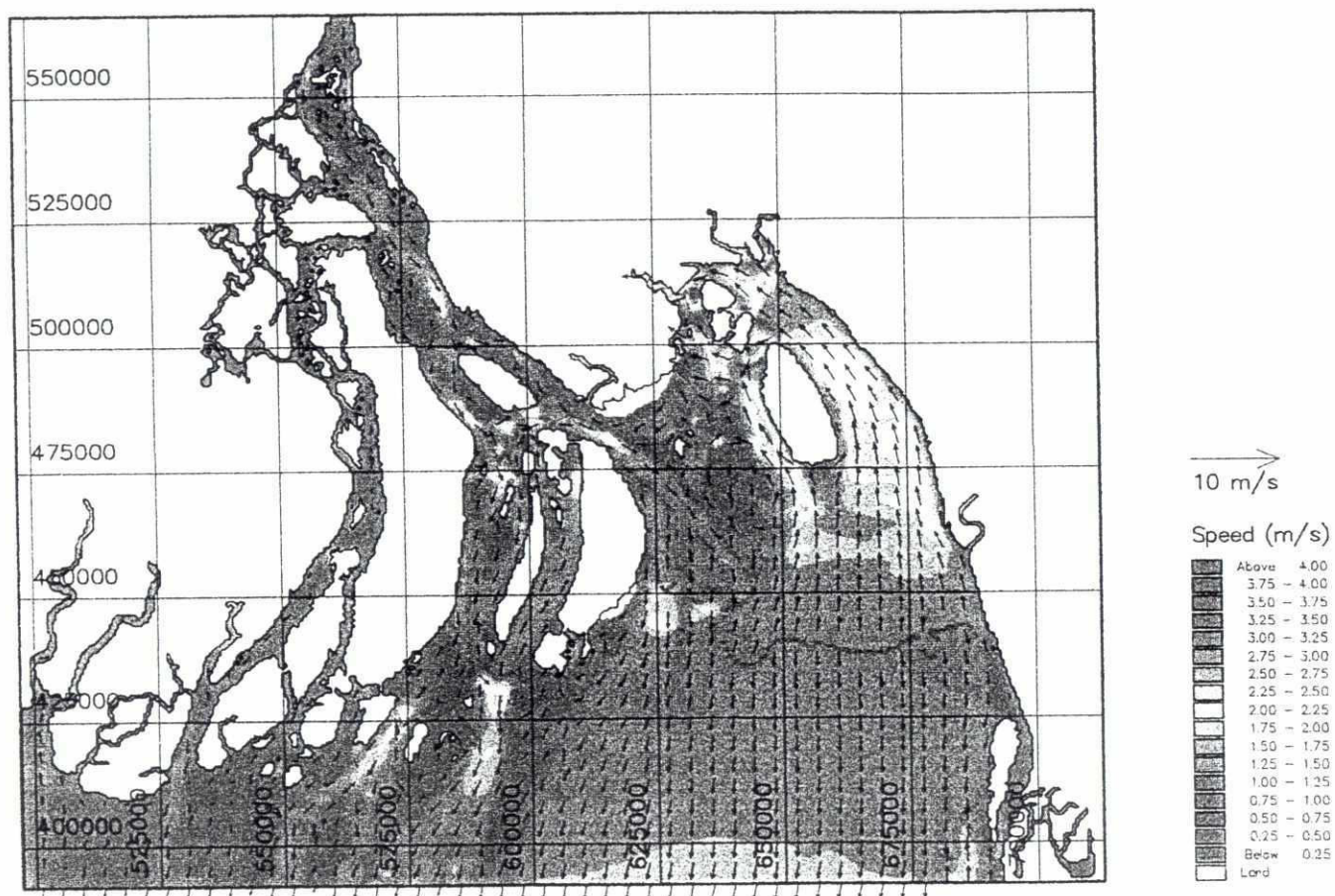


SWMC		Client:	Bangladesh Water Development Board	MIKE 21
		Project:	Meghna Estuary Study	
File:	Date: Mon Jun 8 1998	Max velocities for Spring Tide, Dry Season 1996 Intervention Schemes 1 and 3		Drawing no.
Scale: 1:1500000	Init: p5011			6.1

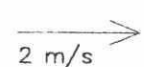
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<div style="text-align: center; font-size: 24px; font-weight: bold;">SWMC</div>		Client:	Bangladesh Water Development Board	MIKE 21
		Project:	Meghna Estuary Study	
File:	Date: Mon Jun 8 1998	Net flow for Spring Tide, Dry Season 1996 Intervention Schemes 1 and 3		Drawing no. <div style="font-size: 24px; font-weight: bold;">6.2</div>
Scale: 1:1500000	Unit: p5011			



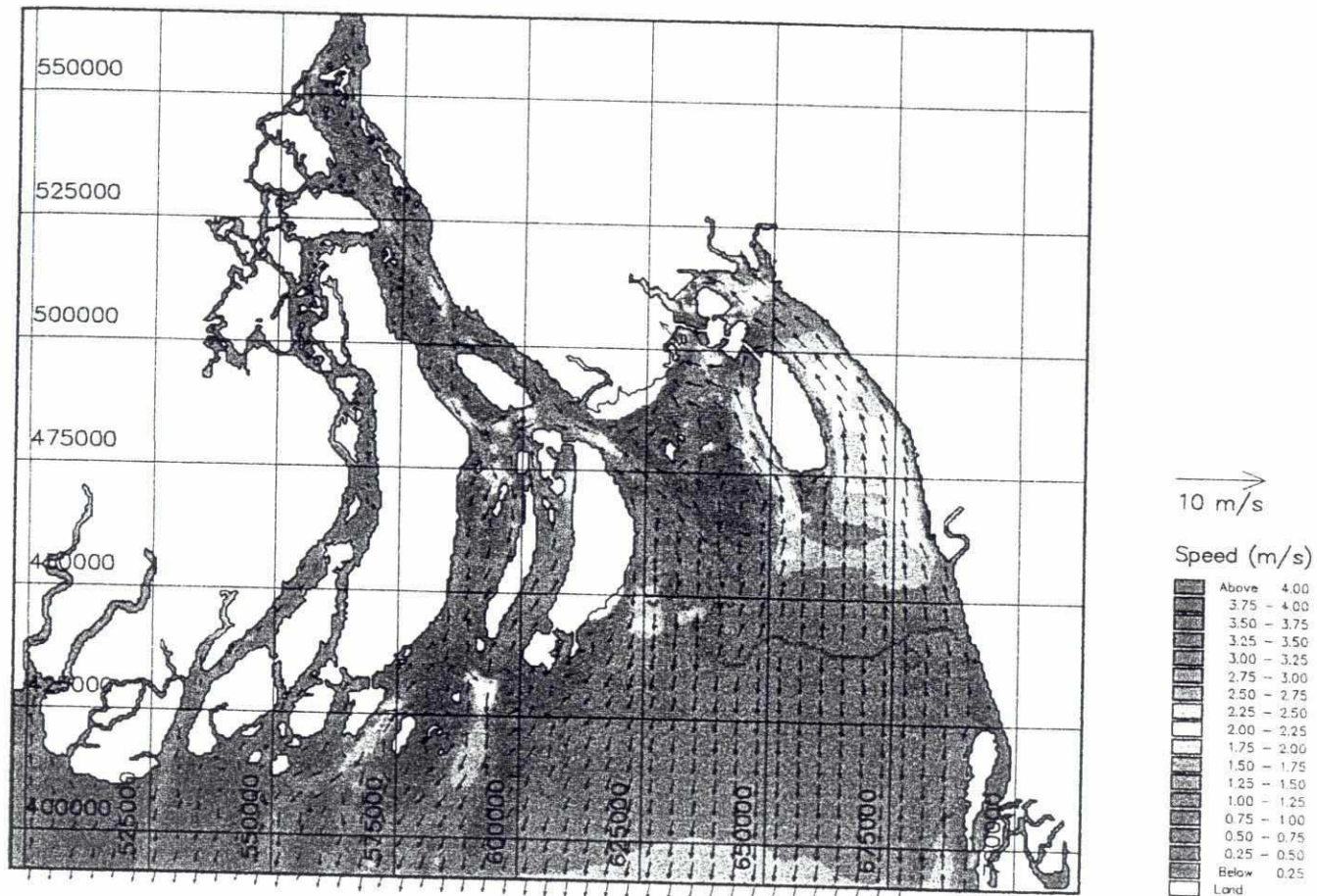
SWMC		Client:	Bangladesh Water Development Board		MIKE 21
		Project:	Meghna Estuary Study		
File:	Date: Mon Jun 8 1998	Max velocities for Spring Tide, Dry Season 1996 All intervention Schemes, excl. 8			Drawing no. 6.3
Scale: 1:1500000	Init: p5011				



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		Project: Meghna Estuary Study		
File:	Date: Mon Jun 8 1998	Net flow for Spring Tide, Dry Season 1996 All intervention Schemes, excl. 8		Drawing no. <div style="font-size: 1.5em;">6.4</div>
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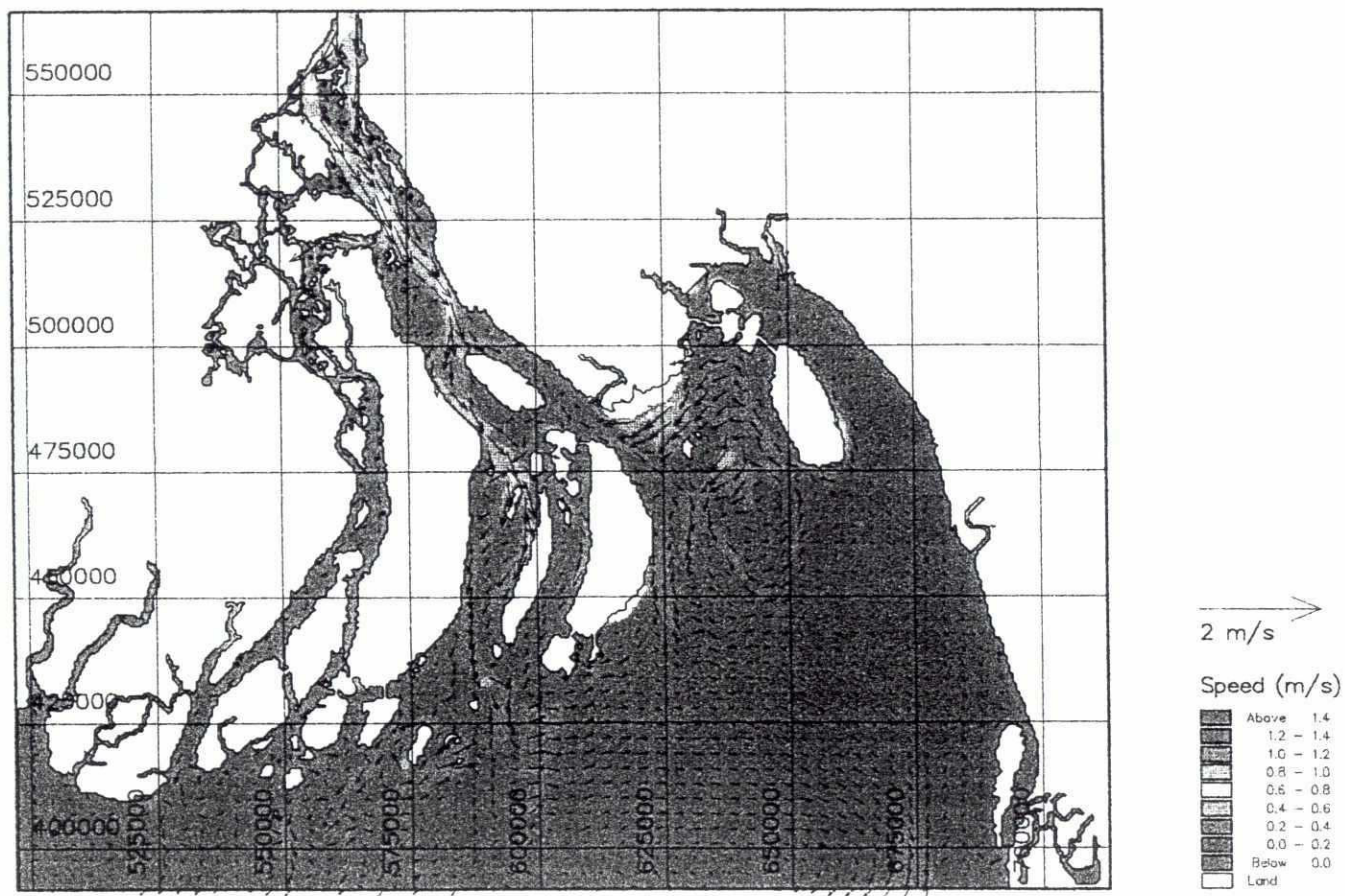
USP/14/ 96/4



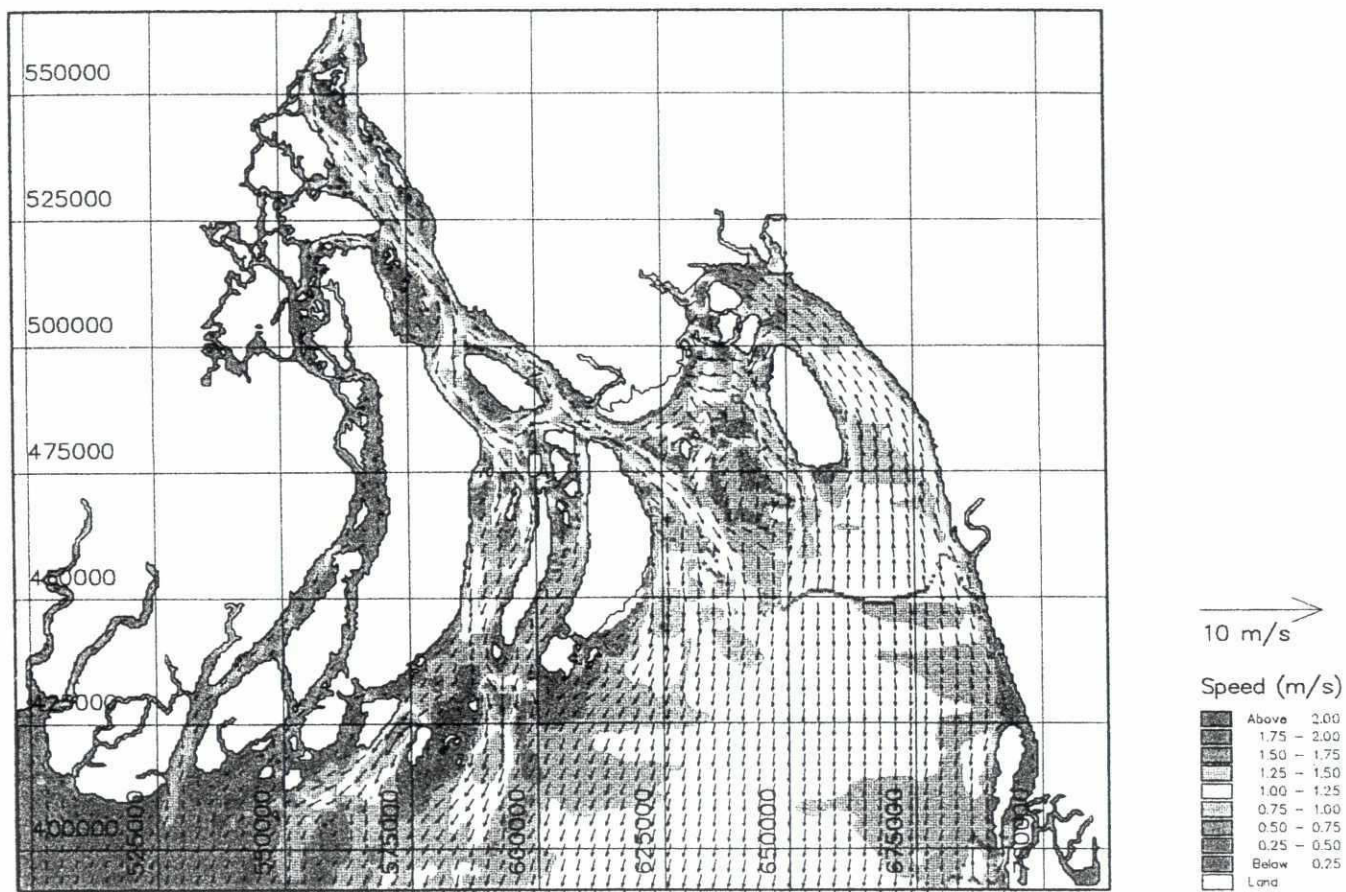
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File:	Date: Mon Jun 8 1998	Max velocities for Spring Tide, Dry Season 1996 All intervention Schemes	Drawing no. 6.5	
Scale: 1:1500000	Init: p5011			

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USP/BAW 91



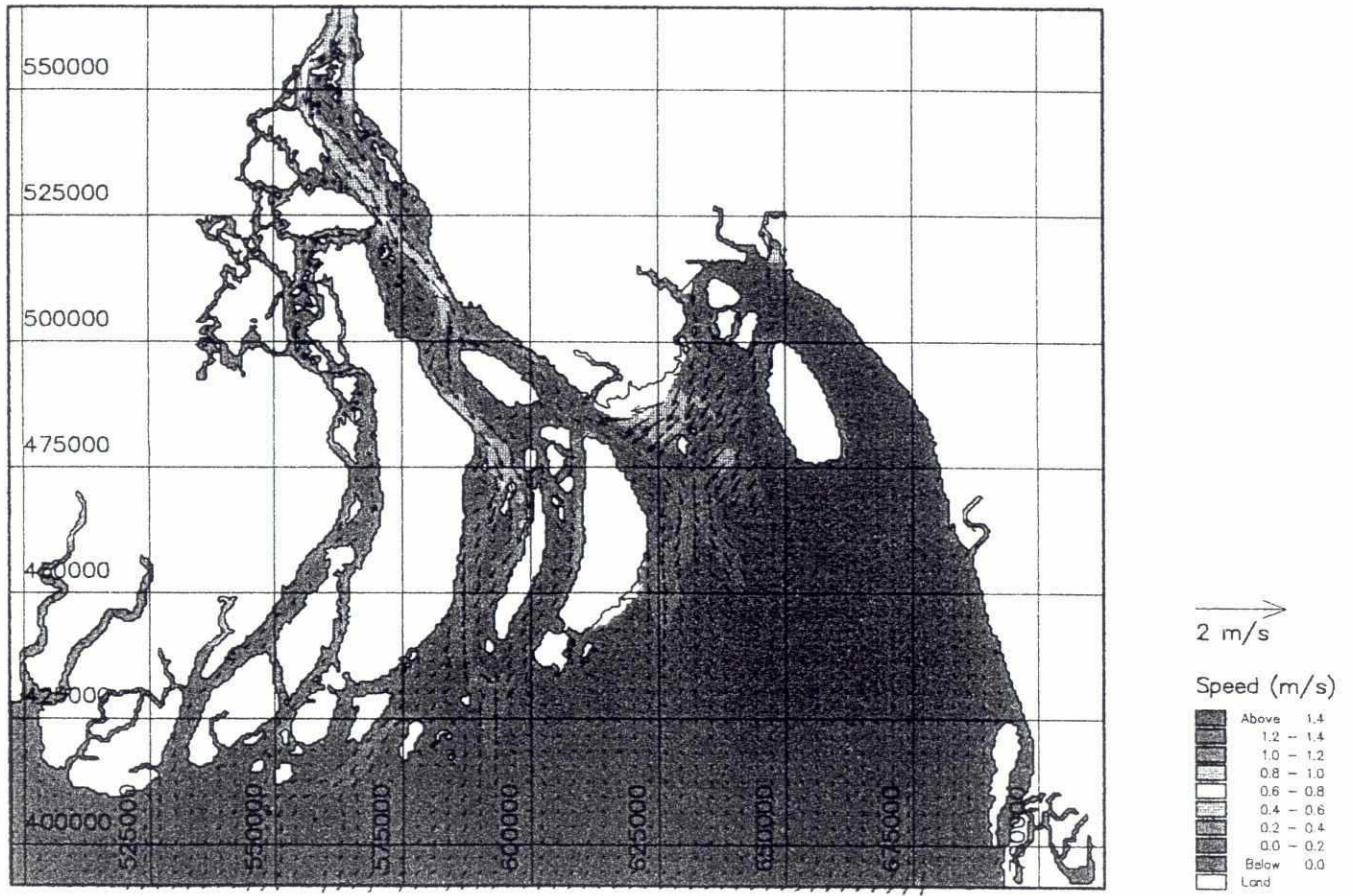
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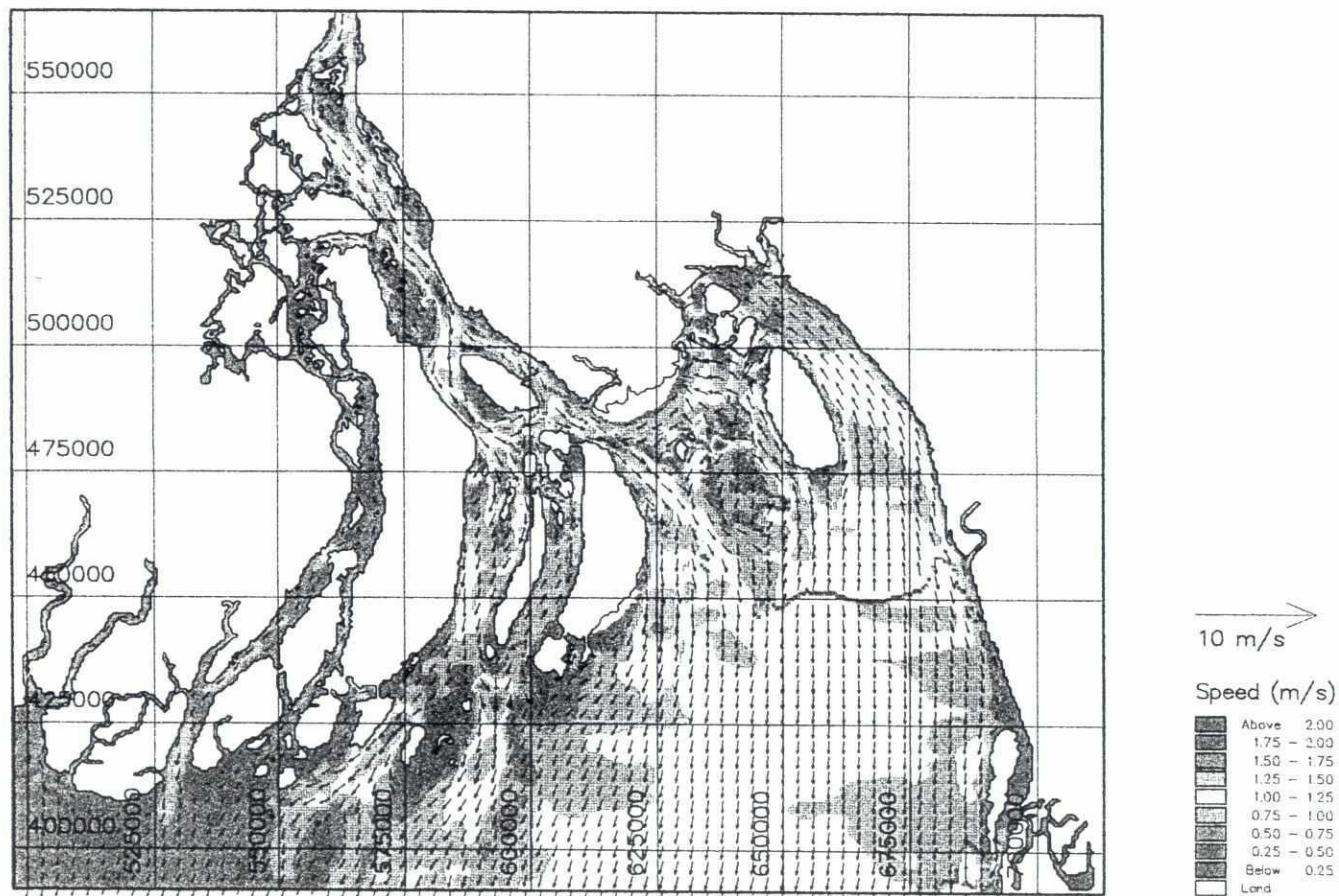
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File:	Date: Mon Jun 8 1998	Max velocities for Neap Tide, Dry Season 1996 Intervention Schemes 1 and 3		Drawing no. 6.7
Scale: 1:1500000	Int: p5011			

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WCTUPN 9654



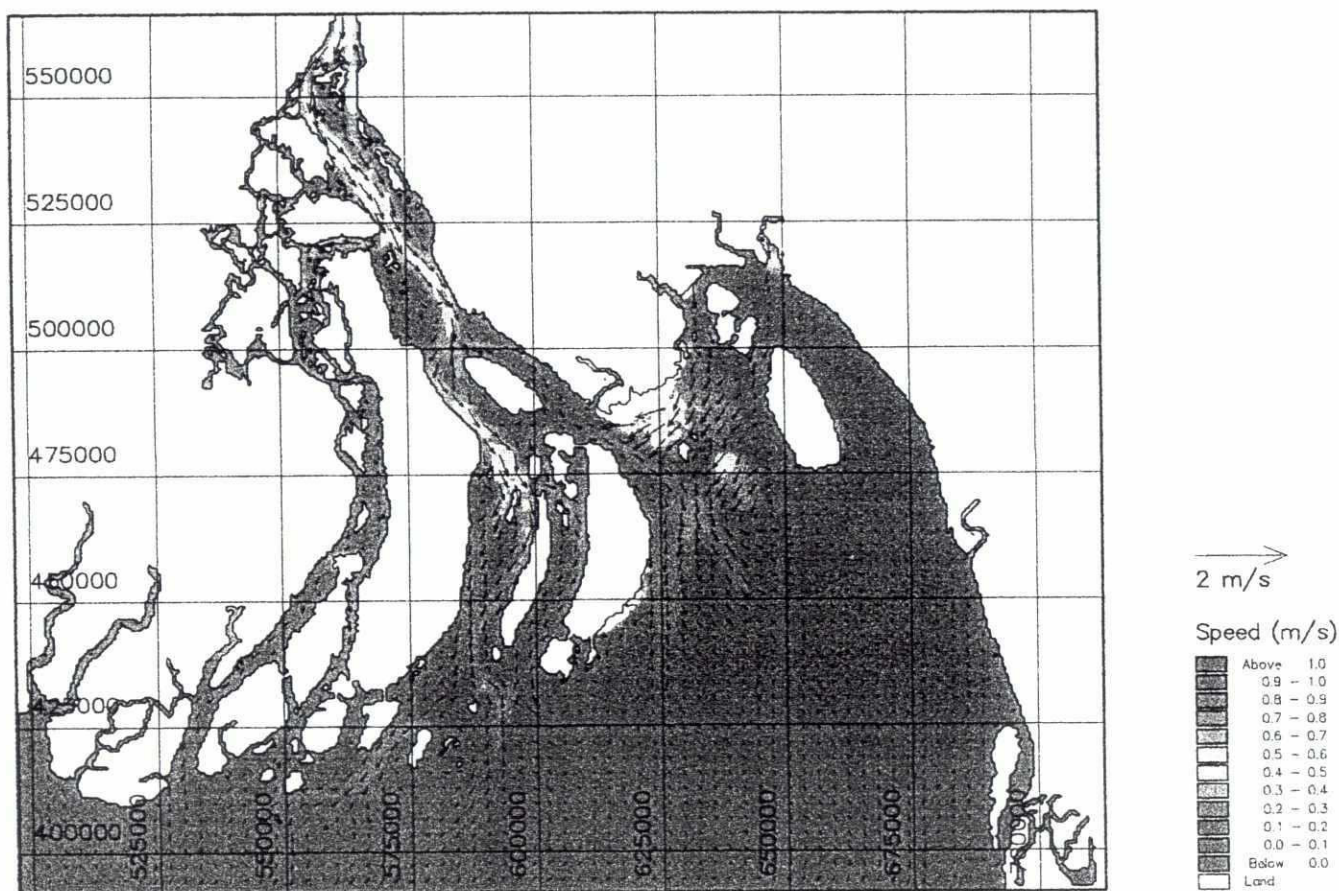
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Scale: 1:1500000	Init: p5011			6.8



SWMC		Client:	Bangladesh Water Development Board	MIKE 21
		Project:	Meghna Estuary Study	
File:	Date: Mon Jun 8 1998	Max velocities for Neap Tide, Dry Season 1996 All intervention Schemes, excl. 8		Drawing no.
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260

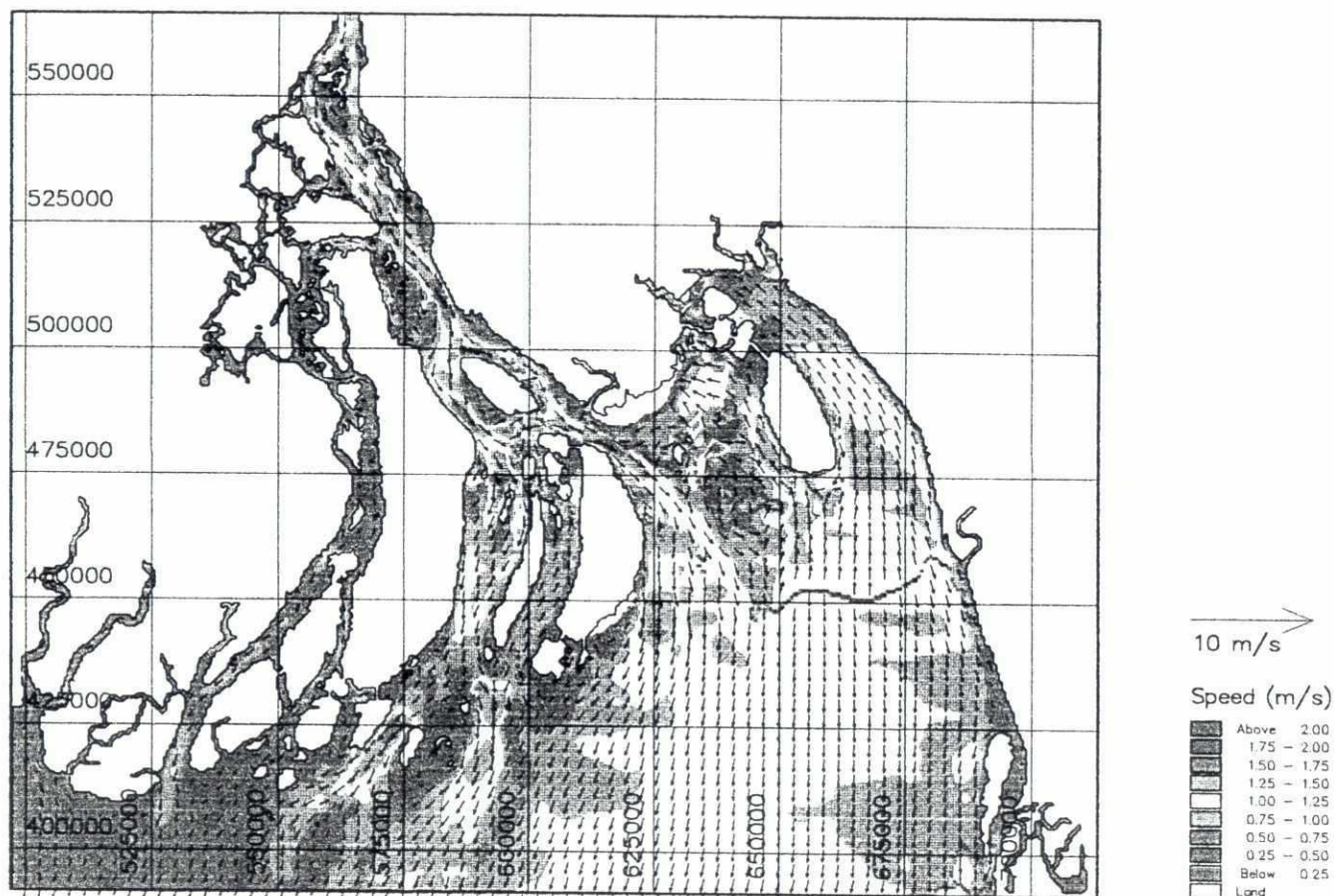
1998/06/08 09:54



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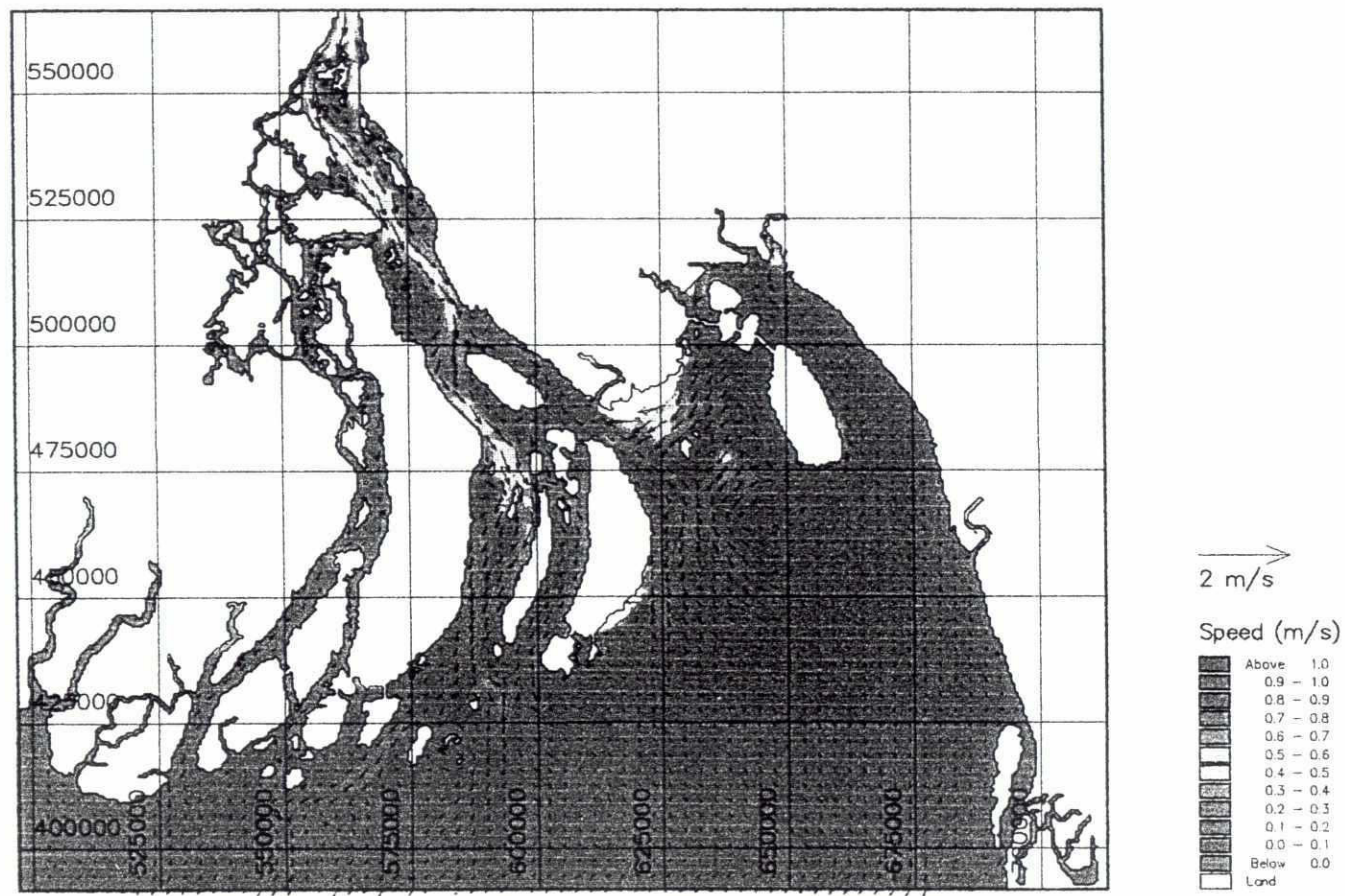
13/06/1998



SWMC		Client:	Bangladesh Water Development Board		MIKE 21	
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File:	Date: Mon Jun 8 1998	Max velocities for Neap Tide, Dry Season 1996 All intervention Schemes				Drawing no.
Scale: 1:1500000	Init: p5011					6.11

202

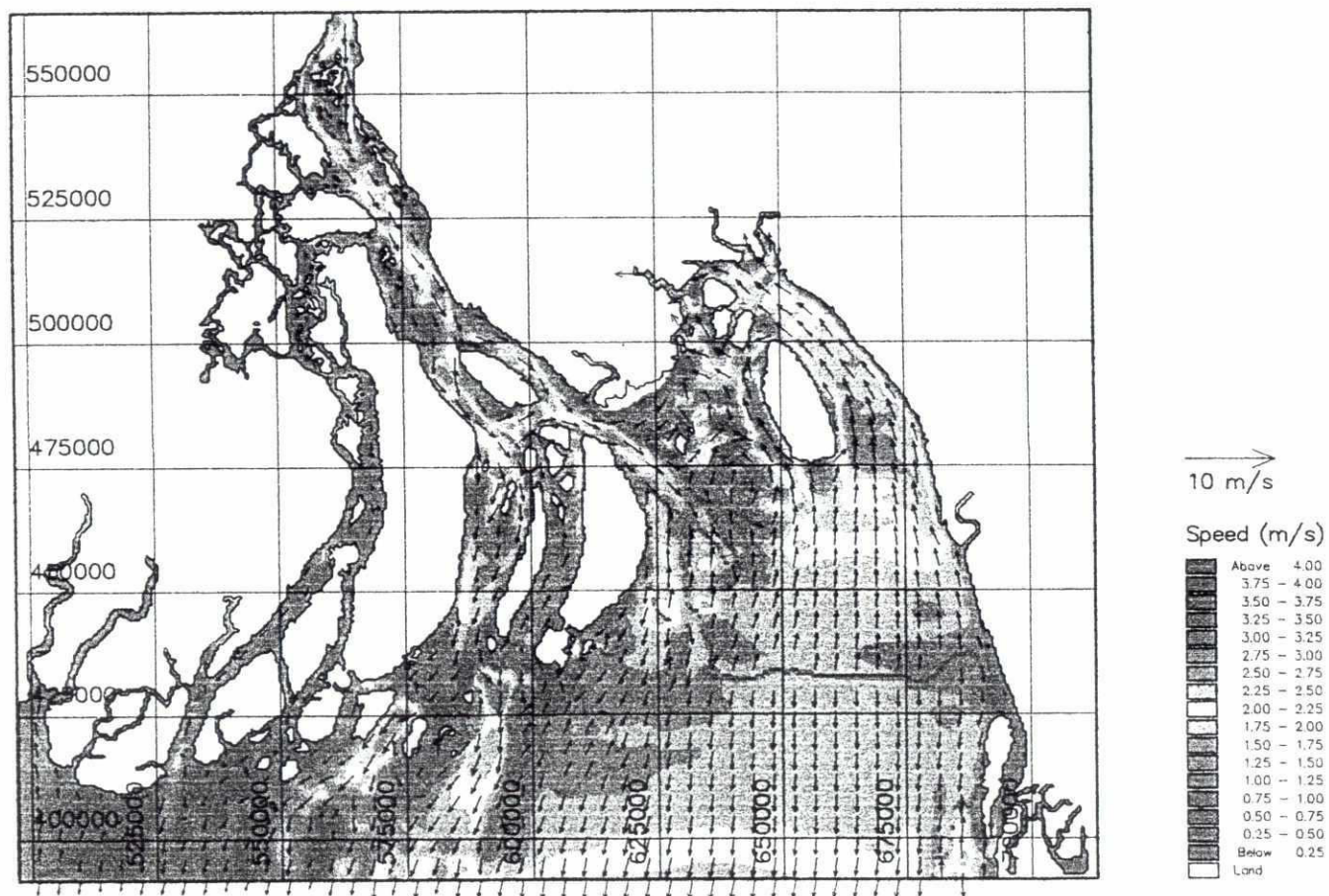
WAPDA 96/4



SWMC		Client:	Bangladesh Water Development Board		MIKE 21
		Project:	Meghna Estuary Study		
File:	Date: Mon Jun 8 1998	Net flow for Neap Tide, Dry Season 1996 All intervention Schemes			Drawing no.
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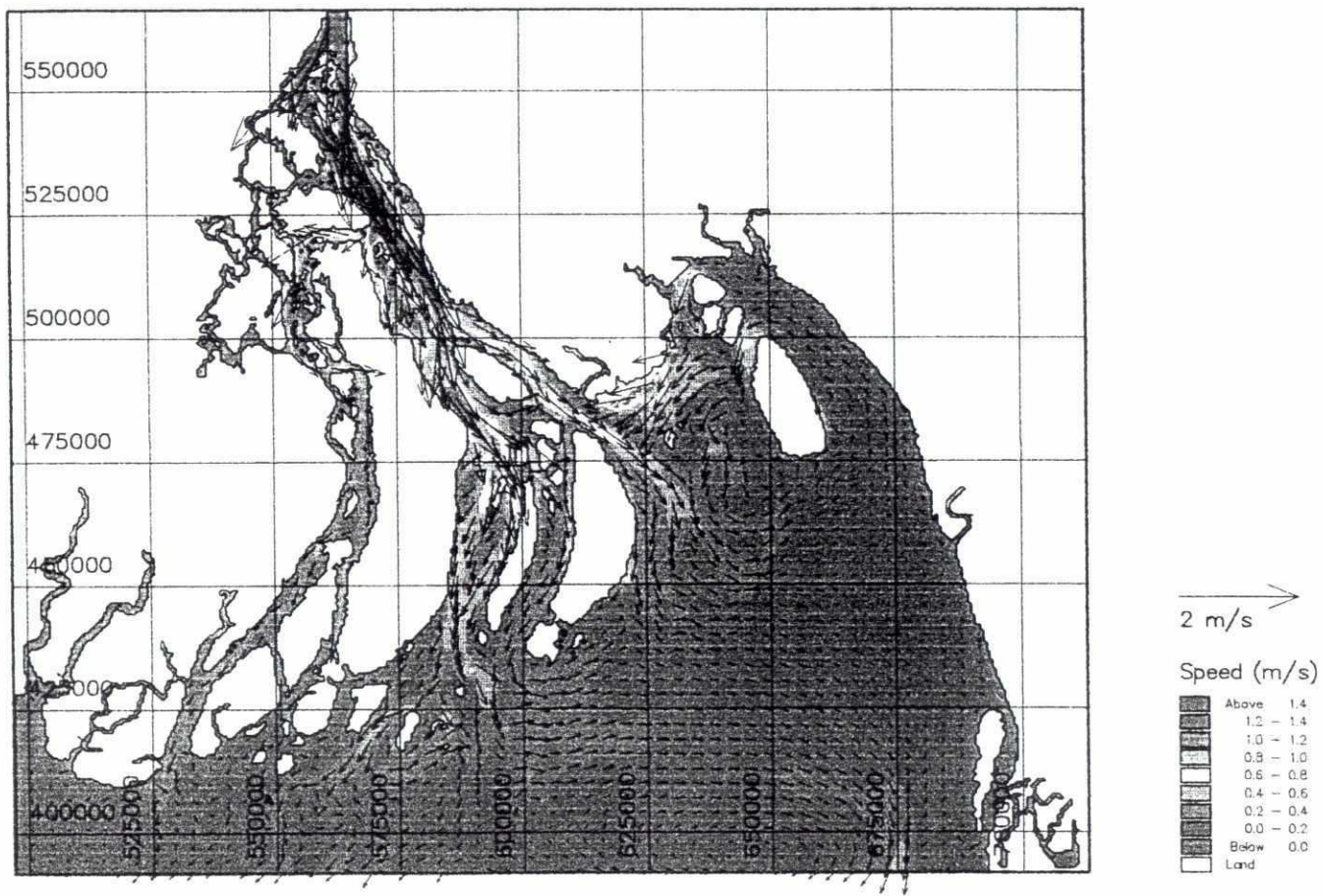
WGS 1984 / UTM



SWMC		Client:	Bangladesh Water Development Board	MIKE 21
		Project:	Meghna Estuary Study	
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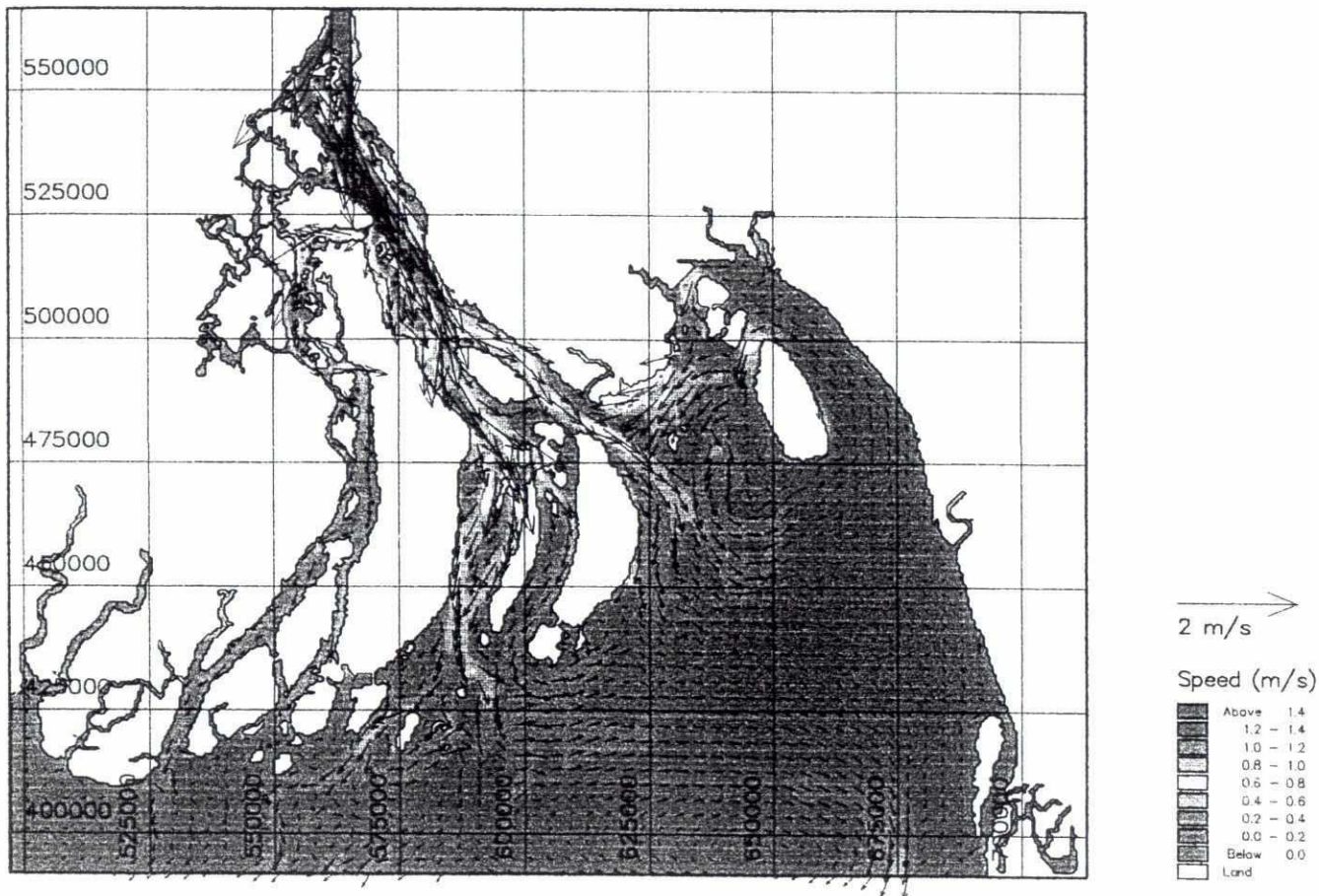
208

5/27/97 11:35a



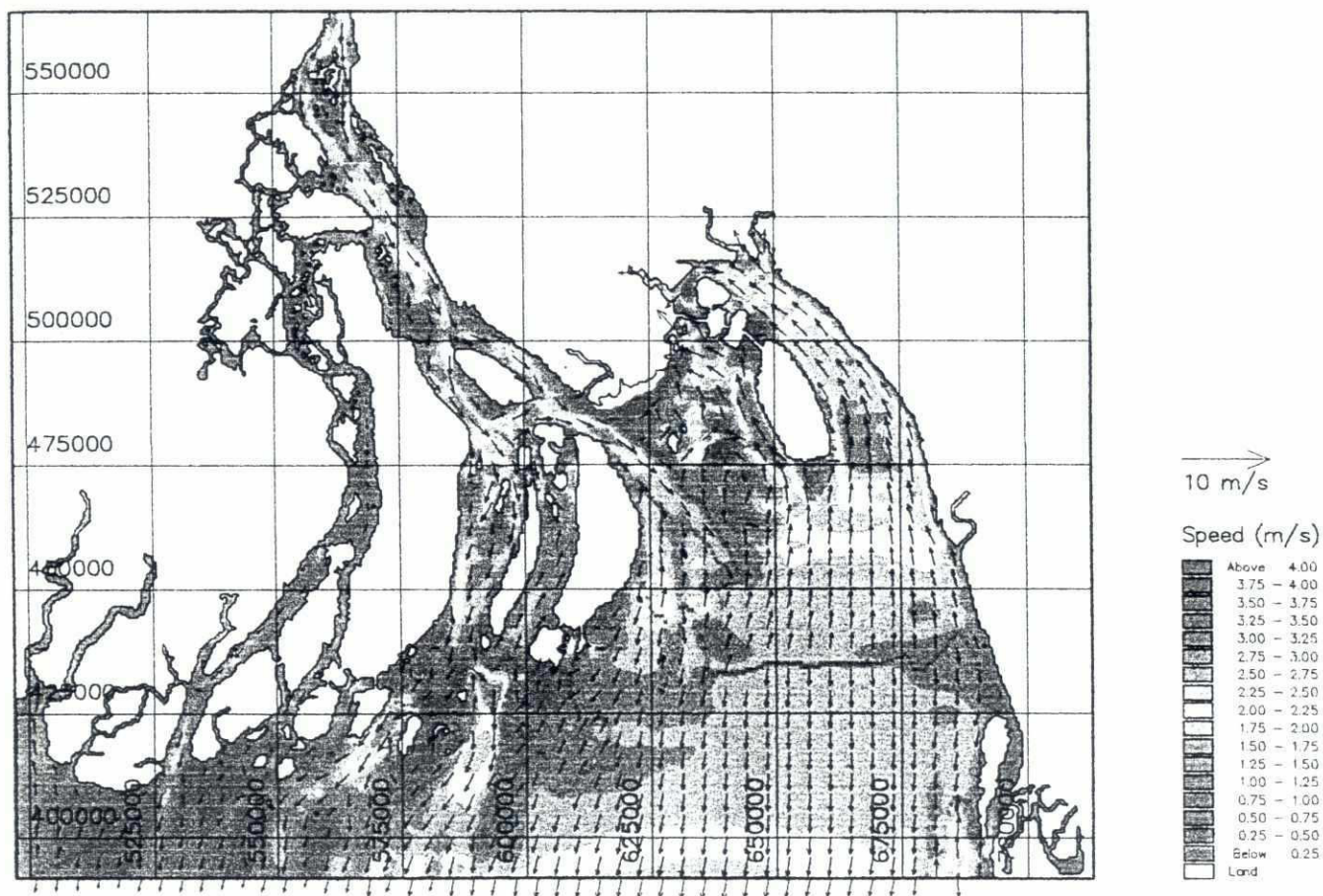
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Scale: 1:1500000	Int: p5011			

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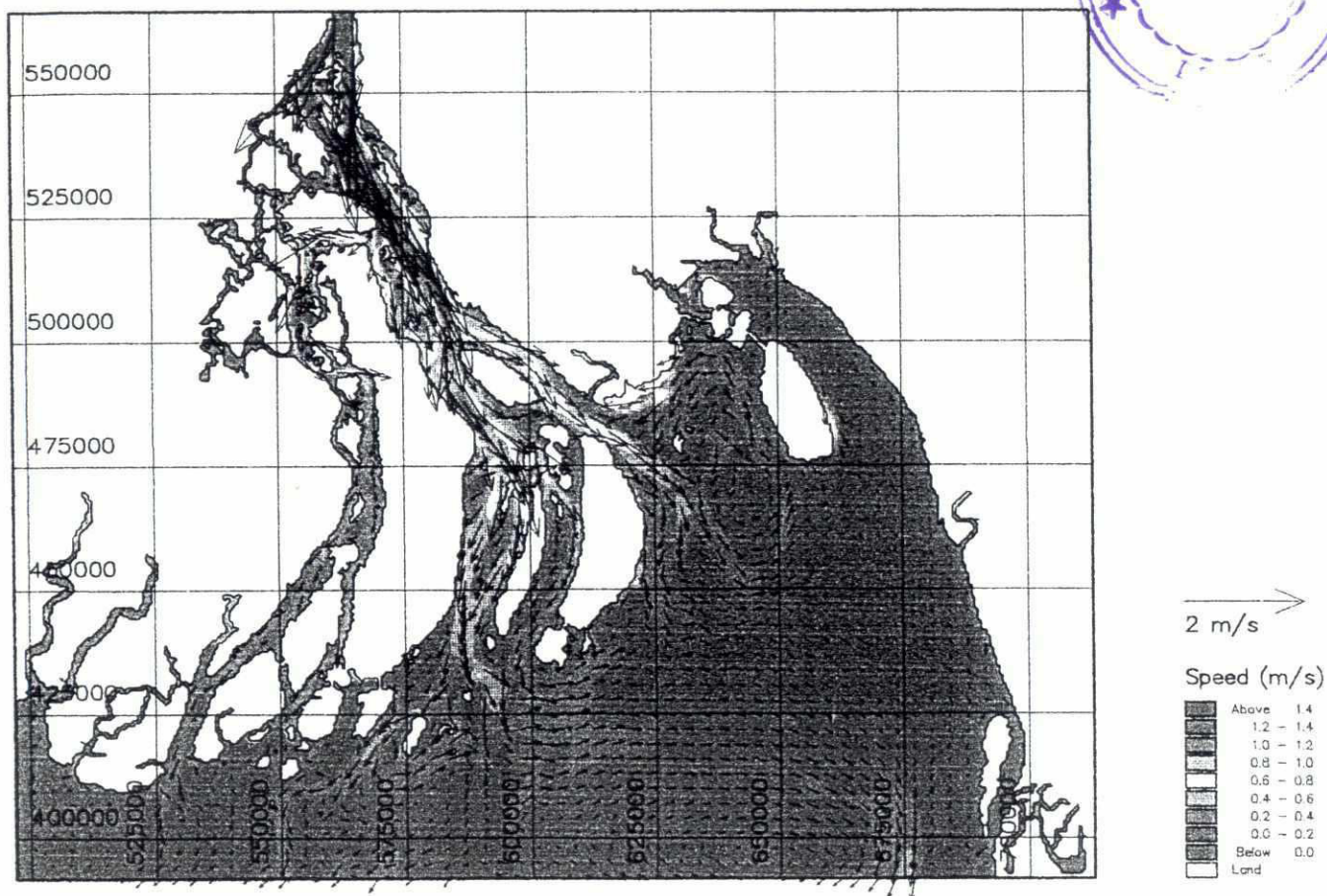
269



SWMC		Client:	Bangladesh Water Development Board		MIKE 21
		Project:	Meghna Estuary Study		
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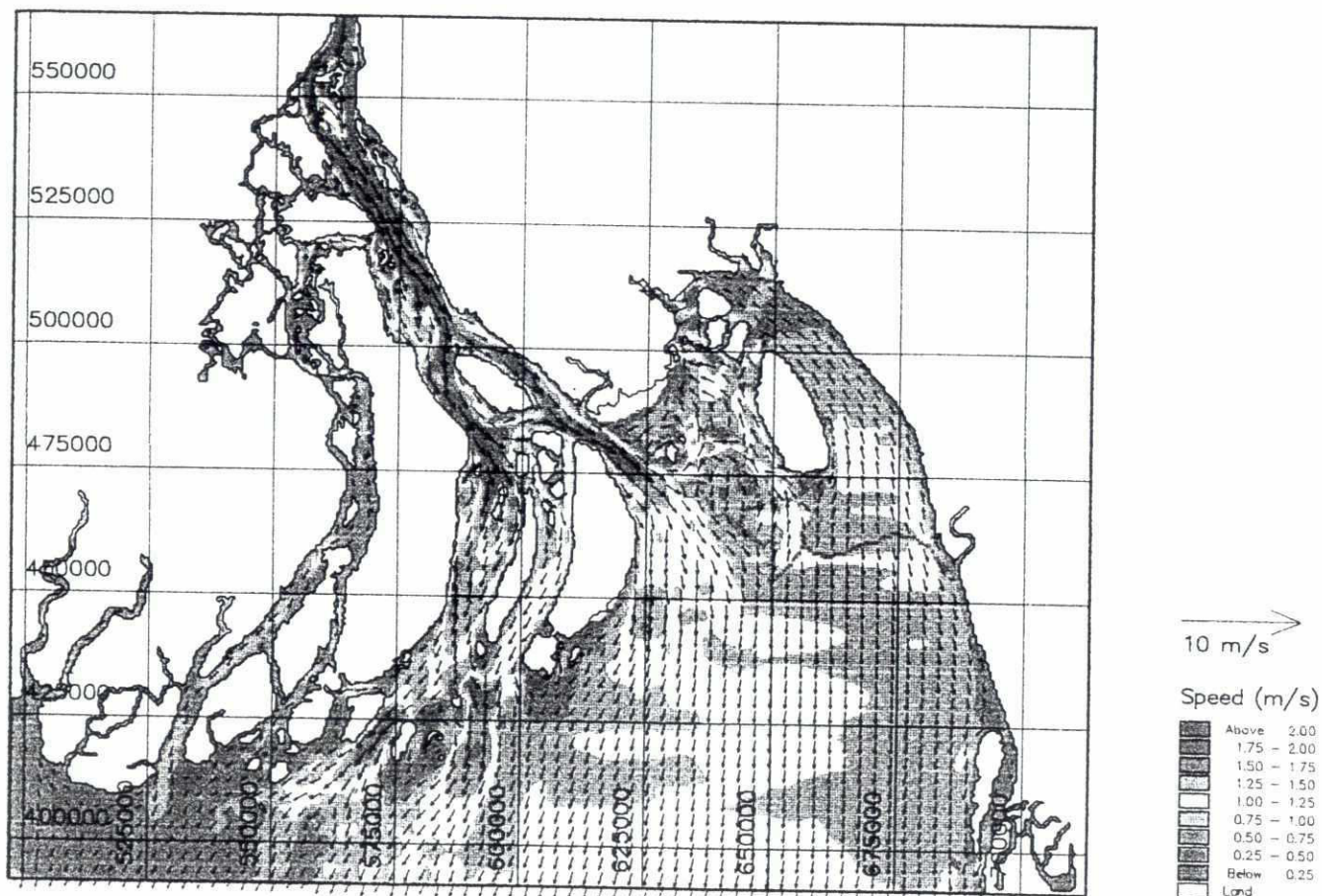
261

6/27/1998

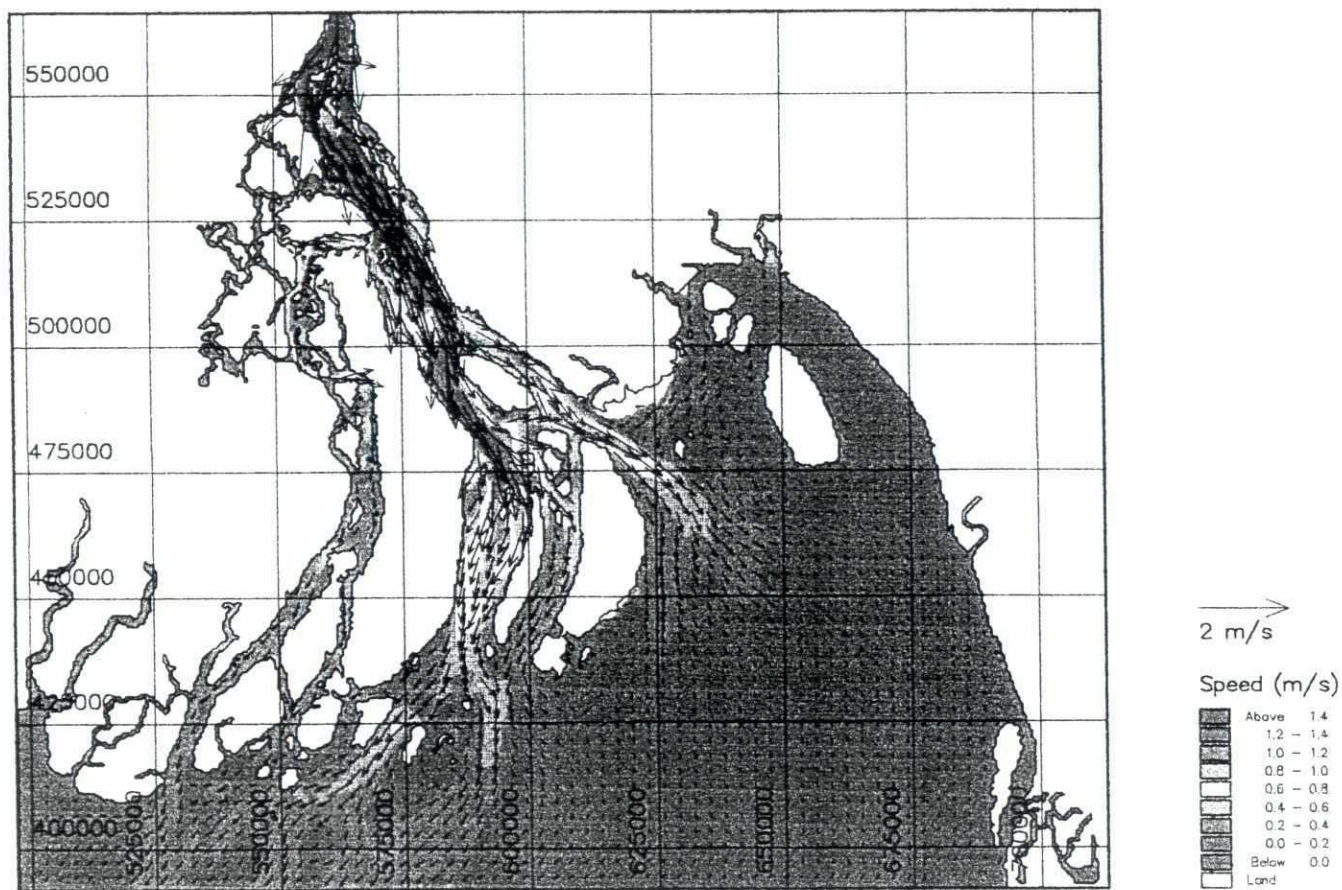


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		Project:	Meghna Estuary Study	
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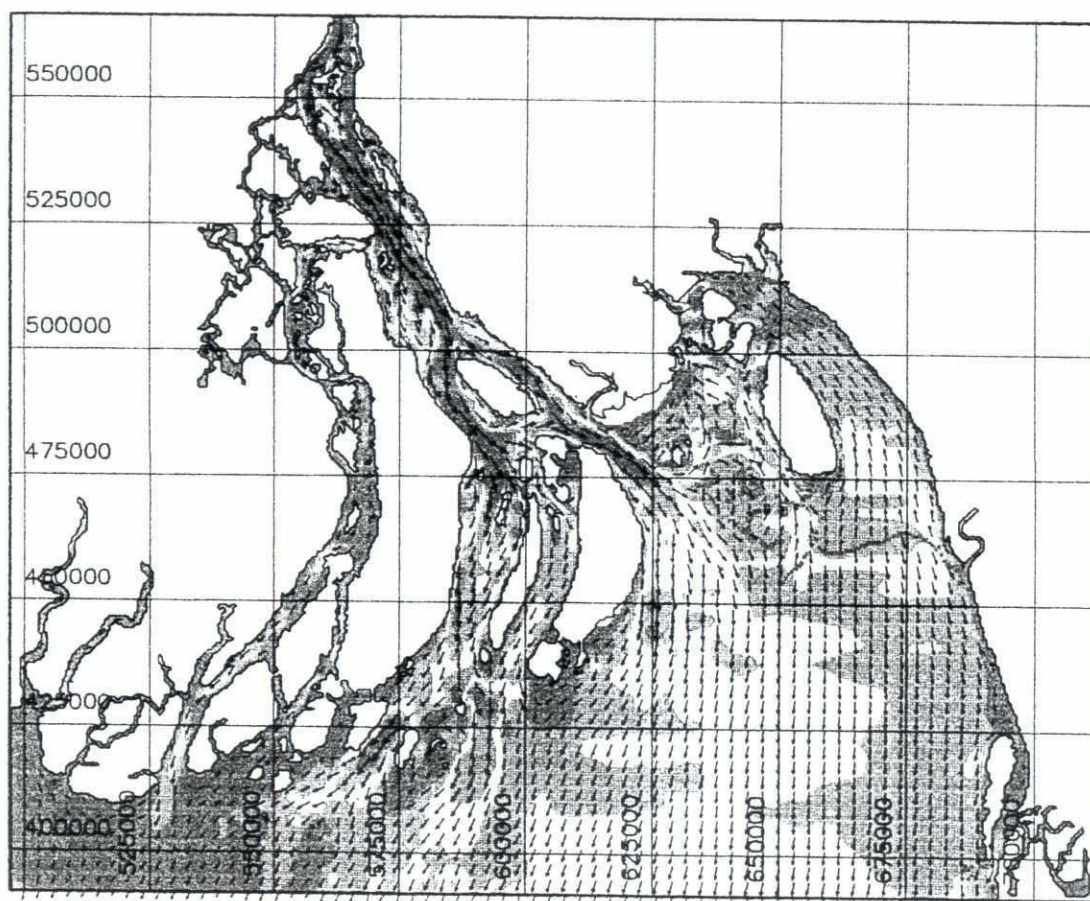
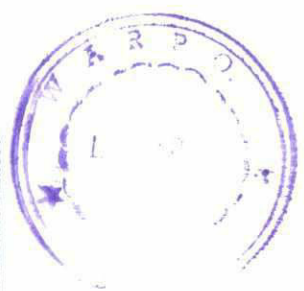
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		Project:	Meghna Estuary Study	
File:	Date: Mon Jun 8 1998	Max velocities for Neap Tide, Monsoon Season 1997 Intervention Schemes 1 and 3		Drawing no. 6.19
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SWMC		Client:	Bangladesh Water Development Board	MIKE 21
		Project:	Meghna Estuary Study	
File:	Date: Mon Jun 8 1998	Net flow for Neap Tide, Monsoon Season 1997 Intervention Schemes 1 and 3		Drawing no. 6.20
Scale: 1:1500000	Init: p5011			

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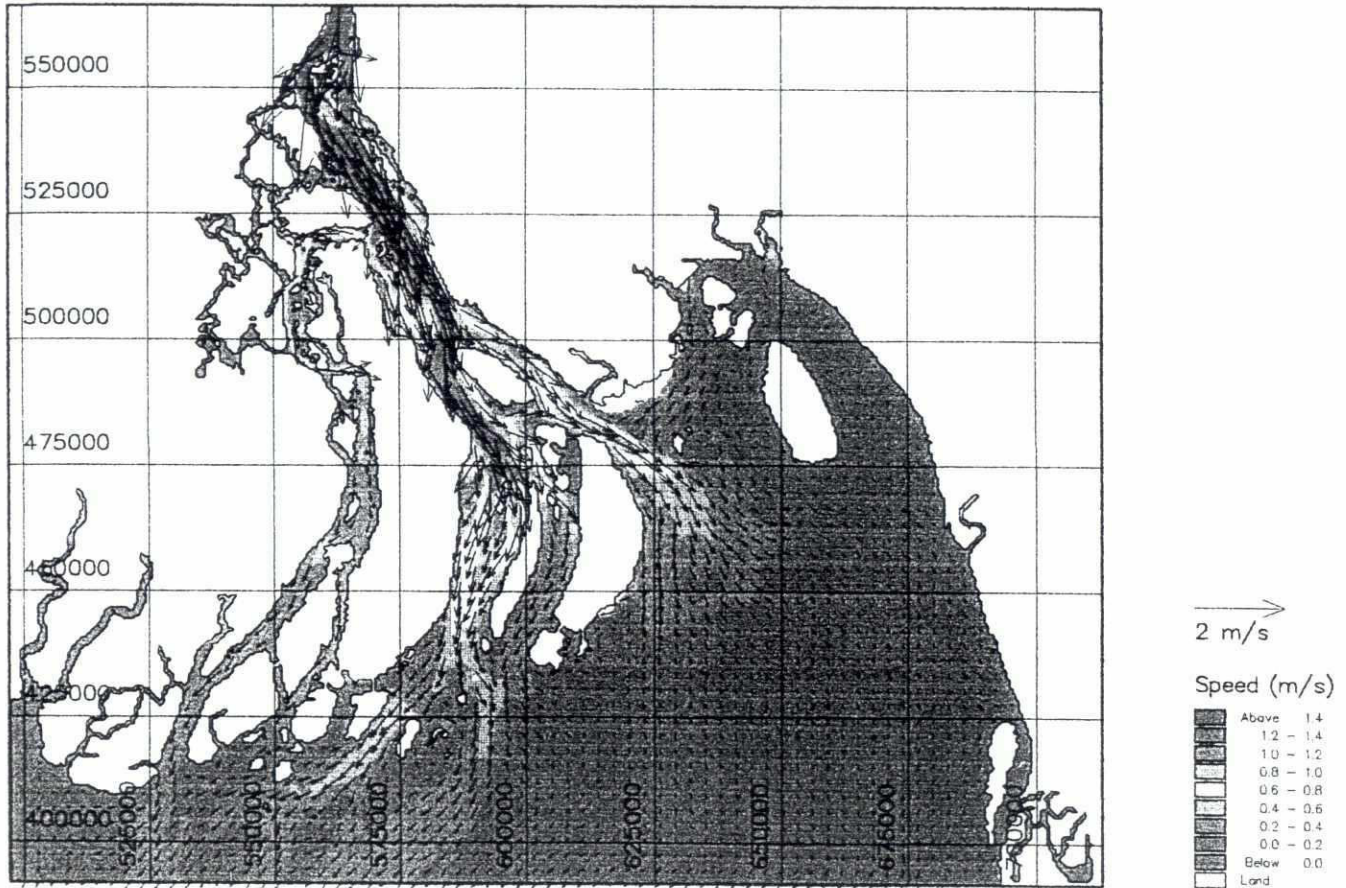


10 m/s

Speed (m/s)

- Above 2.00
- 1.75 - 2.00
- 1.50 - 1.75
- 1.25 - 1.50
- 1.00 - 1.25
- 0.75 - 1.00
- 0.50 - 0.75
- 0.25 - 0.50
- Below 0.25
- Land

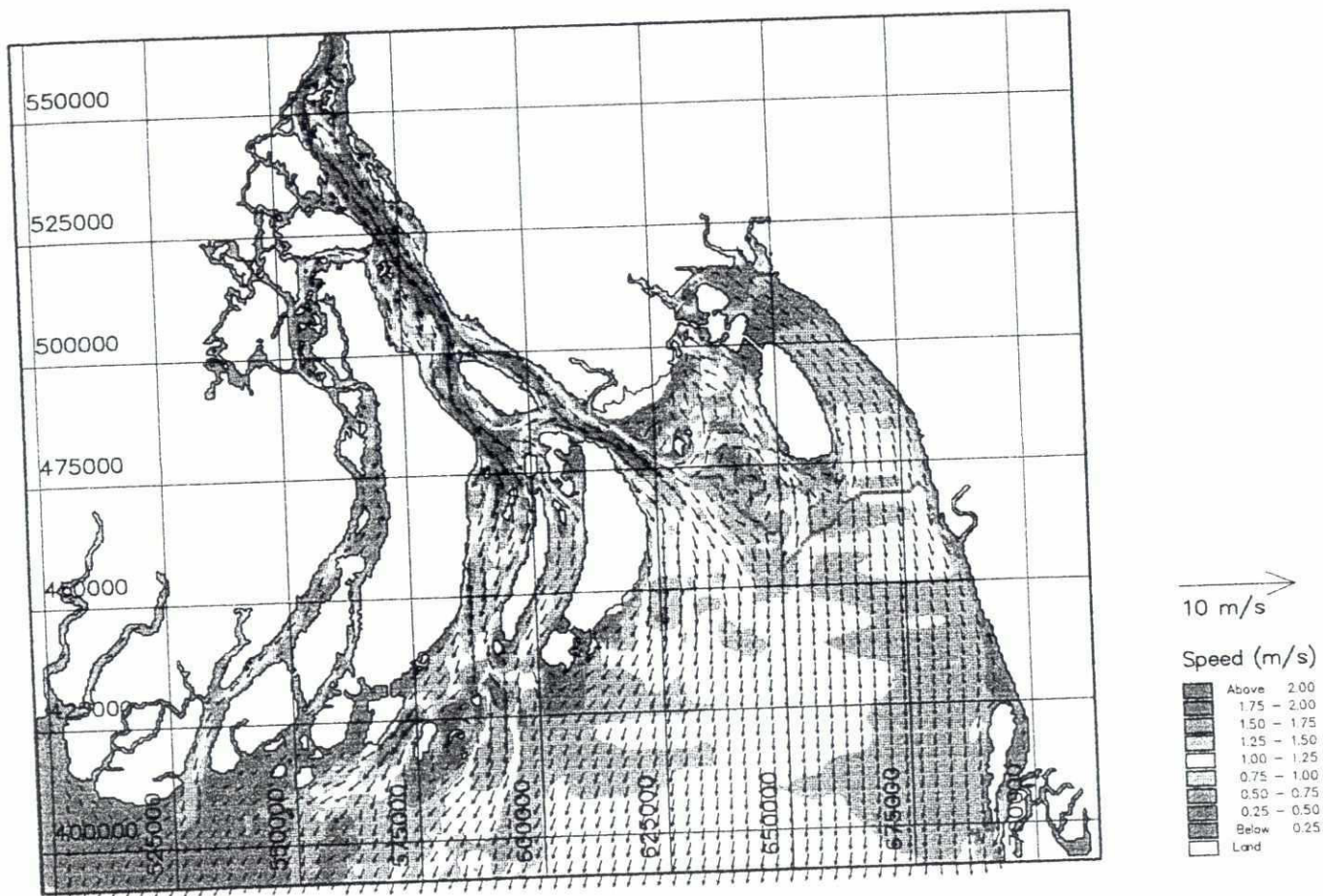
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Scale: 1:1500000	Int: p5011			



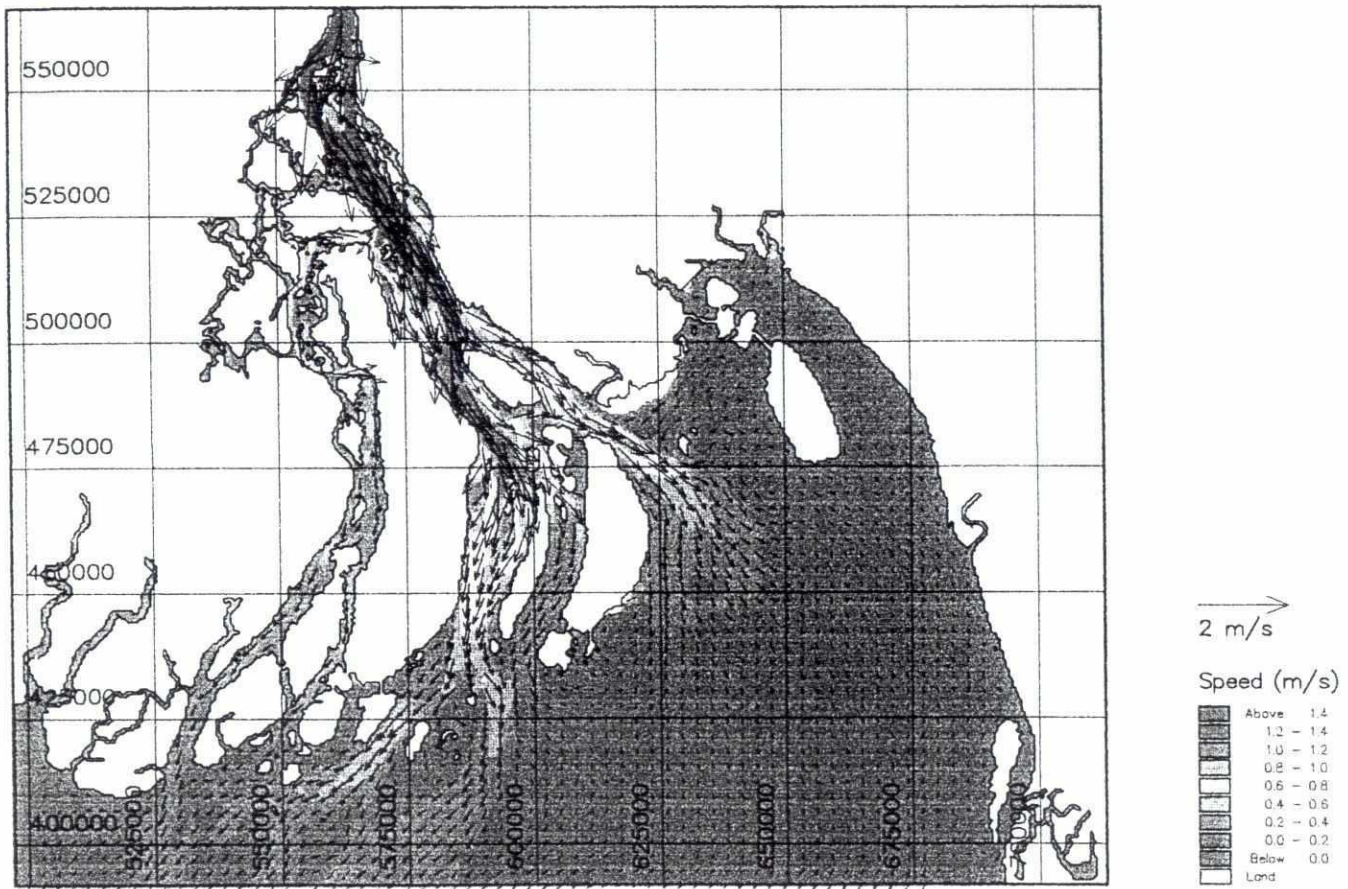
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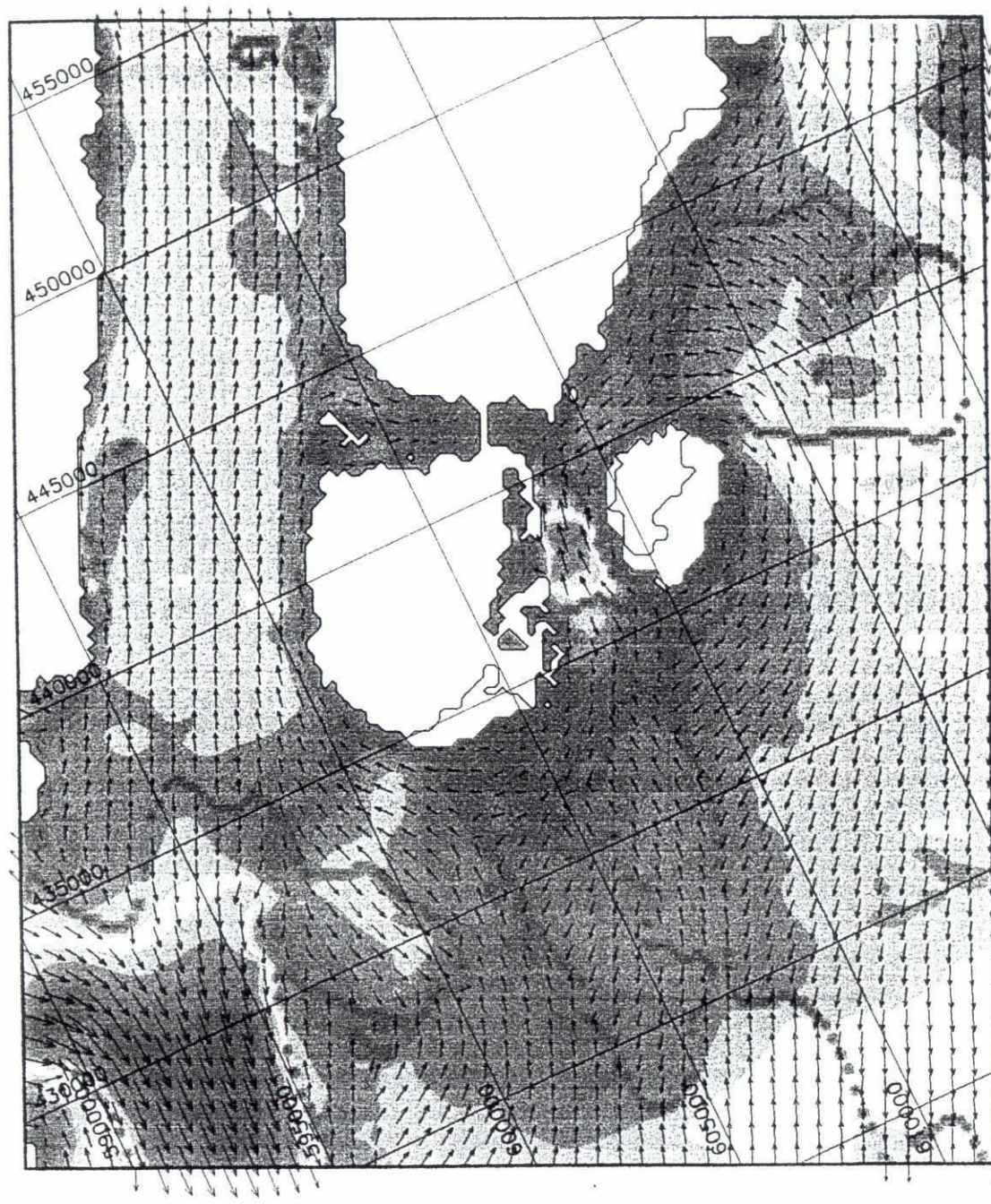
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File:	Date: Mon Jun 8 1998	Max velocities for Neap Tide, Monsoon Season 1997 All intervention Schemes		Drawing no.	
Scale: 1:1500000	Int: p5011			6.23	



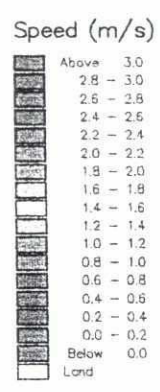
SWMC		Client:	Bangladesh Water Development Board	MIKE 21
		Project:	Meghna Estuary Study	
File:	Date: Mon Jun 8 1998	Net flow for Neap Tide, Monsoon Season 1997 All intervention Schemes		Drawing no.
Scale: 1:1500000	Init: p5011			6.24

288

DATE: 11/11/1998

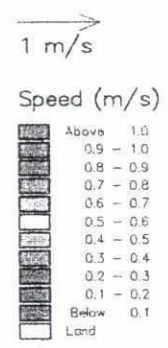
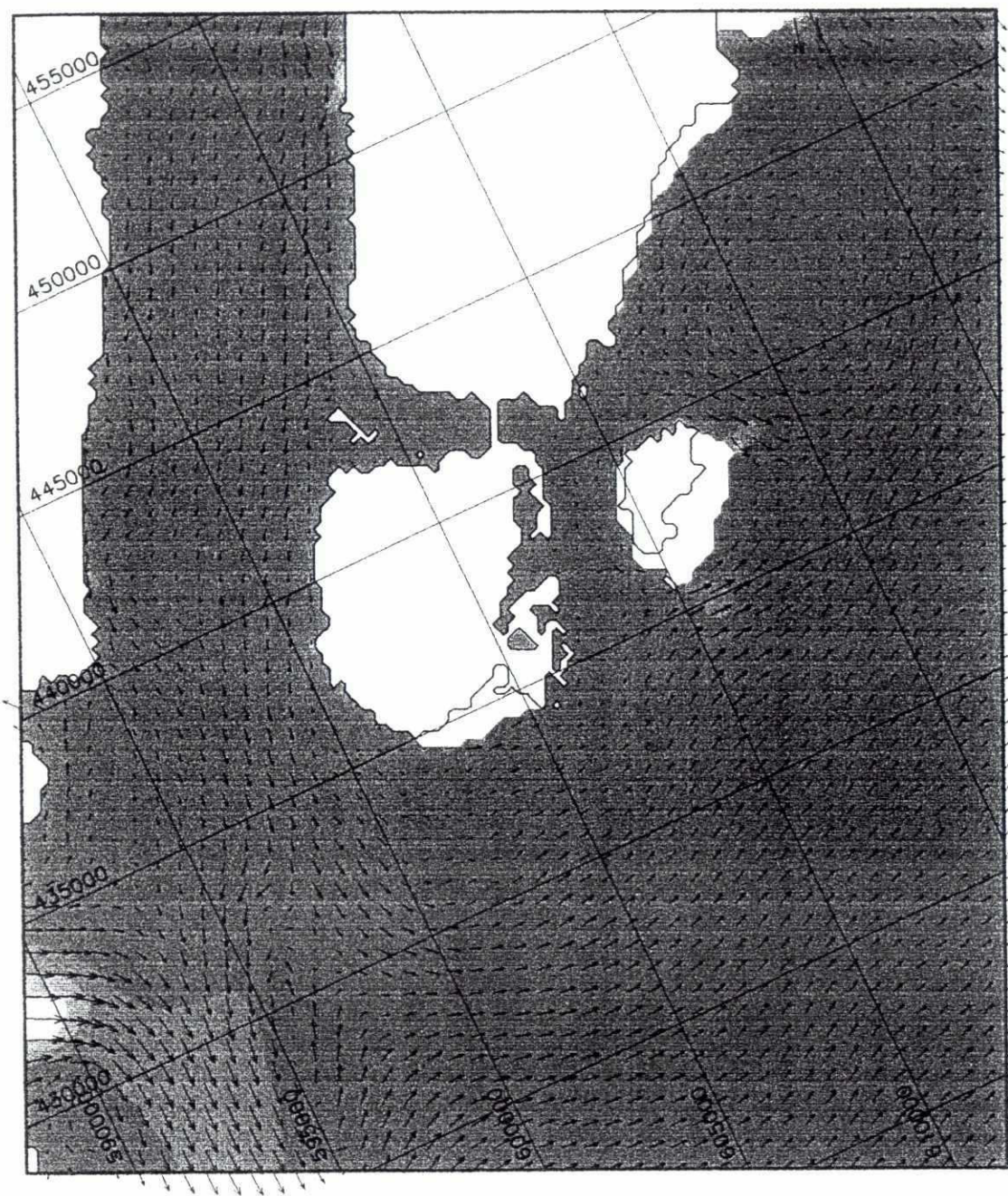


5 m/s



<div>SWMC</div>		Client:	Bangladesh Water Development Board	MIKE 21
		Project:	Meghna Estuary Study	
File:	Date: Mon Jun 8 1998	Max velocities for Spring Tide, Dry Season 1996 Intervention Schemes 1 and 3		Drawing no. 6.25
Scale: 1:185000	Int: p5011			

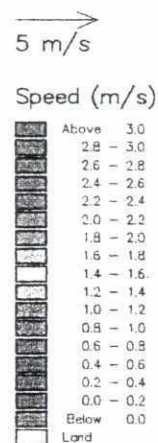
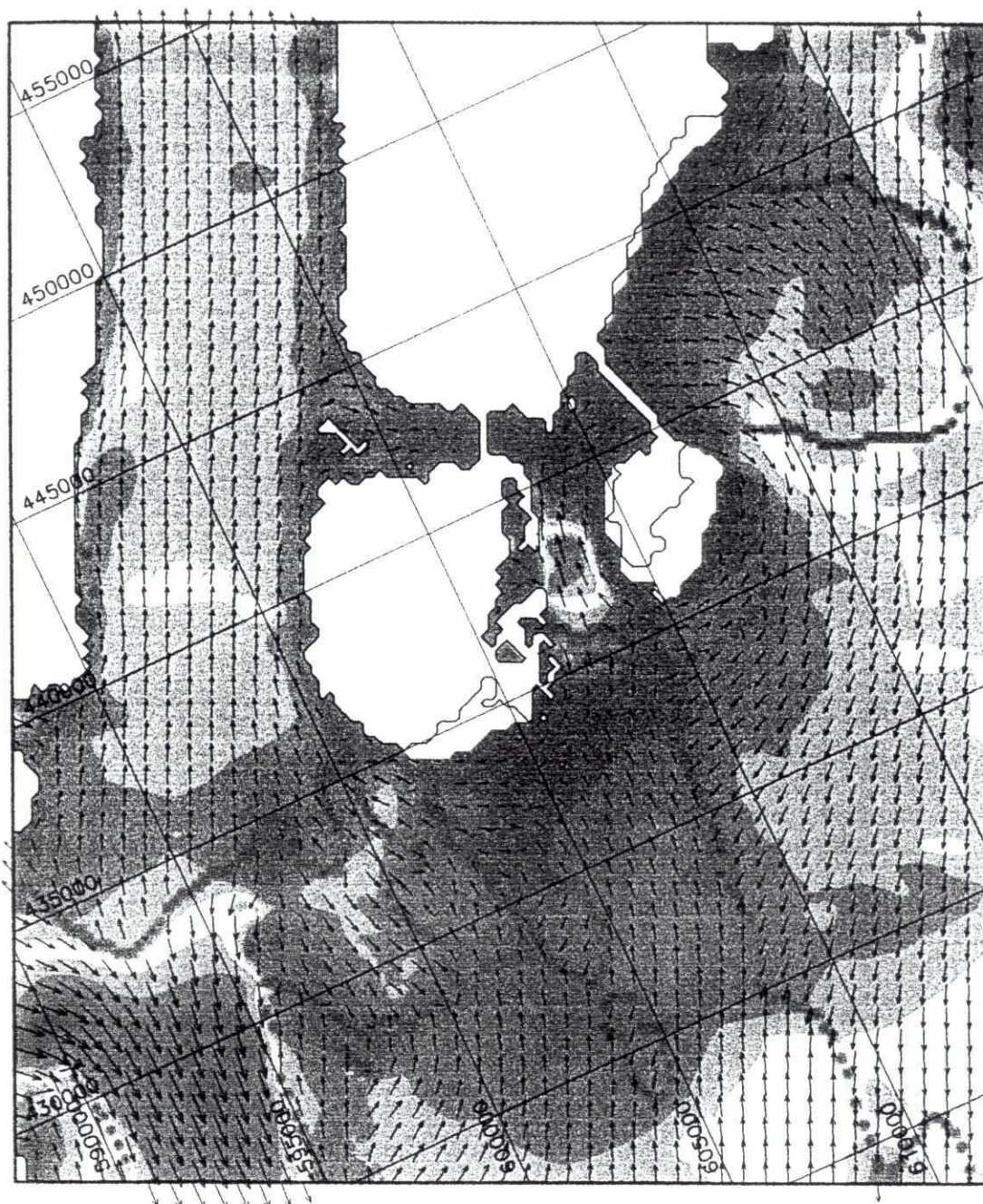
287



SWMC		Client:	Bangladesh Water Development Board	MIKE 21
		Project:	Meghna Estuary Study	
File:	Date: Mon Jun 8 1998	Net flow for Spring Tide, Dry Season 1996 Intervention Schemes 1 and 3		Drawing no.
Scale: 1:185000	Init: p5011			6.26

289

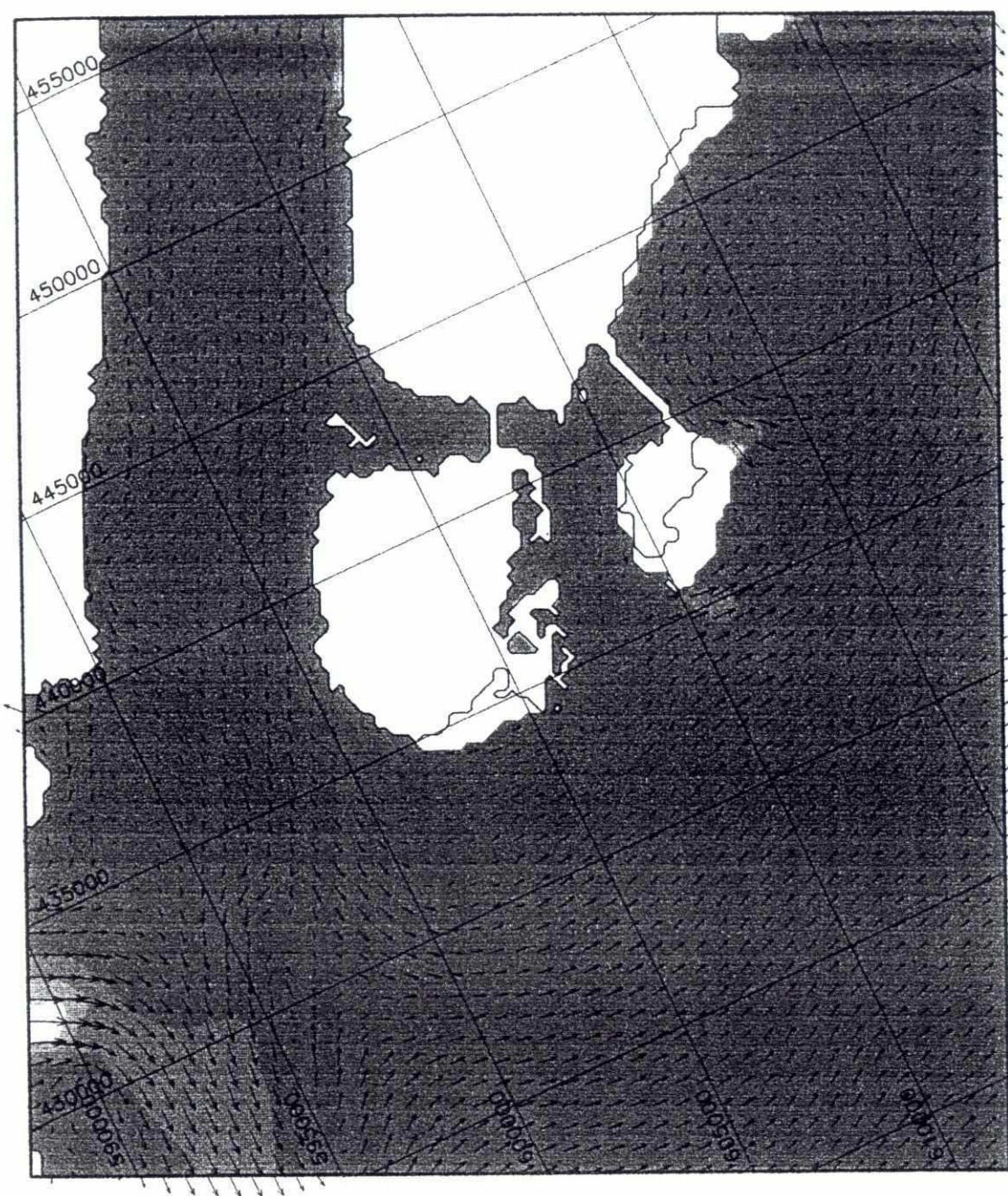
01/06/1998



SWMC		Client:	Bangladesh Water Development Board	MIKE 21
		Project:	Meghna Estuary Study	
File:	Date: Mon Jun 8 1998	Max velocities for Spring Tide, Dry Season 1996 All interventions Schemes		Drawing no. 6.27
Scale: 1:185000	Int: p5011			

28f

05/06/98 10:30



1 m/s

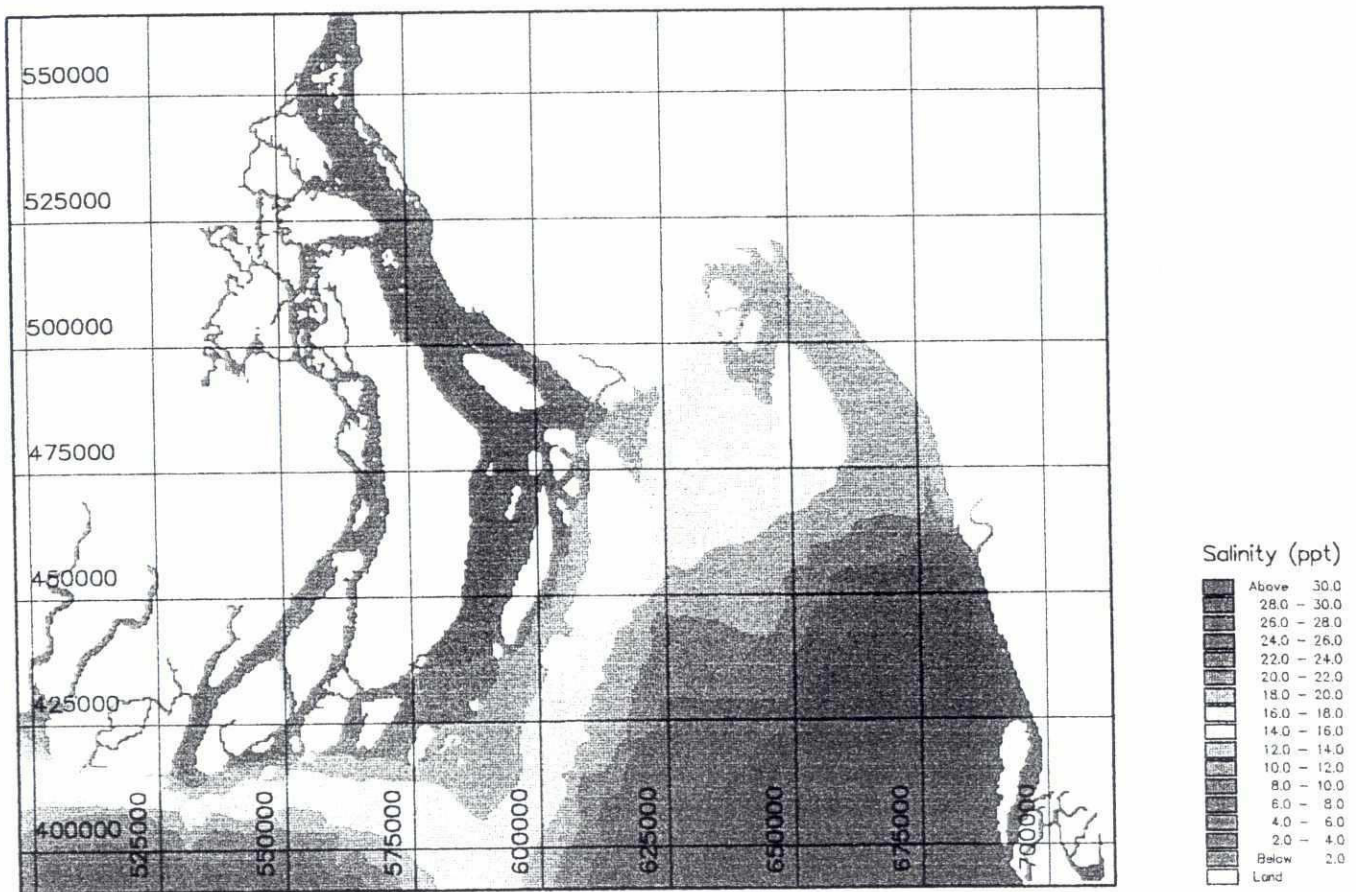
Speed (m/s)

- Above 1.0
- 0.9 - 1.0
- 0.8 - 0.9
- 0.7 - 0.8
- 0.6 - 0.7
- 0.5 - 0.6
- 0.4 - 0.5
- 0.3 - 0.4
- 0.2 - 0.3
- 0.1 - 0.2
- Below 0.1
- Land

<div>SWMC</div>		Client:	Bangladesh Water Development Board	MIKE 21
		Project:	Meghna Estuary Study	
File:	Date: Mon Jun 8 1998	Net flow for Spring Tide, Dry Season 1996 All interventions Schemes		Drawing no.
Scale: 1:185000	Init: p5011			6.28

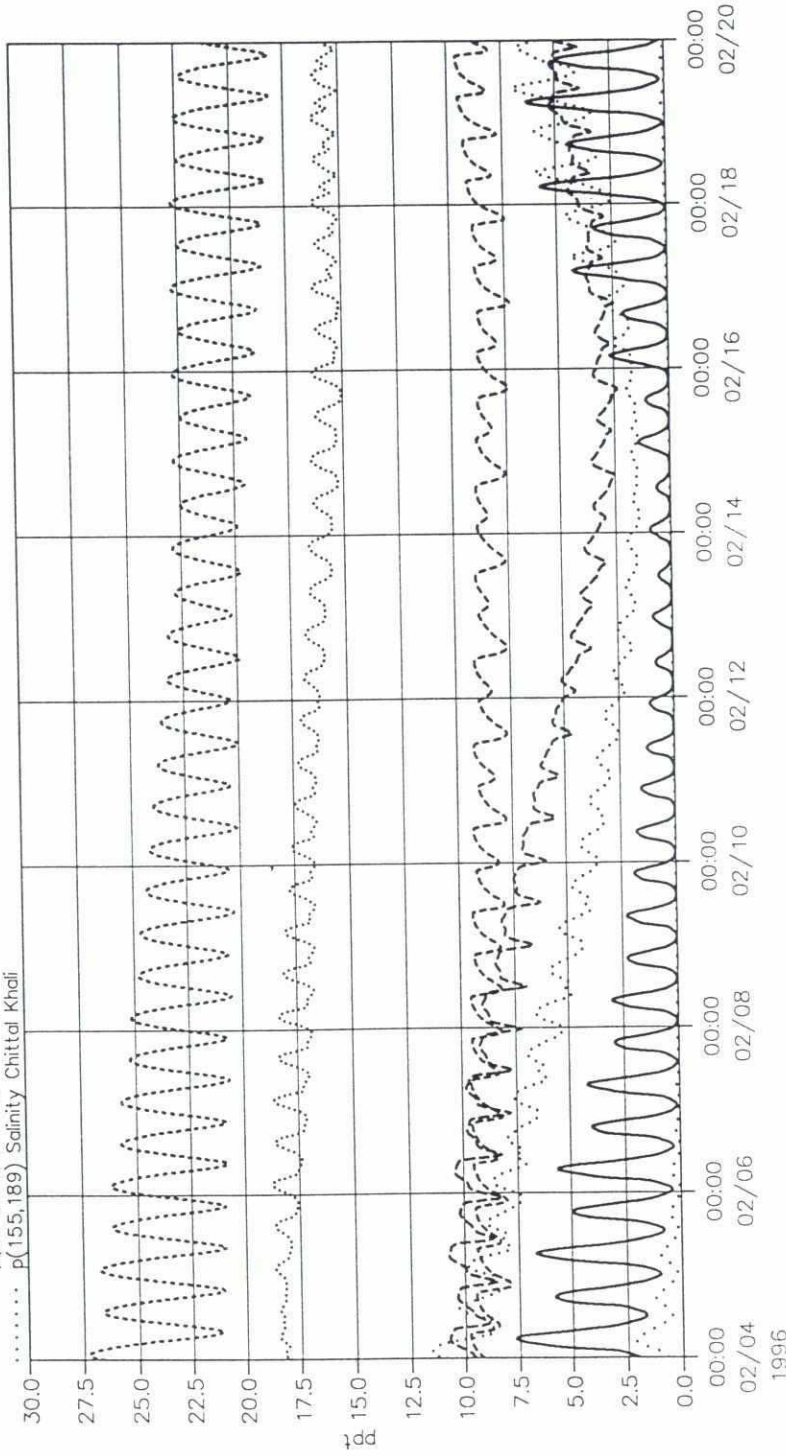
282

Figure 12



<div>SWMC</div>		Client:	Bangladesh Water Development Board	MIKE 21
		Project:	Meghna Estuary Study	
File:	Date: Mon Jun 8 1998	LRP salinity data 0.5 m below surface 1986/03/21 - 1986/03/28		Drawing no.
Scale: 1:1500000	Init: p5011			7.1

- p(121,66) Salinity Kochapia
- p(43,39) Salinity Hatia Bar
- p(43,39) Salinity Normans Point
- p(43,39) Salinity Dhulasar
- p(188,111) Salinity Char Chenga
- p(254,150) Salinity Sandwip
- p(155,189) Salinity Chittal Khali



SWMC		Client: Bangladesh Water Development Board		MIKE 21
		Project: Meghna Estuary Study		
File:	Date: Mon Jun 8 1998	Salinity, Dry season 1996		Drawing no. 7.2
Scale:	Init: p5011			

285

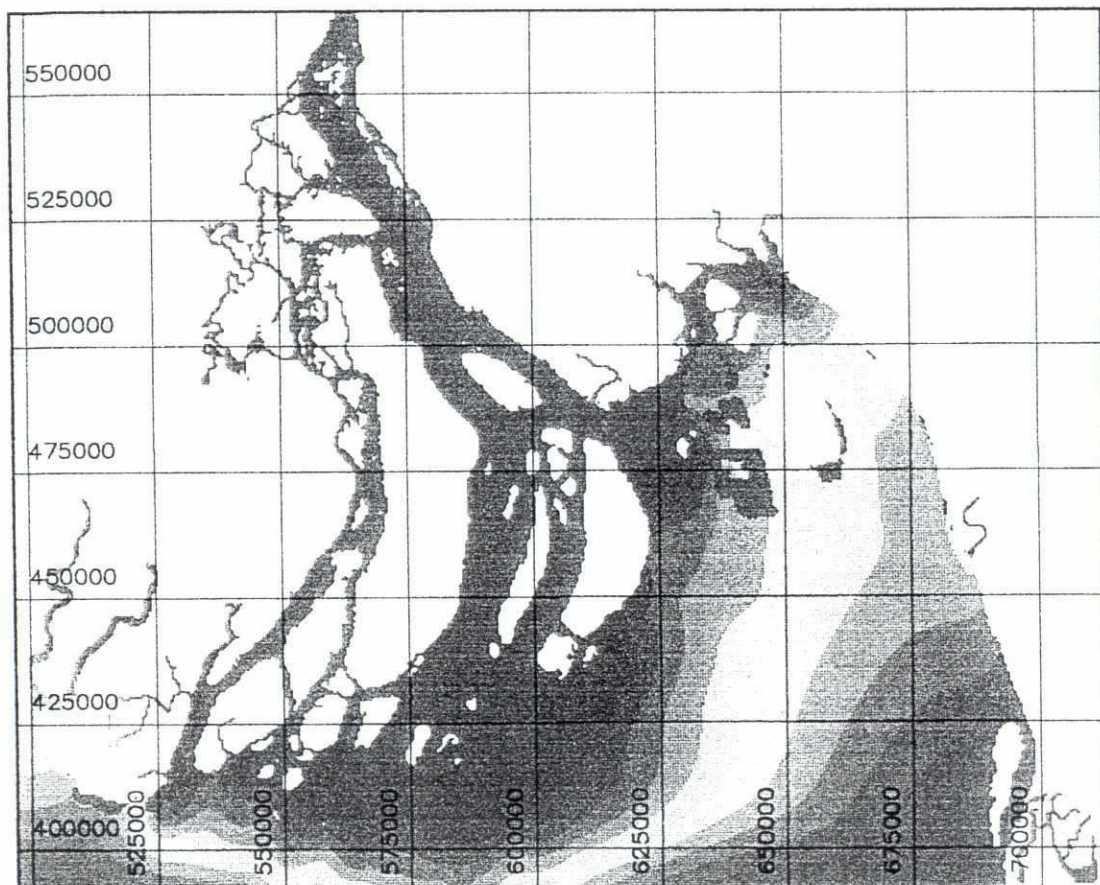
03-04-93 11:04 AM



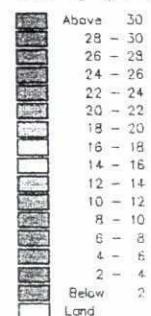
SWMC		Client:	Bangladesh Water Development Board	MIKE 21
		Project:	Meghna Estuary Study	
File:	Date: Mon Jun 8 1998	Difference in mean elevations incl - excl the effect of salinity		Drawing no. 7.3
Scale: 1:1500000	init: p5011			

202

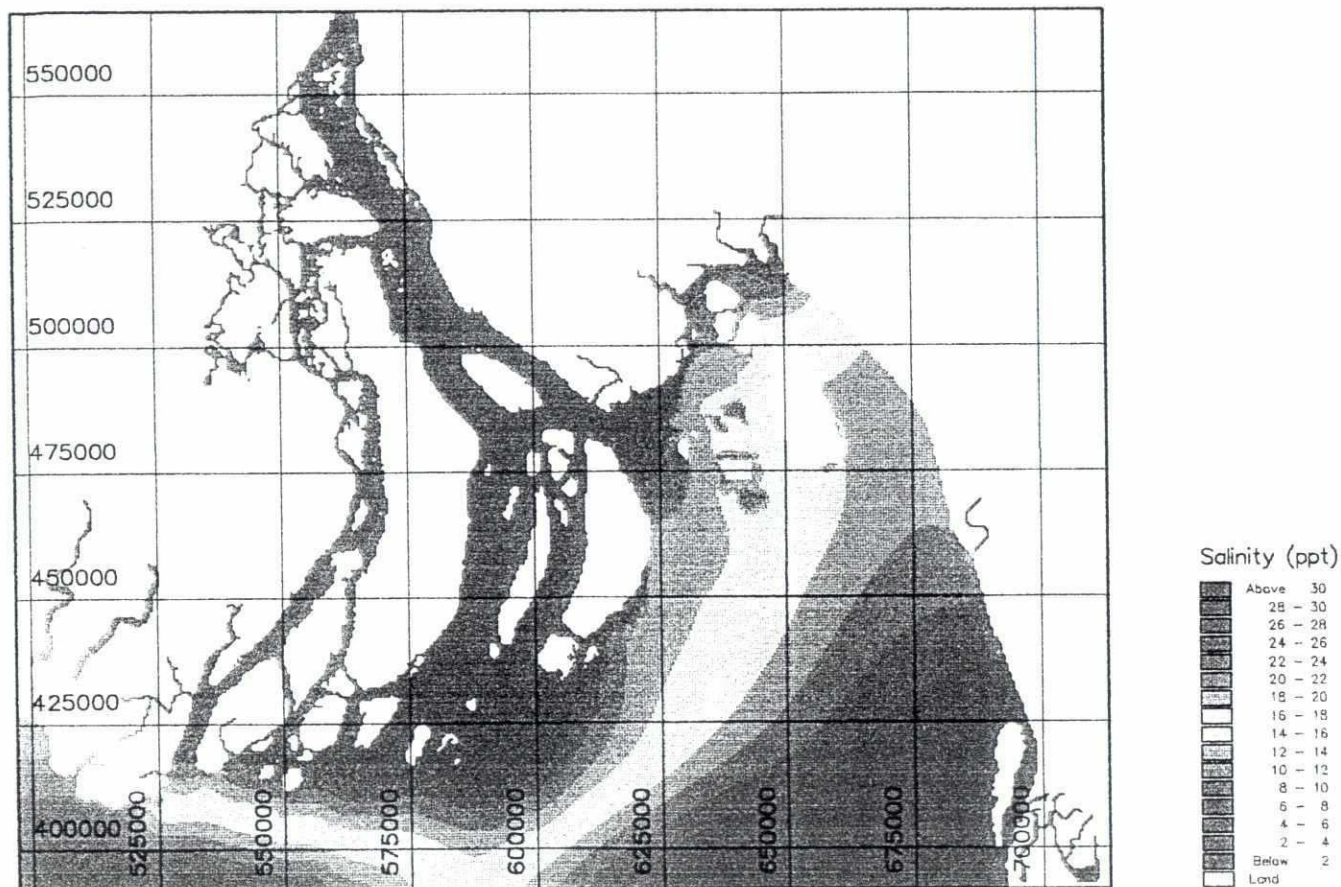
unro p



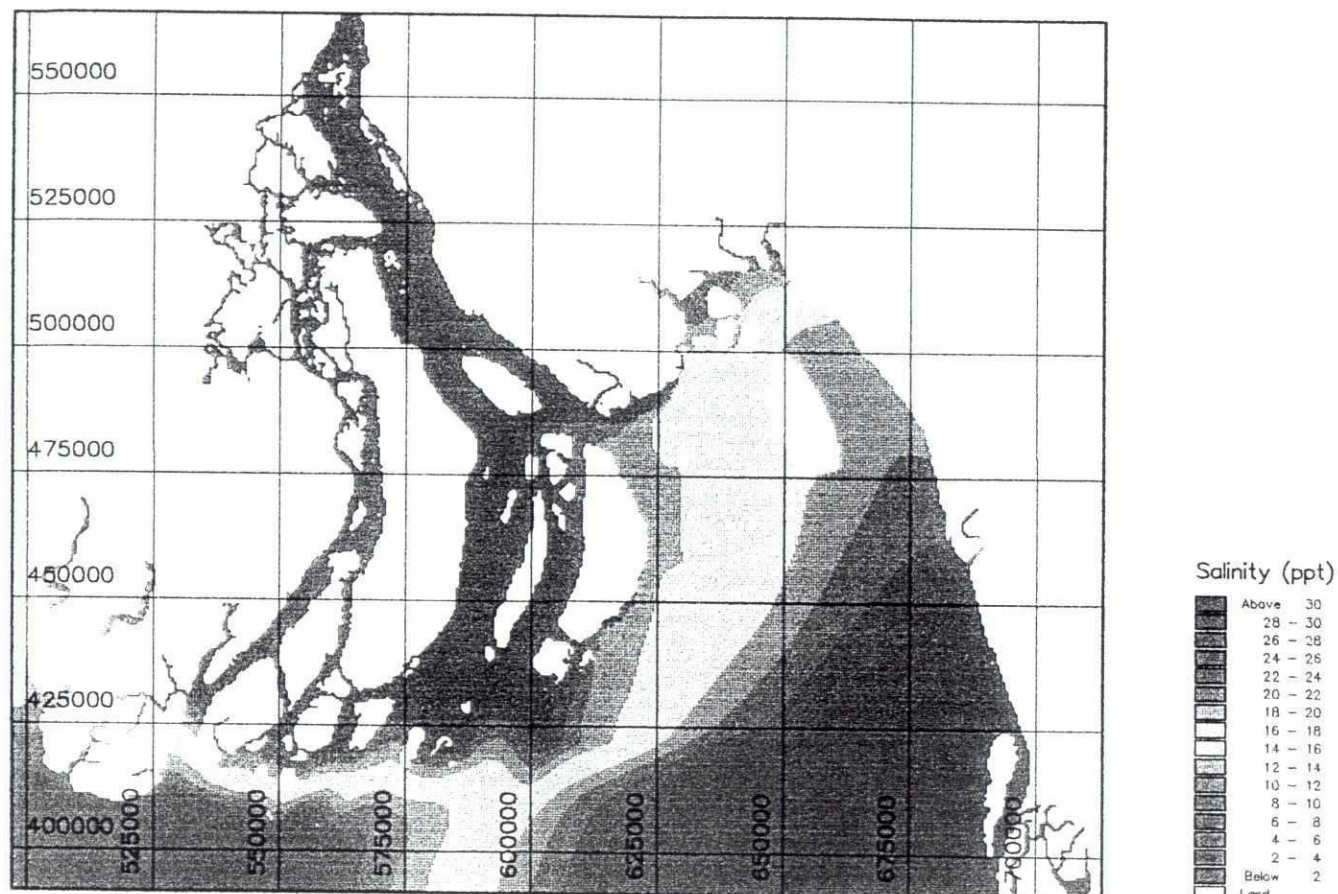
Salinity (ppt)



<div style="text-align: center; font-size: 24pt; font-weight: bold;">SWMC</div>		Client:	Bangladesh Water Development Board	MIKE 21
		Project:	Meghna Estuary Study	
File:	Date: Mon Jun 8 1998	Minimum salinities Dry season 1996 Existing situation		Drawing no. <div style="font-size: 24pt; font-weight: bold;">7.4</div>
Scale: 1:1500000	Int: p5011			



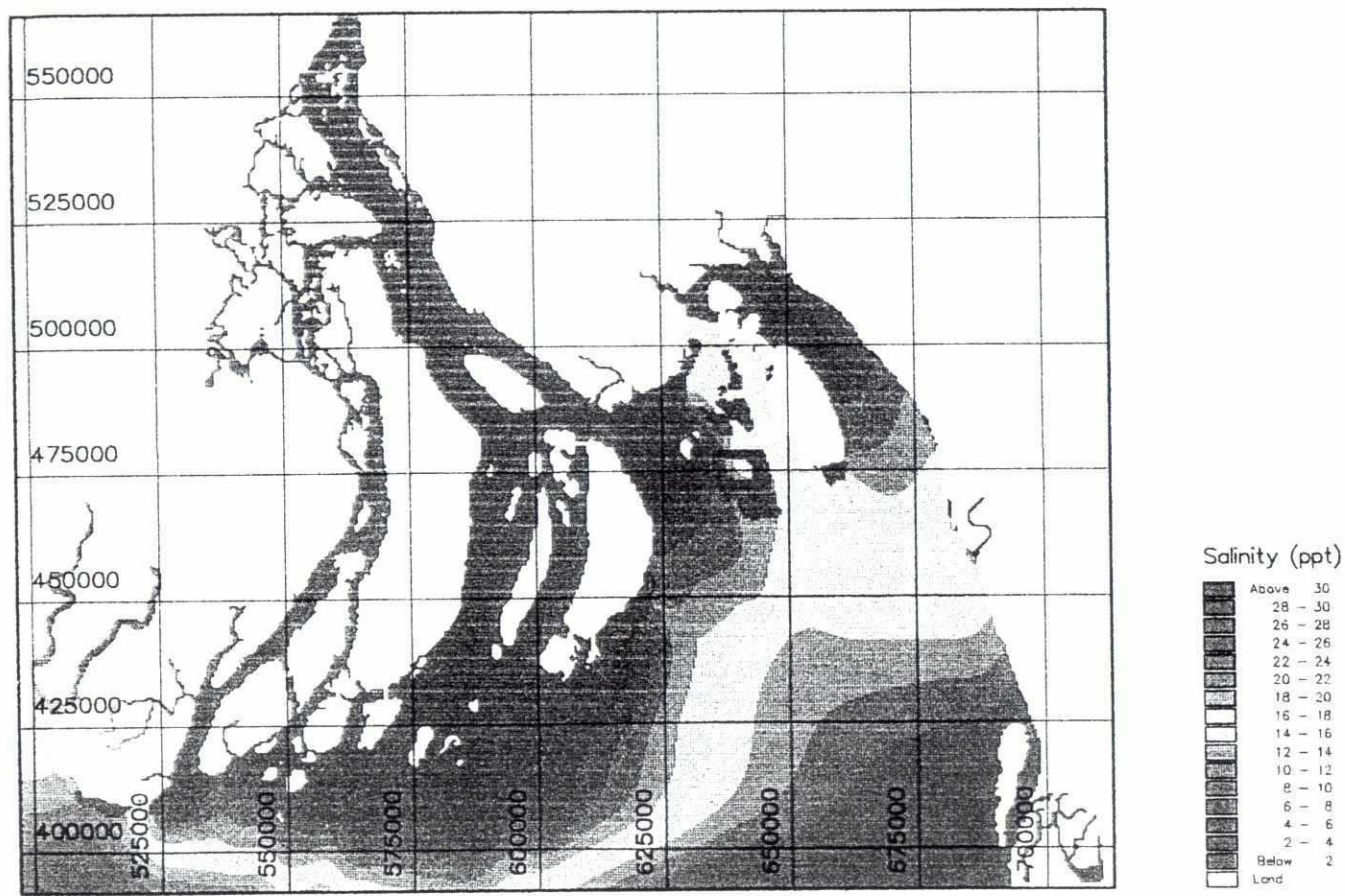
<div>SWMC</div>		Client:	Bangladesh Water Development Board	<div>MIKE 21</div>
		Project:	Meghna Estuary Study	
File:	Date: Mon Jun 8 1998	Mean salinities (ppt) Dry season 1996 Existing situation		Drawing no. 7.5
Scale: 1:1500000	Init: p5011			



SWMC		Client:	Bangladesh Water Development Board		MIKE 21
		Project:	Meghna Estuary Study		
File:	Date: Mon Jun 8 1998	Maximum salinities (ppt) Dry period 1996 Existing situation			Drawing no. 7.6
Scale: 1:1500000	Init: p5011				

280

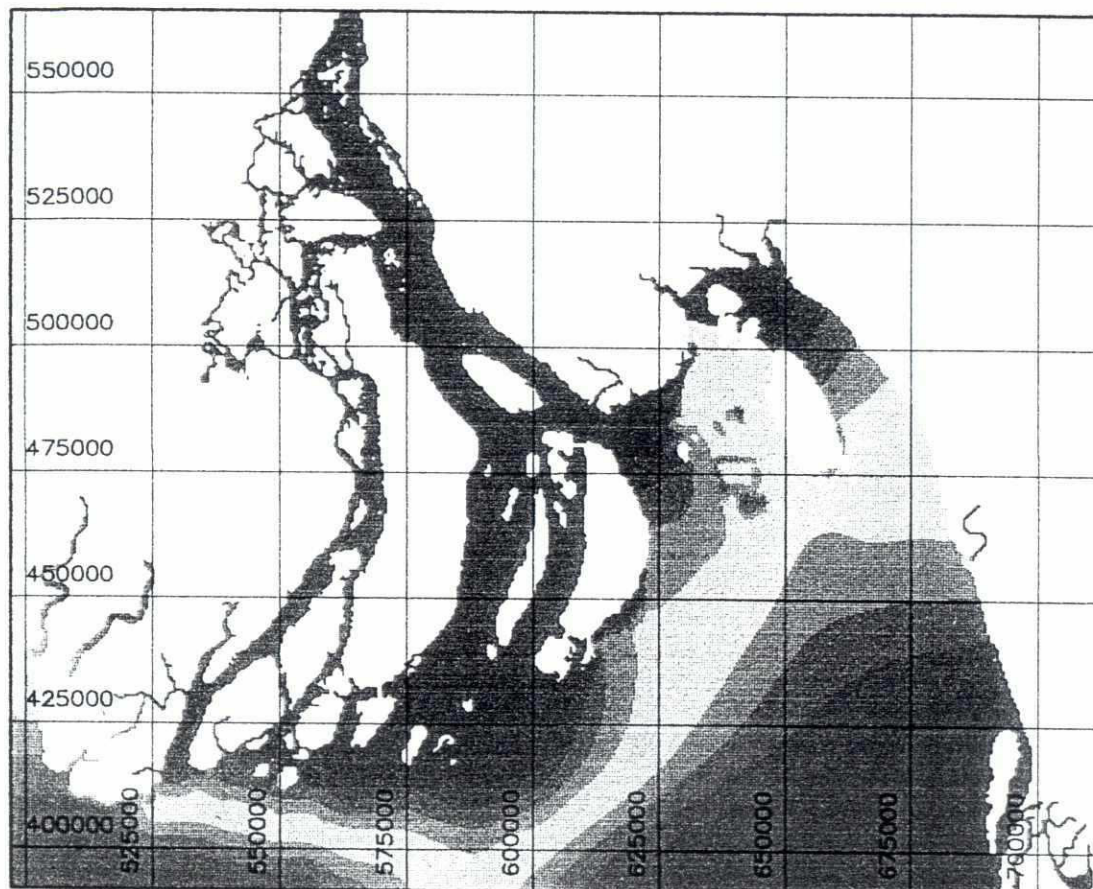
Page 21



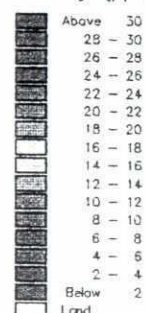
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		Project:	Meghna Estuary Study	
File:	Date: Mon Jun 8 1998	Minimum salinities (ppt) Dry period 1996 Including all interventions		Drawing no.
Scale: 1:1500000	Init: p5011			7.7

289

000000 10



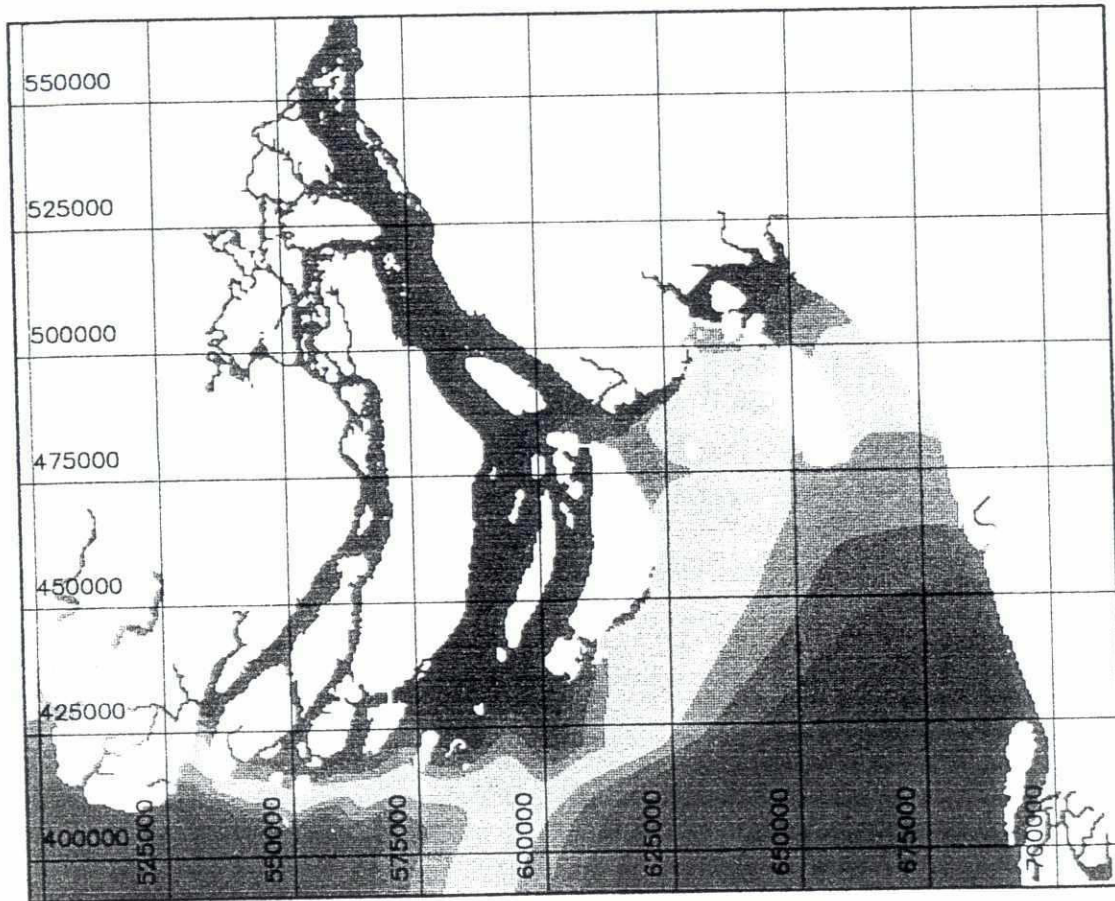
Salinity (ppt)



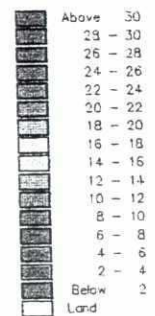
SWMC		Client:	Bangladesh Water Development Board		MIKE 21
		Project:	Meghna Estuary Study		
File:	Date: Mon Jun 8 1998	Mean salinities (ppt) Dry period 1996 Including all interventions		Drawing no. 7.8	
Scale: 1:1500000	Init: p5011				

209

00000 30



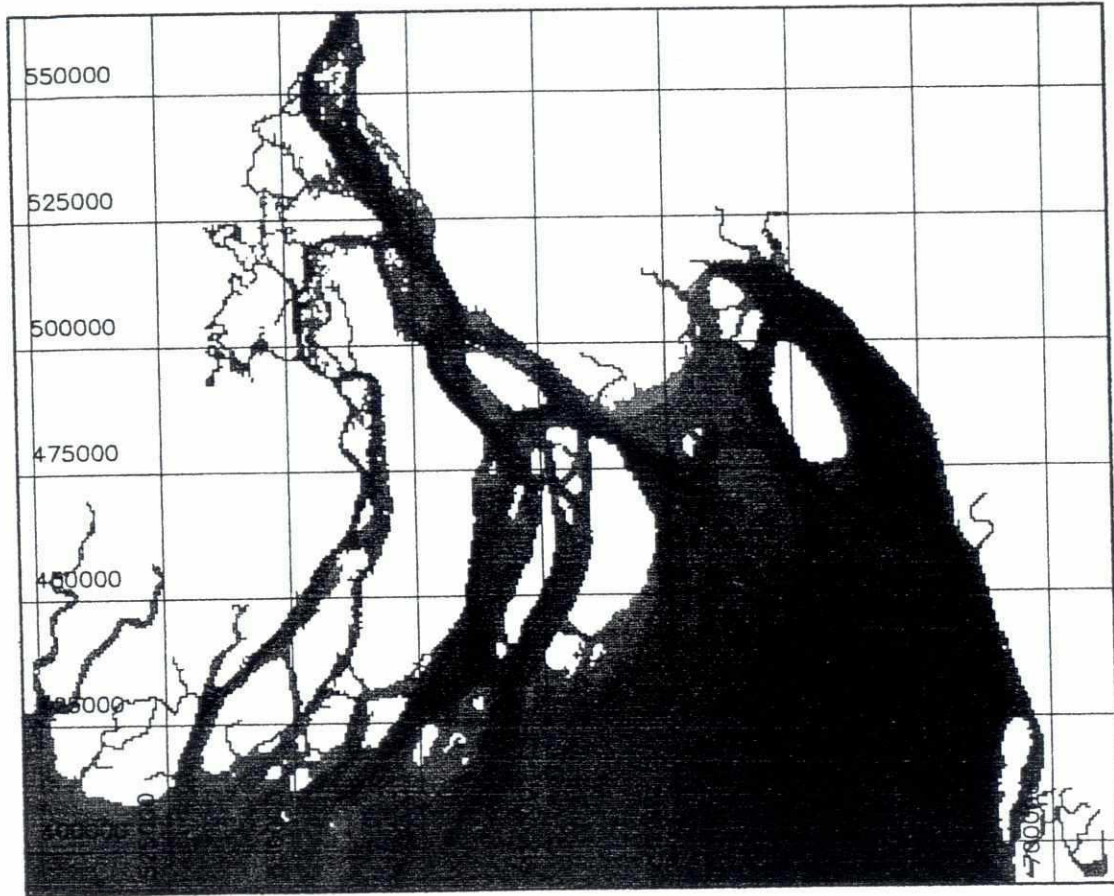
Salinity (ppt)



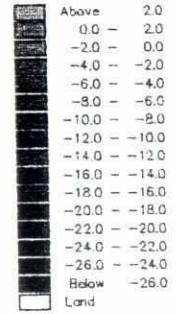
<div>SWMC</div>		Client:	Bangladesh Water Development Board	MIKE 21
		Project:	Meghna Estuary Study	
File:	Date: Mon Jun 8 1998	Maximum salinities (ppt) Dry period 1996 Including all interventions		Drawing no. 7.9
Scale: 1:1500000	Init: p5011			

201

1WS/4/004 4/00



Elevation (m PWD)



SWMC		Client: Bangladesh Water Development Board		MIKE 21
		Project: Meghna Estuary Study		
File:	Date: Mon Jun 8 1998	Model bathymetry for wind-wave model Meghna Estuary Model	Drawing no. 8.1	
Scale: 1:1500000	Int: p5011			

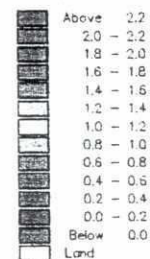
2000

1000000



5 m

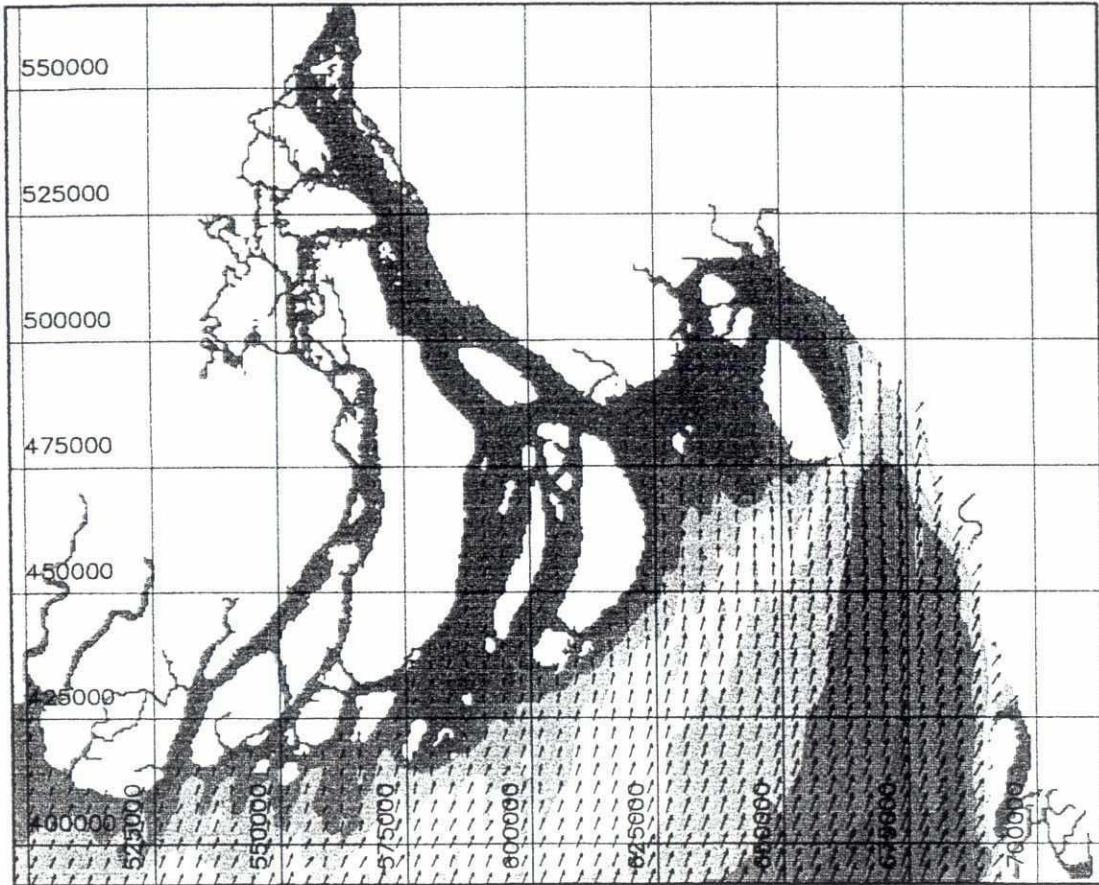
Hs (m)



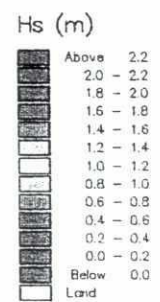
SWMC		Client:	Bangladesh Water Development Board		MIKE 21	
		Project:	Meghna Estuary Study			
File:	Date:	Waves from SSE, wind 8 m/s.				Drawing no.
Scale:	Init:					8.2
1:1500000	p5011					

250

10000 0000



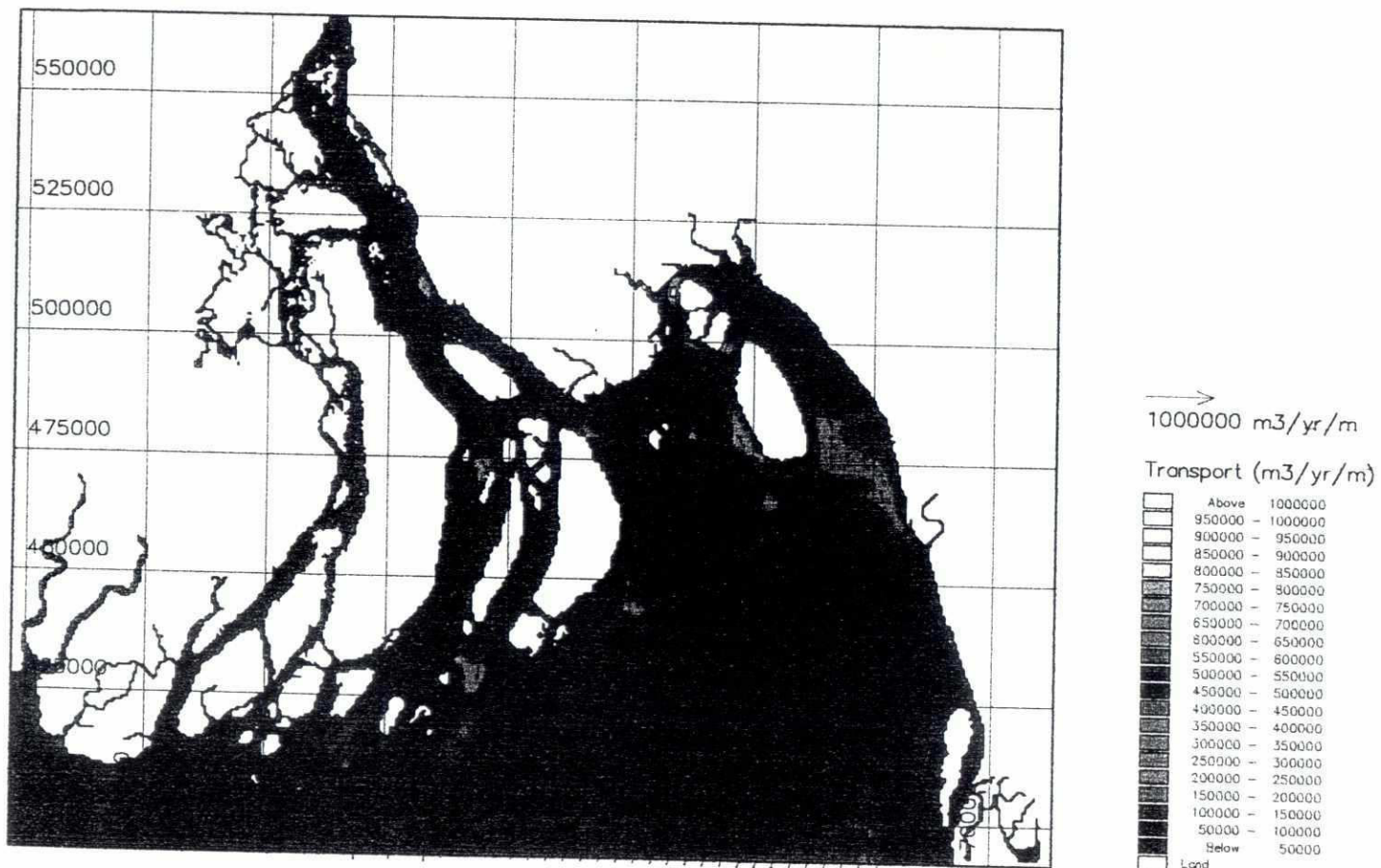
→
5 m



SWMC		Client:	Bangladesh Water Development Board	MIKE 21
		Project:	Meghna Estuary Study	
File:	Date: Mon Jun 8 1998	Waves from SSW, wind 8 m/s		Drawing no. 8.3
Scale: 1:1500000	Int: p5011			

250

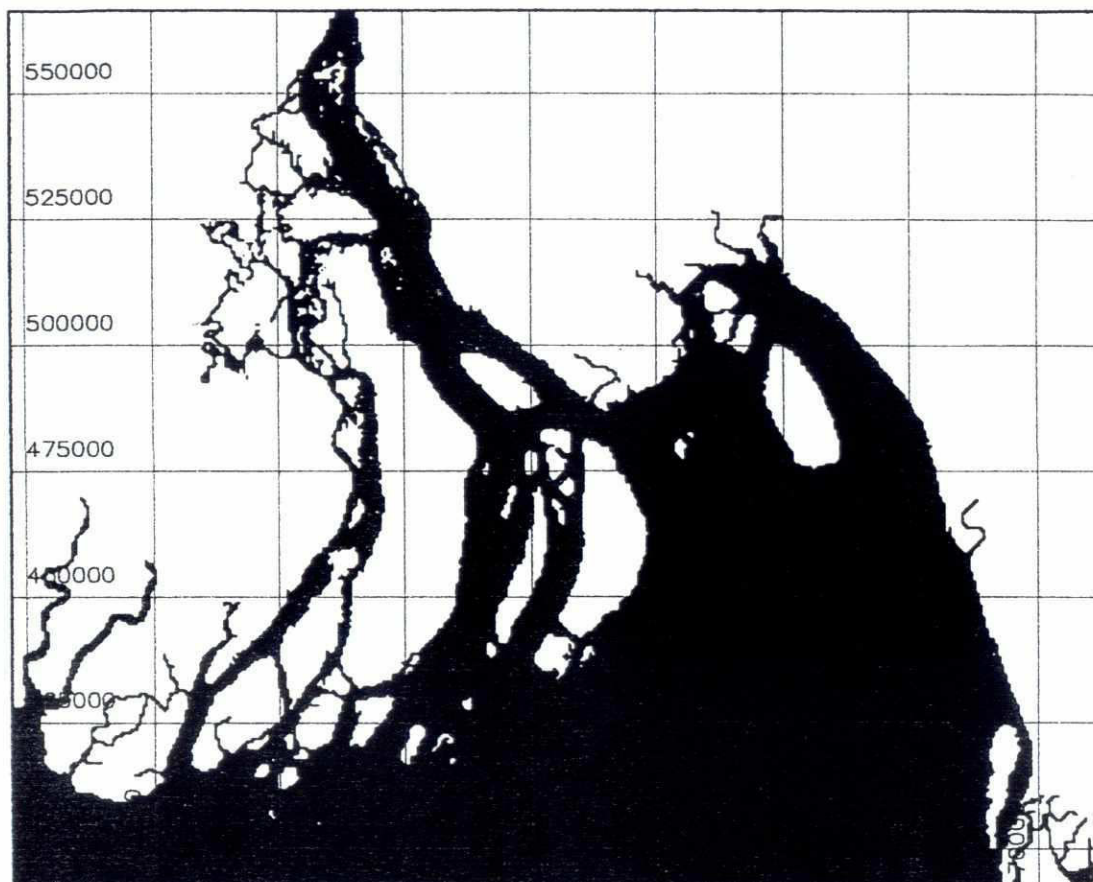
250



SWMC		Client: Bangladesh Water Development Board		MIKE 21	
		Project: Meghna Estuary Study			
File:	Date: Mon Jun 8 1998	Sediment transport rates Dry season 1997, Spring tide No waves			Drawing no. 9.1
Scale: 1:1500000	Init: p5011				

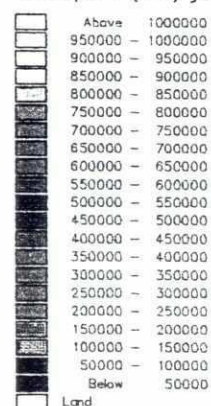
272

JAN 2000



→
1000000 m³/yr/m

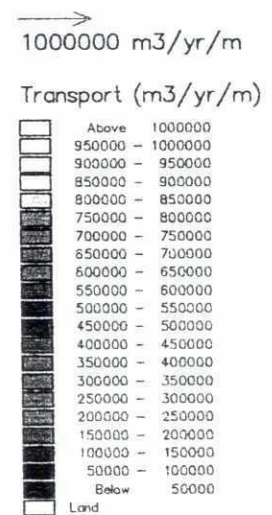
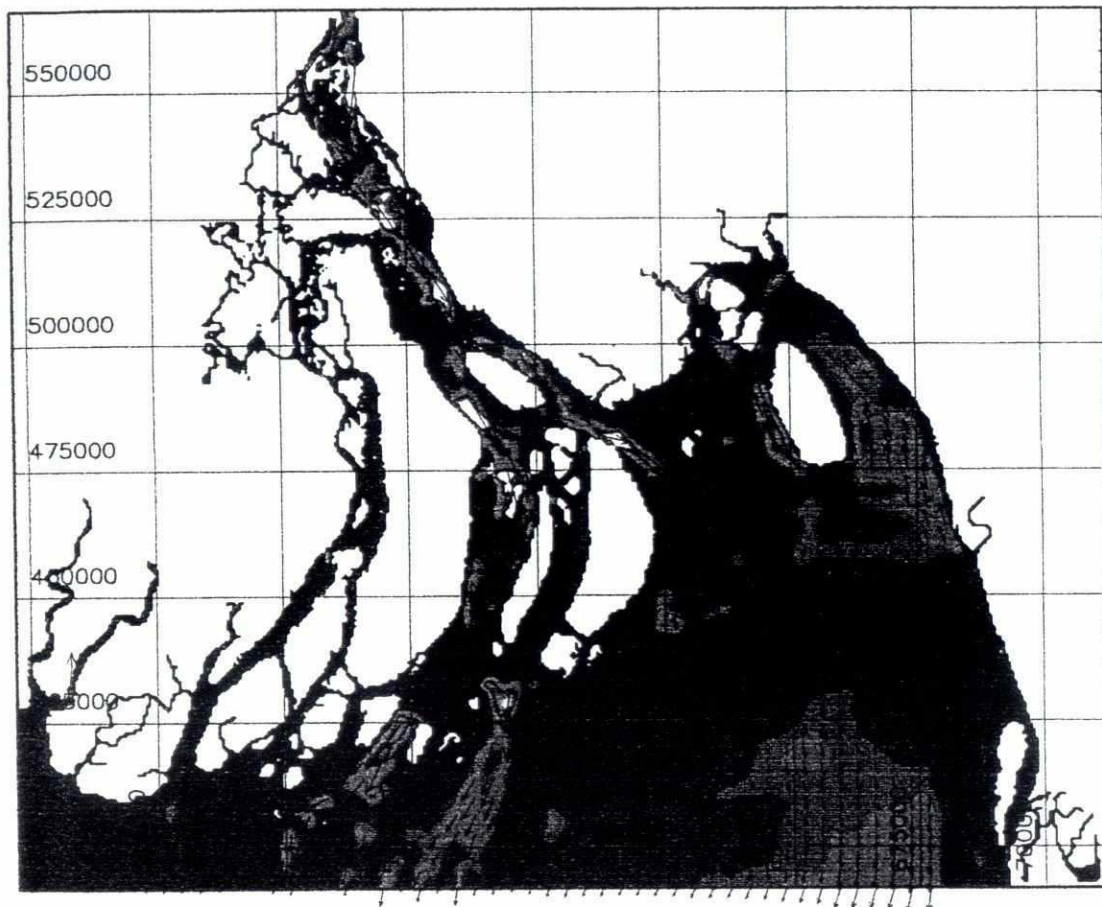
Transport (m³/yr/m)



SWMC		Client:	Bangladesh Water Development Board	MIKE 21	
		Project:	Meghna Estuary Study		
File:	Date: Mon Jun 8 1998	Sediment transport rates Dry season 1997, Neap tide No waves			Drawing no.
Scale: 1:1500000	Int: p5011				9.2

246

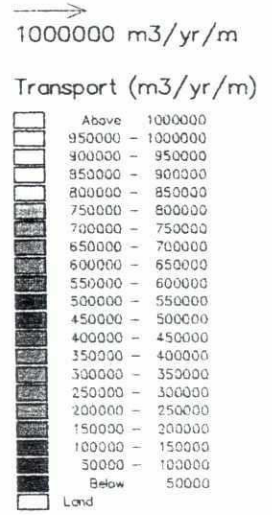
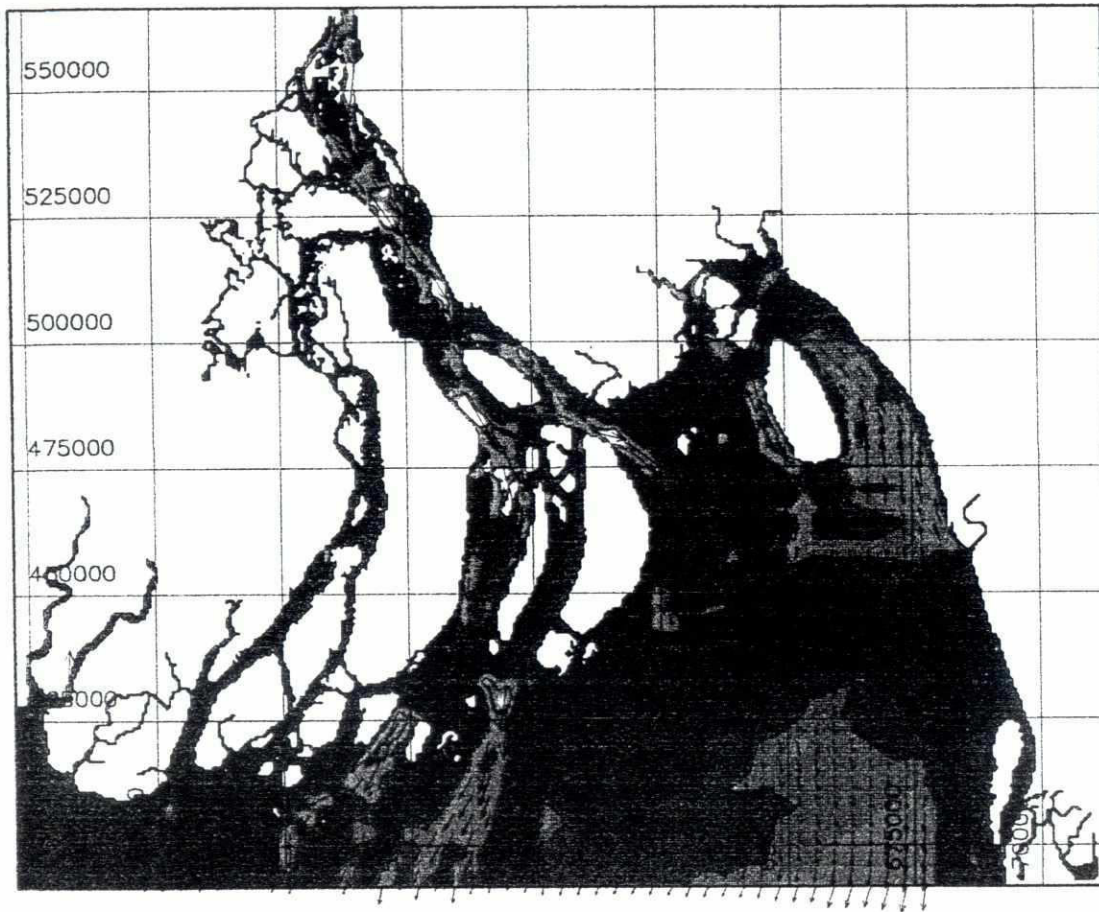
Latitude 18°



SWMC		Client: Bangladesh Water Development Board		MIKE 21
		Project: Meghna Estuary Study		
File:	Date: Mon Jun 8 1998	Sediment transport rates Monsoon 1997, Spring tide Waves corr. to wind of 8 m/s from SSE		Drawing no. 9.3
Scale: 1:1500000	Int: p5011			

208

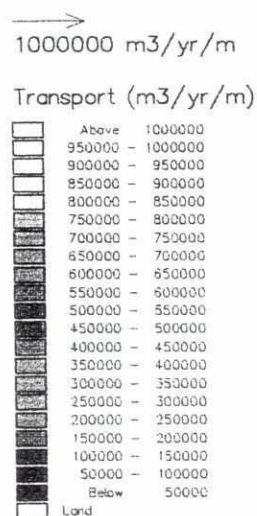
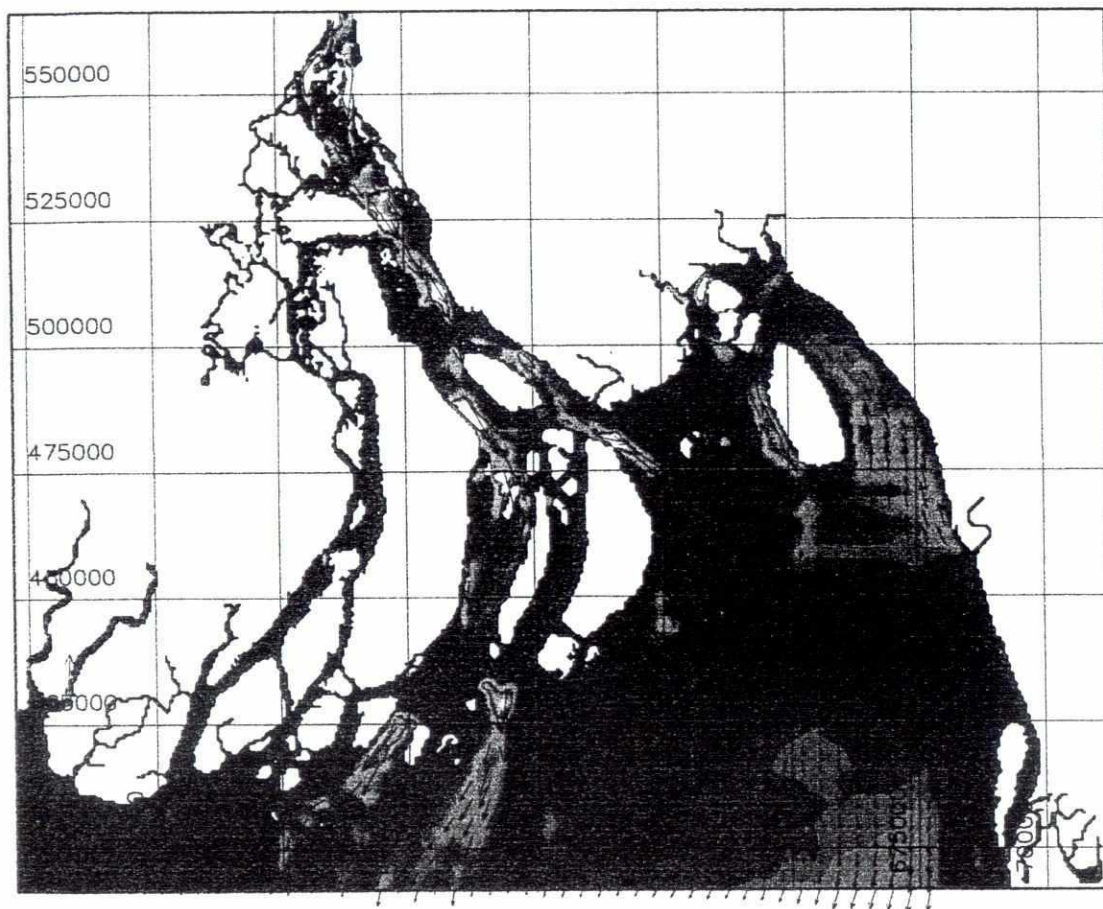
1:100,000



<div>SWMC</div>		Client:	Bangladesh Water Development Board	MIKE 21
		Project:	Meghna Estuary Study	
File:	Date: Mon Jun 8 1998	Sediment transport rates Monsoon 1997, Spring tide Waves corr. to wind of 8 m/s from SSW		Drawing no. 9.4
Scale: 1:1500000	Init: p5011			

250

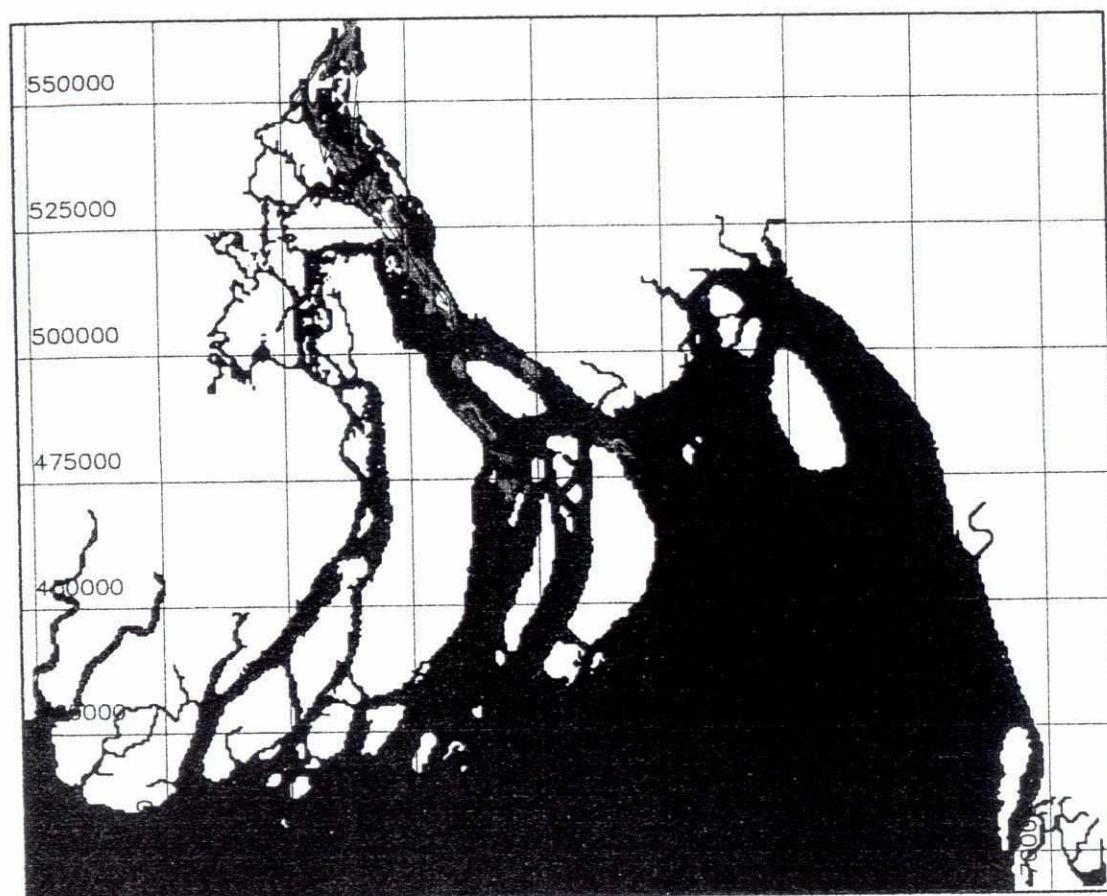
06/05/98



SWMC		Client:	Bangladesh Water Development Board		MIKE 21
		Project:	Meghna Estuary Study		
File:	Date: Mon Jun 8 1998	Sediment transport rates Monsoon 1997, Spring tide No waves			Drawing no. 9.5
Scale: 1:1500000	Int: p5011				

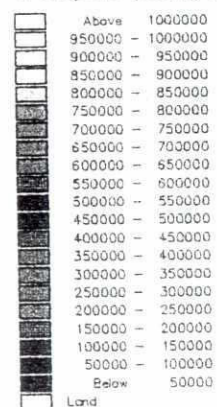
255

1.000000



→ 1000000 m³/yr/m

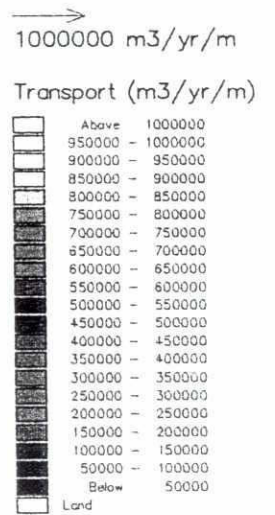
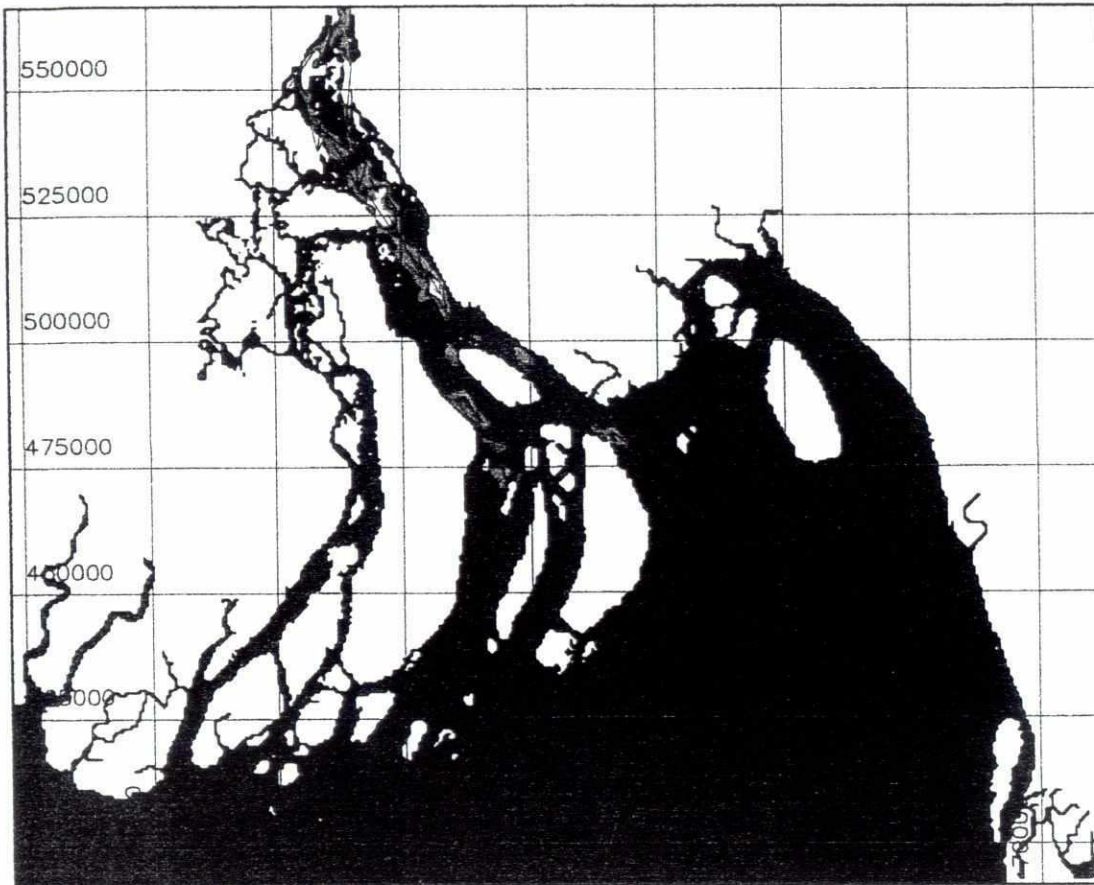
Transport (m³/yr/m)



SWMC		Client:	Bangladesh Water Development Board	MIKE 21
		Project:	Meghna Estuary Study	
File:	Date: Mon Jun 8 1998	Sediment transport rates Monsoon 1997, Neap tide Waves corr. to wind of 8 m/s from SSE		Drawing no. 9'6
Scale: 1:1500000	Int: p5011			

259

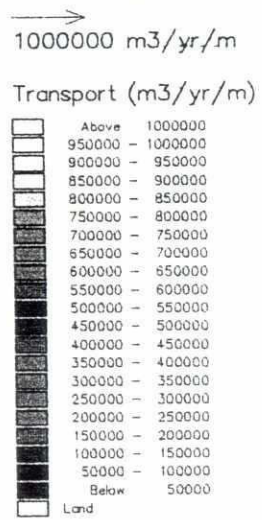
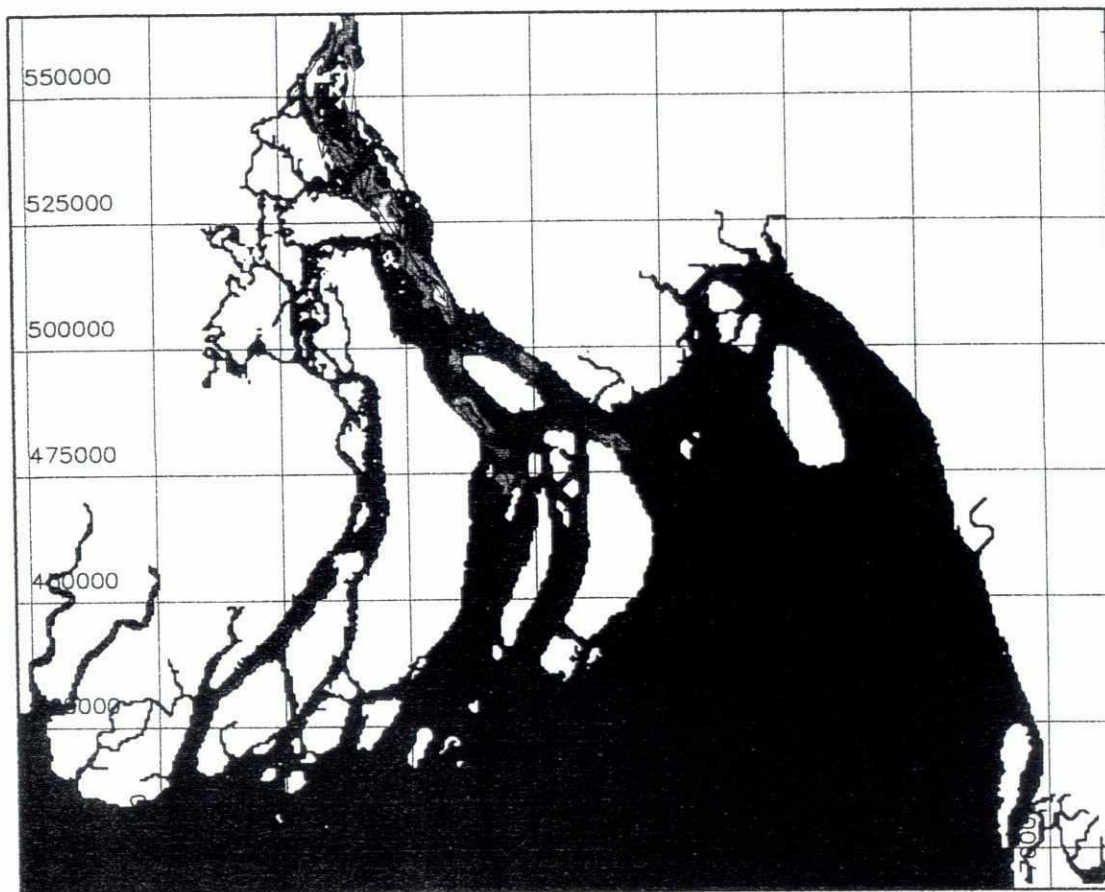
259



SWMC		Client:	Bangladesh Water Development Board	MIKE 21
		Project:	Meghna Estuary Study	
File:	Date: Mon Jun 8 1998	Sediment transport rates Monsoon 1997, Neap tide Waves corr. to wind of 8 m/s from SSW		Drawing no. 9.7
Scale: 1:1500000	Int: p5011			

258

1.00000000



SWMC		Client:	Bangladesh Water Development Board		MIKE 21
		Project:	Meghna Estuary Study		
File:	Date: Mon Jun 8 1998	Sediment transport rates Monsoon 1997, Neap tide No waves			Drawing no.
Scale: 1:1500000	Init: p5011				9.8

